



A RAND NOTE

Appendices to PACER SHARE Productivity and Personnel Management Demonstration Baseline Evaluation

Bruce R. Orvis, James R. Hosek, Michael G. Mattock

December 1990



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92-07376

The research described in this report was sponsored by the Assistant Secretary of Defense (Force Management and Personnel) under RAND's National Defense Research Institute, a federally funded research and development center supported by the Office of the Secretary of Defense and the Joint Chiefs of Staff, Contract No. MDA903-85-C-0030.

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	2. RECIPIENT'S CATALOG NUMBER
N-3146-FMP		
4. TITLE (and Subtitle)	<u> </u>	S. TYPE OF REPORT & PERIOD COVERED
Appendices to PACER SHARE product	ivity and	interim
Personnel Management Demonstration	n Baseline	
Evaluation		4. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(e)		S. CONTRACT OR GRANT NUMBER(s)
B. R. Orvis, J.R. Hosek, M. G	Mattock	
L.A. Haigazian, A. K. Ludwig	· Hattock,	MDA903-90-C-0004
<u> </u>		
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
RAND		THE THOUSAND WOLLDEN
1700 Main Street		
Santa Monica, CA 90401	· · · · · · · · · · · · · · · · · · ·	
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
Office, Assistant Secretary of De	fense for Force	December 1990
Management & Personnell		292
14. MONITORING AGENCY NAME & ADDRESS H Millorent	trem Controlling Office)	18. SECURITY CLASS. (of this report)
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•		15a, DECLASSIFICATION/DOWNGRADING
	, ——, —, —, —, —, —, —, —, —, —	
16. DISTRIBUTION STATEMENT (of this Report)		į
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No Restrictions		
18. SUPPLEMENTARY NOTES		
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19. KEY WORDS (Continue on reverse side if necessary and	identify by block number)	
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Productivity Mili	tary Personnel	ĺ
Test and Evaluation		i
Personnel Management		•
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December 1990

Prepared for the Assistant Secretary of Defense (Force Management and Personnel)



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PREFACE

This volume contains the appendixes to R-3753-FMP, which describes the PACER SHARE Productivity and Personnel Management Demonstration and the plan that has been developed to evaluate it. The report also presents statistical results concerning quality of worklife, organizational flexibility, and work quality during the baseline period before the demonstration. The appendixes contain information on the demonstration, the survey questionnaire used in the baseline evaluation, and supplementary statistical results.

This study is funded by the U.S. Air Force through a special arrangement with the Office of the Assistant Secretary of Defense (Force Management and Personnel), the research sponsor. It is being carried out by the Defense Manpower Research Center, a component of The RAND Corporation's National Defense Research Institute, a federally funded research and development center sponsored by the Office of the Secretary of Defense and the Joint Chiefs of Staff.

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Appendix A

DEMONSTRATION BACKGROUND AND INTERVENTIONS

This appendix is a more detailed version of some of the material in Sec. I of R-3753-FMP. It includes expanded treatment of PACER SHARE's interventions and intended effects and concludes with a comparison of PACER SHARE with other Office of Personnel Management (OPM) demonstrations. The material is drawn from the description of PACER SHARE provided in the Federal Register, Vol. 52, No. 224, November 20, 1987.

THE PACER SHARE INTERVENTIONS

Following are detailed descriptions of the five system changes instituted in the PACER SHARE demonstration project at SM-ALC, including:

- Job series consolidation.
- · Revised base pay determination.
- Revised supervisory grading criteria.
- Revised hiring/retention criteria.
- Productivity gainsharing.

Job Series Consolidation

Purpose. This intervention replaces the General Schedule (GS) and Federal Wage System (FWS) classification systems, consolidating 66 current job series into six broadly defined processes. The regrouping aims to improve responsiveness to work and mission requirements by allowing an individual to be assigned to any job in a process for which he is qualified. It should also enrich the quality of worklife through expanded career and training opportunities, because multiple skill training will be provided to take advantage of the flexibility in making job assignments. Finally, the intervention should improve the job classification process by reducing the paperwork and complexity associated with narrowly defined job series.

Classification System. Both the PACER SHARE and traditional job classification systems classify work at different levels to reflect differences in difficulty and responsibilities. However, under the new system, substantially fewer classification levels are used. The job series have been consolidated according to three classification structures, each corresponding to a new pay schedule:

- Demonstration Hourly (DH), covering all Wage Grade and Wage Leader nonsupervisory positions
- Demonstration Salaried (DW), covering all GS nonsupervisory positions
- 3. Demonstration Supervisory (DX), covering all supervisory positions.

The allocation of work to specific categories in the demonstration system is based on contribution to a common outcome (product or service). Each category represents a "process," defined as "the progressive and interdependent arrangement of events, machines, methods, and resources that produce a good or service." Work contributing to the same goal is allocated to the same process; the tasks, knowledges, skills, and abilities required may vary.

Within the DH class, 27 FWS series are consolidated into two processes (see Table A.1):

- Material Handling Process encompasses physically receiving, examining, packing, moving, storing, and issuing items.
- Facilities and Equipment Maintenance encompasses physically maintaining and repairing material processing equipment and facilities.

Within the DW class, 39 GS series positions are consolidated into three processes:

Table A.1

HOW PREDEMONSTRATION JOB SERIES ARE GROUPED INTO DEMONSTRATION PROCESSES AND SUBPROCESSES

	ocess (DW-9200)		Tachnical Support Subprocess
GS-301	Contractor Monitor	GS-818	Engineering Draftsman
GS-1152	Production Control	GS-895	Industrial Engineering Technician
GS-1910	Quality Assurance		
GS-2001	General Supply Specialist		
GS-2003	Supply Management	Administration	" B (D1/ 0.100)
GS-2005	Supply Management Supply Clerk/Technician	matenai Handi	ing Process (DH-9400)
		WG-3502	Laboring
GS-2010	Inventory Management	WG-4602	
GS-203 0	Storage/Distribution Facilities		Blocking and Bracing
	Specialist	WG-4604	Wood Working
GS-2032	Packaging Specialist	WG-5413	Fuel Distribution Systems Operating
GS-2101	Transportation Specialist	WG-5703	Motor Vehicle Operating
GS-2102	Transportation Clerk and Assistant	WG-5704	Fork Lift Operating
GS-2130	Traffic Management Specialist	WG-5706	Road Sweeper Operating
GS-2131	Freight Rate Specialist/Assistant	WG-5725	Crane Operating
GS-2132	Travel Assistant/Clerk	WG-6901	General Equipment Examining
GS-2134	Shipment Clerk	WG-6904	Tool and Parts Attending
GS-2135	Transportation Loss/Damage	WG-6907	Warehouse Working
	Claims Examiner	WG-6910	Material Expediting
GS-2144	Cargo Scheduler	WG-6968	Aircraft Freight Loading
GS-2150	Terminal Management/	WG-7002	Packing
	Transportation Services	WG-7004	Preservation Packaging
GS-2151	Dispatcher		
		Facilities and I	Equipment Maintenance
anagoment (Operations Process (DW-9201)	Process (DH-	
_		Electronic S	·
GS-260	EEO Specialist		
GS-301	Administrative Specialist/Quality	WG-2606	Electronic Industrial Controls Mechanic
00.004	Circle Facilitator	WG-2610	Electronic Integrated Systems Mechan
GS-301	Human Resources Analyst	Classical Co	h
GS-301	Industrial Management Relations	Electrical Su	oprocess
GS-301	Specialist Reserve Affairs Coordinator	WG-2805	Electrician
GS-303	Clerk/Assistant/Technician	Metal Workin	ng Subprocess
GS-305	File Clerk/Assistant		3
GS-318	Secretary	WG-3414	Machinist
GS-322	Clerk-Typist	WG-3806	Sheet Metal Mechanic
GS-332	Computer Operator		
GS-334	Computer Programmer/Analyst	Painting Sub	process
GS-343	Management Analyst	WG-4102	Painting
GS-344	Management Clerk/Assistant		
GS-345	Program Analyst	WG-4104	Sign Painting
		Carpentry St	uborocess
GS-356	Data Transcriber	ourpoint, o	50p.00035
GS-392	Communications Operator	WG-4605	Woodcraftsman
GS-560	Budget Analyst	WG-4607	Carpentry
GS-1001	Graphic Arts		
GS-1020	Illustrator	Industrial Eq	uipment Repair Subprocess
GS-1 531	Statistical Clerk/Assistant	WG-5352	Industrial Equipment Mechanic
			oment Repair Subprocess
ngineerina Pi	rocess (DW-9202)	• •	·
	Engineering Subprocess	WG-5803 WG-5806	Heavy Mobile Equipment Mechanic Mobile Equipment Servicing
		#G-360 0	moone Equipment octationing
GS-801	General Engineer	Cupaniaca: D	
GS-896 GS-899	Industrial Engineer Engineering Student Trainee	Supervisory P	rocess (DX-9300)
JJ 133	Chymeeting Otal Chi Hamee	All GS super	visory positions
			ervisory positions (WS)

- Distribution Process covers all custody and transportation transactions.
- Management Operations Process covers clerical and general management administrative work.
- Engineering Process covers all engineering services.

Within the DX class, all supervisory positions have been consolidated into one process.

Since the processes (and classification levels, see below) under FACER SHARE are broadly defined, work allocation is simplified and required paperwork, classification actions, and promotions are reduced. Only one classification standard is used for each process, incorporating four sets of grading criteria (see below).

Revised Base Pay Determination

Purpose. Base pay determination is revised to achieve three basic grals: (1) allow employees greater salary potential without formal primotion procedures, (2) allow managers more flexibility in the assignment of work, and (3) shift incentives away from individual rewards. The need for formal promotions will be reduced because they will apply only to movement across the four broad pay bands instead of the more narrowly defined current grades. There are four pay bands for each of three classification structures. Each corresponds to a range of GO/GM or FWS grades. Also, through the increased salary potential within bands, pay inversion can be addressed. Historically, pay inversion has served as a potential motivation for migration to FWS positions. The uncertainty of promotion also will be replaced by a predictable pay progression system. Within each band, employees may perform work of varied difficulty and responsibility corresponding to the range of traditional grades. This broadening of potential duties within a single classification level should facilitate the assignment of work to meet the organization's needs. Finally, by deemphasizing individual performance reviews, this intervention will reinforce the emphasis on organizational-level productivity that is the goal of productivity gainsharing.

New Pay Schedules. As noted, the new system consists of three pay schedules covering all employees: blue-collar (DH), white-collar (DW), and supervisory (DX). Within each schedule, current pay grades are banded into broad levels (see Table A.2). The new schedules retain overlapping levels of pay; a senior employee in a lower band may receive higher basic pay than a new employee in the next band up.

The DH pay schedule will be adjusted in accordance with annual Sacramento area wage survey results. The DW schedule will be adjusted whenever a comparability increase changes the GS. Because the DX schedule is based on the DW schedule, it will be adjusted whenever the DW schedule is adjusted.

Table A.2

DEMONSTRATION PAY SCHEDULES AND BANDS

New Pay Schedule	Current Schedule
and Band	and Grades
DH	FWS
2	75
DH-1	WG-1 to WG-3
DH-2	WG-4 to WG-8
DH-3	WG-9 to WG-11
DH-4	WG-12 to WG-15
DW	GS
DW-1	GS-1 to GS-4
DW-2	GS-5 to GS-8
DW-3	GS-9 to GS-12
DW-4	GS-13 to GS-15
DX	GS
DA	93
DX-1	GS-5 to GS-8
DX-2	GS-9 to GS-12
DX-3	GS-13 to GS-14
DX-4	GS-15

Eliminating Individual Annual Performance Ratings. Under this change, annual performance appraisals with their performance elements, standards, and achievement ratings will no longer be used as a basis for movement within the pay bands. It has been hypothesized that individual performance appraisals are counterproductive because they encourage rivalry and short-term performance at the expense of teamwork and long-term planning. Cooperation is especially important in an organization like DS where work units are interdependent. This intervention dispenses with individual ratings, allowing the time and effort entailed in producing them to be allocated elsewhere.

Nonetheless, some individual incentives remain. Employees may still be promoted from band to band, they will find their career opportunities enhanced through increased cross-training, and on-call workers may earn conversion to career status.

Pay Progression. Within-grade increases, quality step increases, merit increases under the Performance Management and Recognition System, and promotions to grades contained within a given pay band will be replaced by annual pay adjustments. Each employee whose pay is below the upper limit of a pay band will receive a fixed percentage increase to base pay. The increase will be based on which pay band the employee is in and his time in the band, and the length of time set for progression through the band (12 years for DH bands, 25 years for DW-1-3 tands, 16 years for DW-4 and DX-3 bands, and 11 years for DX-4).

Promotions will result in a 10 percent increase to current pay or receipt of the minimum basic pay of the new level, whichever is greater. Employees promoted into the demonstration project will have their pay established by GS and FWS pay-setting practices.

Revised Supervisory Grading Criteria

Purpose. The revised supervisory grading criteria should provide a more flexible system. All supervisors will be placed into the "Supervisory Process" with four pay bands (see Table A.2) based on actual job responsibilities. This "Supervisory Process" consolidates current differences in supervisory job series and pay schedules.

The intervention should increase organizational flexibility in assigning supervisors to the positions where they are most needed by eliminating the need for a specific subordinate structure to be in place. It should also reduce supervisors' disinclination to recommend appropriate staff reductions, because their salaries will no longer be based on the numbers and grades of subordinates supervised. This flexibility in turn should lead to a more optimal organizational structure and improved supervision. By definition, supervisors' pay will become more dependent on their actual job responsibilities. The consolidation of all supervisory and managerial positions into a single process also will establish supervision and management as a distinct career field and should help to reduce pressure on senior level technicians, professionals, and trades personnel to become supervisors in order to realize salary advancement.

Supervisory Position Grading Criteria. The classification of supervisory and managerial positions under the demonstration project aims to emphasize the supervisors' importance to the organization. Six classification criteria with several levels each will be used to base supervisors' pay on their job responsibilities and the difficulty of executing those responsibilities. Points are assigned for each of the six classification criteria; the classification level then is determined based on the total number of points. The six criteria are (1) workload of the organizational unit; (2) position criticality; (3) degree and scope of responsibility delegated; (4) level and purpose of contacts; (5) kind, degree, and character of supervision exercised; and (6) planning horizon. The initial conversion will be made according to the grade conversions shown in Table A.2 (or their salary equivalents).

Revised Hiring/Retention Criteria

Purpose. The traditional on-call hiring authority has been revised to a Demonstration On-Call (DOC) program. For DOC appointees, there will be no automatic conversion to career status after three years; the complex, formal reduction in force (RIF) procedures will not be required for termination if a RIF is mandated; and a ten-day release and recall

notification period will be applicable. The program's main goal is to increase the organization's capability to rapidly adjust the size of the workforce in response to workload and budgetary changes and still retain key skills and personnel. Considerable flexibility should be gained because the ten-day release and recall provision applies to all DOC employees, who are expected to constitute 25 percent of the workforce. Also, by limiting workforce adjustments to DOC employees, the effect can be limited to a segment of the workforce. Potential RIF costs would also be reduced.

Characteristics of the DOC Program. Normally, employees will be hired into the DOC program. They will be given career-conditional appointments and work regular tours. Current career-conditional and career employees will be excluded but may work the on-call schedules consistent with existing provisions (for other than full-time career employment).

Conversion of DOC employees from career-conditional to permanent career status will depend on the needs of DS and employee seniority. A minimum of one year of DOC service will be required. Seniority will be determined based on the date of entry into DS. Although conversion to career status after three years will not be automatic, the planned percentage of career employees will remain close to its predemonstration level. Most individuals should be eligible for conversion after three years, assuming the conversion is consistent with the needs of the organization at the time.

Management will attempt to confine workforce adjustments to DOC employees. First, the processes and levels affected will be determined. DOC employees will then be released (or separated) on the basis of veteran preference and seniority. They subsequently will be entitled to priority placement over new hires for a period of one year.

Productivity Gainsharing

Purpose. Productivity gainsharing provides an extrinsic (economic) incentive to DS employees that should help them and the Air Force realize the opportunities for greater productivity made possible by the accompanying changes in the personnel system and intrinsic (noneconomic) motivators. It is designed to equally distribute the benefits earned by employees and the organization.

The desired effect is to provide a direct connection between organizational performance and individual compensation. The Directorate of Distribution will pay equal dollar shares to all employees; this practice is consistent with the DS organizational perspective. Payments will not be tied to individual performance appraisals, which will be eliminated, and will not provide an incentive for branches or divisions within DS to perform work of uncertain value or lower priority to DS as a whole in an attempt to maximize their own workload indicators. The organization approach also prevents problems concerning inequity of opportunity to earn gainshares within DS. This issue is potentially important, given possible differences in the ability of the individual divisions, branches, and sections within DS to control treir own workloads. Gainsharing is also intended to reinforce the current Quality Circle program in DS, by providing a stronger (financial) incentive to participate.

Characteristics of Productivity Gainsharing. Gainsharing will be based exclusively on labor costs, which account for more than 90 percent of total controllable costs. Productivity will be defined as the ratio of work completed to labor dollars expended. Therefore, increases in productivity will be based on increased efficiency in the use of personnel dollars by DS. Such cost savings will be realized only by performing the same work for fewer labor dollars or performing more work for the same labor cost. Thus, unless the workload and funding for DS are increased during the project, the major source of cost savings will be through the ability of the workforce to absorb the workload of employees who leave through natural attrition.

Gainsharing will be based on a quarterly assessment of the labor cost for the actual level and mix of outputs achieved. The cost of producing that level and mix of outputs will be compared with the estimate of what it would have cost to produce the same output during the predemonstration period. If it is determined that there are savings, half of the savings will be returned directly to the Air Force; the remaining half will be split in equal dollar shares among the workers.

RISKS OF THE DEMONSTRATION

Organizational change can involve risk whenever there is uncertainty about how to implement specific changes and the range of their possible outcomes. If the expected outcomes were certain and positive, the changes would be made immediately, barring some factor beyond the organization's control. The interventions of the Sacramento work incentive demonstration are designed to improve the organization, but an intervention could have negative outcomes. Analysts and the proponents of the demonstration must be aware of downside risks, both to ensure the evaluation accounts for them and to understand why the interventions were, or were not, effective.

The following examples, though by no means exhaustive, illustrate negative outcomes that could arise during the demonstration from individual interventions. These issues will be considered at greater length in the annual evaluation reports of the demonstration's outcomes. The reports also will examine the interrelationships among the interventions that are required if they are to be effective—for example, whether the training required to improve responsiveness to workload under series consolidation and pay banding was provided.

Negative Feedback Created by Eliminating Performance Appraisals

The elimination of appraisals may lead workers to believe that their individual efforts will not be recognized or, even if they were recognized, would not increase their pay, which, in their view, should be commensurate with the greater effort expended. Fixed annual

increases will not be tied to their individual performance, however imperfectly measured; instead, they will be set at the same rate for others within the same pay band and could be augmented if a gainshare were paid. By weakening the link between individual effort and individual reward, the worker's incentive to shirk could increase. If that occurred, the productivity of organizational labor would be less likely to increase, and could decrease.

Inefficient Expansion of Supervisory Positions

The supervisory grading intervention permits supervisory positions to be established with fewer subordinate positions than typically required under the current system. It therefore becomes possible to increase the number of supervisors for a given workforce. If supervisory positions are not created in a way that improves efficiency, organization labor productivity might decrease.

Adverse Drift in Productivity Standards

For the purpose of managing the demonstration, cost savings will be computed by an aggregate approach (outlined in Sec. I of the report) that depends on productivity standards. These standards may be periodically reviewed and revised. Although the methods for standard setting are documented and carefully applied, there is room for judgment; thus there will be some variance in the standard that might be chosen. If, by chance, revised standards—unit costs—tended to be set on the low side, then the computation of labor productivity would be biased down, reducing the chance of a gainshare; as a result, the employees could believe that their efforts to be more industrious and innovative were not paying off and they might not make any greater effort than before the demonstration. Further, their effort might conceivably be lower if they mistakenly thought that the downward drift had been caused by their greater effort.

Higher Outflow of Workers Because of Expanded Training

Under the consolidated job series intervention, workers must be given multiple skill training. The additional training should qualify them for a wider range of jobs in both the public and private sectors. If pay did not rise commensurately with these expanded opportunities, the outflow of workers would increase once they had been trained. Thus, Sacramento would be spending more to train workers and having a reduced expected payoff period. The higher training and turnover costs could increase the cost of a given workload relative to the current system.

Higher Outflow of Workers From Pay Banding

Workers eligible to compete for promotions under the current system will not be able to do so (within DS) under pay banding if the grade falls within the same band (e.g., GS-9 to GS-11). Since dissatisfaction is likely to result from perceived opportunities as well as actual qualification for such promotions, migration and separation rates could increase. Turnover could also increase among individuals whose nearterm step increases exceed their annual pay adjustments under PACER SHARE. Such persons would tend to be drawn from the lower steps within a grade and, thus, from those recently promoted.

Unexpectedly Fast Wage Growth

All workers in a given pay band (or those in the upper or lower half) will receive the same annual relative pay growth. The rate of increase is intended to allow workers' pay (exclusive of gainshare) to rise as fast during the demonstration as it otherwise would have on average, while providing greater salary potential for those at lower pay levels. Suppose, however, that the algorithm used to determine annual pay adjustments overestimated the rate of pay growth before the demonstration. Then the average wage rate under PACER SHARE might rise more rapidly than before, possibly causing cost increases rather than cost savings.

Pressure from Above Not to Reduce Staff

SM-ALC is part of a larger organization, the Air Force Logistics Command (AFLC). If faced with decrease of workload, to protect its own budget or prevent layoffs AFLC could encourage the ALCs to spend all of their current budgets. This might require the performance of discretionary tasks (inventory, rebinning, maintenance, for instance) more frequently or extensively than otherwise. Such tasks are legitimate. However, if the objective is to exhaust the budget rather than accomplish the required workload at least cost, positions vacated by turnover would be filled and there would be little incentive to use the added flexibility in allocating labor provided by the interventions. The budget can be spent faster by less efficient use of labor. In this case there would be little chance for improving productivity or gainsharing, and the workforce could become disillusioned with the prospects held out by the demonstration for improving the organization and the quality of worklife, reducing their identification with DS goals. Further, to outside observers it could appear as if the situation at Sacramento were worsening under the demonstration. Within the framework of the evaluation model, however, Sacramento's relative outcomes would be compared with those of the other ALCs. This would show whether the possible deterioration at Sacramento was any greater than at the comparison sites.

PACER SHARE VS OTHER OPM DEMONSTRATION PROJECTS

PACER SHARE is one of several demonstration projects being conducted under OPM authority to test different initiatives to improve productivity and employee performance by making the federal personnel system more flexible and responsive. Three of those demonstrations began before PACER SHARE:

 Integrated Approach to Pay, Performance Appraisal, and Position Classification for More Effective Operation of Government Organizations (Department of the Navy)

- Alternative Personnel Management System (National Institute of Standards and Technology)
- Airway Science Curriculum (Federal Aviation Administration)

The first of these demonstrations is being conducted at the Naval Ocean Systems Center in San Diego and the Naval Weapons Center at China Lake. Its purpose is to demonstrate whether federal laboratory effectiveness can be enhanced by allowing management greater control over personnel functions and expanding the opportunities available to employees. Like PACER SHARE, this project examines the benefits of a simplified classification system and pay banding. However, it does not emphasize organizational productivity, it retains performance ratings, and it provides merit pay to reward individual performance rather than gainsharing to reward collective performance. Also, its participants are largely white-collar.

The demonstration by the National Institute of Standards and Technology has much in common with the Navy project. Its goals are to simplify the classification process, make it more understandable, and place more decisionmaking authority with line managers. It establishes pay banding and links salaries to individual performance. It differs from the Navy demonstration by testing such innovations as sabbaticals and compensation comparability with the private sector. Participants are primarily scientists and engineers.

The FAA demonstration is intended to develop alternative qualifications and recruitment sources primarily for agency technical occupations. It thus has little in common with PACER SHARE.

Since PACER SHARE began, OPM has approved two more demonstration projects. One is another FAA demonstration, this one testing retention allowances covering difficult-to-staff positions at air traffic control facilties in the Chicago, Los Angeles, New York, and Oakland areas. The other is a test of skill-based pay by the Defense Logistics Agency at its Ogden, Utah, depot. A third personnel management demonstration was legislated by Congress. It provides lump-sum relocation bonuses and retention allowances to alleviate severe recruitment and retention problems at the FBI in New York City.

Appendix B

BASELINE SURVEY QUESTIONNAIRE

This appendix presents the questionnaire used in the baseline survey of the workforces at the Air Logistics Centers.

SURVEY OF ATTITUDES IN THE DIRECTORATE OF DISTRIBUTION

This survey was designed to enable you to provide information on how you feel about your work at the Directorate of Distribution (DS). The results of the survey are completely confidential and anonymous. The completed questionnaires will be taken to The RAND Corporation in Santa Monica, California for analysis. No individual respondents will be identified. No completed questionnaires will be given to DS--only statistical summaries will be provided. We have taken these steps to enable you to answer the questionnaire as openly and honestly as you can. Please feel free to do so. Farticipation is voluntary. We appreciate your cooperation.

SECTION 1: CURRENT ATTITUDES

Each statement in this section concerns your feelings about your work at the Directorate of Distribution (DS). Please indicate the extent to which you agree or disagree with each statement. Mark an "X" in the numbered box below the response that best indicates how you feel. Remember, we are interested in YOUR feelings about YOUR work situation. There are no right or wrong answers to these questions.

1. I usually know whether or not my work is satisfactory.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

Regular pay increases here depend on how well a person performs his/her job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

3. The union and management are hostile toward each other.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

4. My unit works well together.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

5. If we have a decision to make, everyone is involved in making it.

Strongly				Strongly	
Disagree	Disagree	Undecided	Agree	Agree	
[1]	[2]	[3]	[4]	[5]	

6. Under the present system it is very difficult to motivate employees with financial rewards.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

7. ¥	When changes	are made	in DS.	the	emplovees	usually	lose	out	in	the er	nd.
------	--------------	----------	--------	-----	-----------	---------	------	-----	----	--------	-----

Strongly	Strongly			
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

8. Considering my skills and the effort I put into my work I am satisfied with my pay.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

9. High performers tend to stay with DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

10. What happens to DS is really important to me.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

11. I have confidence and trust in my co-workers.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

12. It is clear how pay decisions are made around here.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

13. Employees here feel you can't trust management in this directorate.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

14. My job duties are clearly defined by my supervisor.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

15.	My supervisor	encourages	subordinates	to	participate	in	important	
	decisions.							

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

16. To help DS, it is necessary that I think of ways to help other sections, branches, or divisions do their jobs.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

17. I have control over how I spend my time working.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

18. My co-workers encourage each other to give their best effort.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

19. My supervisor handles the administrative parts of his/her job well.

Strongly				Strongly	
Disagree	Disagree	Undecided	Agree	Agree	
[1]	[2]	[3]	[4]	[5]	

20. I am satisfied with my opportunities for advancement.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

21. My supervisor gives me adequate information on how well I am performing.

Strongly				Strongly	
Disagree	Disagree	Undecided	Agree	Agree	
[1]	[2]	[3]	[4]	[5]	

22.	Other employers in	this area	pay more	than the	government	does for
	the kind of work I	am doing.				

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

23. My supervisor has strong technical skills.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

24. Promotions here depend on how well a person performs his/her job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

25. Coming up with new ways to do my job leads to good job performance.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

26. If I had the chance I would take a different job within DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

27. I will be promoted or given a better job if I perform especially well.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

28. My supervisor demands that people give their best effort.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

29. My pay is determined by my individual job performance.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
(11	(2)	131	[4]	[5]

30.	I could find a	job with another	employer with	about the	same pay
	and benefits a	s I now have.			

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

31. My supervisor works well with people.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

32. All in all, I am satisfied with the position classification procedures in DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
(1)	[2]	[3]	[4]	[5]

33. My job allows me to achieve personal satisfaction.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

34. My supervisor is interested in my opinion on how to improve things in DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

35. DS gives me adequate training to do my job well.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
กา้	(21	[3]	[4]	[5]

36. If DS saves money because we (i.e., the employees) work harder or better, some of the savings will be shared with us.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

37. I will be demoted or removed from my position if I perform my job poorly.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

38. In DS, conflict that exists between work units gets in the way of getting the job done.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

39. My supervisor keeps informed about the way subordinates think and feel about things.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

40. Management in DS is concerned about me as a person.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

41. If one of my co-workers isn't working hard enough, I would tell him/her so.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

42. It is necessary for DS to minimize costs and maximize performance.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

43. Working hard on my job leads to good job performance.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

44. It is necessary for everyone in DS to help support other directorates such as Maintenance.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

45. In general, I like the way the union handles things.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

46. Coordination among work units is good in DS.

Strongly				Strongly Agree
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

47. It would be very hard for me to leave my job even if I wanted to.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

48. Pay differences in DS fairly represent real differences in levels of responsibility and job difficulty.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

49. I deserve most of the credit or blame for how well my work gets done.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

50. My supervisor sets clear goals for me in my present job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

51. I will be given simpler work or less work if I perform my job poorly.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
111	(2)	[3]	[4]	[5]

52.	People	in	DS	will	do	things	behind	your	back.
-----	--------	----	----	------	----	--------	--------	------	-------

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

53. To help DS it is necessary that I think of ways to help my section do its job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

54. In general, I like working here.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

55. I have a great deal of say over what has to be done on my job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

56. If I have ideas on how other people in DS could improve their work I should tell their supervisors.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	(21	[3]	[4]	151

57. My co-workers are afraid to express their real views.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

58. In general, I am satisfied with my job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

59. In DS, employees receive equal pay for equal work	59.	In DS.	employees	receive	equal	pav	for	equal	work
---	-----	--------	-----------	---------	-------	-----	-----	-------	------

Strongly				Strongly
Di sagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

60. The amount of money I will receive for working harder is enough to make me work harder.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

61. Working hard on my job leads to gaining respect from my co-workers.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

62. I am personally responsible for helping DS improve its performance.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

63. Low performers tend to leave DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

64. In DS, you make more money in blue-collar jobs than in white-collar jobs.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

65. New employees in DS are well qualified for their jobs.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

66. In general, disciplinary actions taken in DS are fair and justified.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

67. Employees here take full advantage of their grievance and appeal rights.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

68. In my work unit we tell each other the way we are feeling.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

69. I have all the skills I need in order to do my job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

70. My pay is fair considering what other places in this area pay for the same kind of work.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

71. In DS, authority is clearly delegated.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

72. For DS to do its mission well it is necessary for me personally to do a good job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

73. If I have ideas on how people in DS could improve their work I should tell them.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

74.	My supervisor	encourages	me	to	help	in	developing	work	methods	and
	job procedure	s .								

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

75. My supervisor helps me solve work related problems.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

76. If I were subject to an involuntary personnel action, I believe I would be told about my grievance and appeal rights.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

77. I have the authority I need to accomplish my work objectives.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

78. Quality control programs help me do my job better.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

79. I will receive more money if I work harder for DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

80. It is necessary for DS to maintain high work quality and timeliness.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

81. All in all, I am satisfied with my pay.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

82.	I will get a l	arger pay inc	crease if I per	form espec	cially well.
	Strongly				Strongly
		Diezeroe	Undecided	Agree	Agree
	Disagree	Disagree		-	(5)
	[1]	[2]	[3]	[4]	(5)
83.	I have too muc	h at stake in	n my job to cha	inge jobs r	now.
	Strongly				Strongly
	Disagree	Disagree	Undecided	Agree	Agree
	-	_		_	[5]
	[1]	[2]	[3]	[4]	(5)
84.	Under the pres		inancial reward	is are seld	dom related
	Strongly				Strongly
	Disagree	Disagree	Undecided	Agree	Agree
	[1]	[2]	[3]	[4]	[5]
	(-;	(-)	(0)		(0)
85.	I often think	about quittir	ng.		
	Strongly				Strongly
	Disagree	Disagree	Undecided	Agree	Agree
	[1]	[2]	[3]	[4]	[5]
86.	My job is chal	lenging.			
	Strongly				Strongly
	Disagree	Disagree	Undecided	Agree	Agree
	[1]	[2]	[3]	[4]	[5]
87.	My pay is fair paid.	considering	what people in	n other di	rectorates are
	Strongly				Strongly
	Disagree	Disagree	Undecided	Agree	Agree
	[1]	[2]	[3]	[4]	[5]
88.	Management is	flexible enou	igh to make cha	inges when	necessary.
	Strongly				Strongly
	Disagree	Disagree	Undecided	Agree	Agree
	[1]	[2]	[3]	[4]	[5]
89.	On my job I kr	now exactly wh	nat is expected	i of me.	
	Ch manal				Ch man = 1
	Strongly	D .	فيداد المساهمة	1	Strongly
	Disagree	Disagree	Undecided	Agree	Agree
	[1]	[2]	(3)	[4]	[5]

90.	The	work	I	do	on	mv	dor	is	meaningful	to	me.
-----	-----	------	---	----	----	----	-----	----	------------	----	-----

Strongly		Strongly		
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

91. I am satisfied with the chances I have to learn new things on my job.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

92. I am given the opportunities I want to participate in training programs.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

93. Management and the union are willing to try solutions which haven't been tried before.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

94. In my work unit everyone's opinion gets listened to.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

95. I can save money for DS by working harder or better.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

96. My supervisor is concerned about me as a person.

Strongly				Strongly
Disagree	Disagree	Undecided	Agre e	Agree
[1]	[2]	[3]	[4]	[5]

97. I have idea, about how I could do a better job for DS.

Strongly	Strongly			
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

98. Ma	nagement i	s onl	y willing	to	negotiate	about	a	few	specific	issues.
--------	------------	-------	-----------	----	-----------	-------	---	-----	----------	---------

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

99. I will have better job security if I perform especially well.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

100. All in all, I am satisfied with my work unit.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

101. Employees do not have much opportunity to influence what goes on in DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

102. Competition for jobs here is fair and open.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

103. I am satisfied with the amount of job security I have.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

104. I would prefer not to receive an annual performance appraisal from my supervisor.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

105. During the next year I will probably look for a new job outside DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

106. My own hard work will lead to recognition as a good performer.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

How satisfied are you with the efforts your union has made to get each

	e following outcomes for its	_	s?
107.	More meaningful work for	[1]	Very dissatisfied
10	members?	[2]	-
		[3]	
		[4]	
			Very satisfied
			man and an analysis and and
108.	Fairer job classifications?	[1]	
		[2]	
		[3]	
		[4]	
		[5]	Very satisfied
109.	Fairer promotion policies?	[1]	Very dissatisfied
		[2]	-
		[3]	Neither satisfied nor dissatisfied
		[4]	
		[5]	
	18	/11	Very dissatisfied
110.	How satisfied are you with	[1]	-
	the success your union has	[2]	
	in bargaining non-wage	[3]	
	issues?	[4] [5]	
		(5)	very sacisfied
If I	took a new job, I would do so	to	[1] More responsibility
gain:	: (Mark the THREE most import	ant.)	[2] Better pay
			[3] More job security
111.			[4] Better supervisors
112.			[5] More interesting work
113.			[6] More important program
			[7] Better working conditions
			[8] More convenient office hours
			[9] Better promotion opportunities
			[10] More congenial colleagues

[10] More congenial colleagues [11] Better geographical location

[12] Better benefits

Please indicate how important each of the following is in determining your pay:

114. The quality of your job performance? [1] Not important at all [2] Somewhat important [3] Important [4] Very important [5] Extremely important 115. The quality of your work unit's [1] Not important at all performance? [2] Somewhat important [3] Important [4] Very important [5] Extremely important 116. The amount of responsibility on your [1] Not important at all job? [2] Somewhat important [3] Important [4] Very important [5] Extremely important 117. Your length of service? [1] Not important at all [2] Somewhat important [3] Important [4] Very important [5] Extremely important 118. Would you be willing to serve as a [1] Yes member of a union-management [2] No committee? [1] No effort 119. Please rate the amount of effort you put into work activities [2] A little effort during an average workday. [3] Some effort [4] A lot of effort [5] Extreme effort How important is each of the following to you: 120. Challenging work responsibilities? [1] Not important at all Somewhat important [2] [3] Important [4] Very important [5] Extremely important 121. The chance to accomplish something [1] Not important at all worthwhile? [2] Somewhat important [3] Important [4] Very important

[5] Extremely important

122.	The chance to learn new things on on your job?	[1] [2] [3] [4] [5]	Not important at all Somewhat important Important Very important Extremely important
123.	Getting a feeling of accomplishment from your job?	[1] [2] [3] [4] [5]	Not important at all Somewhat important Important Very important Extremely important
124.	Retirement benefits?	[1] [2] [3] [4] [5]	Not important at all Somewhat important Important Very important Extremely important
125.	Your chances for getting a promotion?	[1] [2] [3] [4] [5]	Not important at all Somewhat important Important Very important Extremely important
126.	The amount of job security you have?	[1] [2] [3] [4] [5]	Not important at all Somewhat important Important Very important Extremely important
127.	Your chances for obtaining a permanent "career" position?	[1] [2] [3] [4] [5]	Not important at all Somewhat important Important Very important Extremely important

IF YOU ARE A SUPERVISOR, PLEASE CONTINUE WITH QUESTION 128 ON PAGE 20.

IF YOU ARE NOT A SUPERVISOR, PLEASE GO TO QUESTION 151 ON PAGE 24.

SECTION 2: SUPERVISORS' ATTITUDES

128. It takes too long to get decisions made in DS.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

129. My pay is based partly on the performance of the workers I supervise.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

130. The work I am responsible for supervising probably could be done with fewer employees.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

131. There is enough staffing flexibility to meet changing work loads.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

132. I have enough authority to hire competent people when I need them.

Strongly	Strongly			
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

133. Top management generally supports the personnel decisions made by supervisors in DS.

Strongly				Strongly
Disagree	Disagree	Under ded	Agree	Agree
[1]	[2]	1-1	[4]	[5]

134. In DS jobs are classified fairly and accurately.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

135. Without performance appraisal it would be more difficult to reward or discipline employees.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

136. The criteria used to grade supervisory positions in DS are fair.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

137. The personnel office helps me perform my job effectively.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

138. My pay level is based partly on the number and grades of the people I supervise.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

139. It takes too long to process the paperwork needed to fill vacancies here.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

140. Supervisors here cooperate with each other for the attainment of DS's goals.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	(3)	[4]	[5]

141. I have enough authority to determine my employees' pay.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

142. In DS, my organization recognizes supervisors who take the time to develop their subordinates' knowledge, skills, and abilities.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

143. The personnel department here provides line management with valuable support services.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

144. The work I am responsible for supervising probably could be done with fewer mid-level supervisors.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

145. I have to devote too much time to position classification.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

146. I have enough authority to promote people.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

147. The current system enables me to help the people I supervise improve their performance.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

148. I have enough authority to influence classification decisions.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

149. Supervisors in DS feel their ability to manage is restricted by unnecessary personnel rules and regulations.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

150. I have enough authority to remove people from their jobs if they perform poorly.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

PLEASE GO TO QUESTION 151 ON PAGE 24.

SECTION 3: BACKGROUND

THE INFORMATION COLLECTED IN THIS SECTION WILL ONLY BE USED TO HELP SUMMARIZE THE SURVEY DATA. INDIVIDUALS WILL NOT BE IDENTIFIED.

151. What is your office symbol (e.g., DSTEW)?

(office symbol)

- 152. How long have you worked in DS?

 [1] Less than 1 year
 [2] 1 3 years
 [3] 3 5 years
 [4] Over 5 years
- 153. Have you ever been a regular member [1] Yes of a quality circle at DS? [2] No

IF YOU HAVE BEEN A MEMBER OF A QUALITY CIRCLE PLEASE ANSWER QUESTION 154.

IF YOU HAVE NEVER BEEN IN A QUALITY CIRCLE PLEASE GO TO QUESTION 156.

154. Are you in quality circle now? [1] Yes [2] No

IF YOU ARE IN A QUALITY CIRCLE NOW PLEASE ANSWER QUESTION 155.

IF YOU ARE NOT IN A QUALITY CIRCLE PLEASE GO TO QUESTION 156.

155. How long have you been in this quality circle?

[2] 3 - 6 months
[3] 6 months to 1 year
[4] 1 - 2 years
[5] 2 - 5 years
[6] Over 5 years

156. What is your pay category?

[1] GS [4] WL
[2] GM [5] WS

[3] WG

[6] SES

157	What is your pay grade?	(11	•	,,,	6	(111	
137.	what is your pay grade:	[1]		[6]		[11] 11	
		[2]		[7]		[12] 12	
		[3]		[8]		[13] 13	
		[4]		[9]		[14] 14	
		[5]	5	[10]	10	[15] 15	
158.	How long have you been in you	ır		(11	Less	than 1 year	
	present grade or pay level?				1 - 2		
				[3]		years	
				[4]		5 years	
					•••	70015	
159.	What type of appointment are		[1]	Tempora	ry/ten	m appointmen	it
	you serving under?		[2]	Probati	onary	career condi	tional
	-			Career			
			[4]	Career			
				Other			
160.	How long have you worked for	your		[1]	0 - 3	months	
	present immediate supervisor:			[2]		months	
	•			[3]		ths to 1 yea	r
				[4]		years	_
				[5]		years	
				[6]		5 years	
				(0)	OVEL	J Years	
161.	How many years have you been	a Fe	deral	[1]	Less 1	than 1 year	
	Government employee? (Exclud			[2]	1 - 3	years	
	military service.)			[3]		years	
	-			[4]		14 years	
				(5)		29 years	
				[6]		ars or more	
162.	How many years of full-time e	emplo	yment	[1]	Non e		
	have you had in the private s	secto	r?	[2]	Less 1	than 1 year	
	-			[3]	1 - 2	years	
				[4]		years	
				[5]		5 years	
163.	How many times have you moved	i bet	ween	[1]	Never		
	Federal agencies in the last		•	[2]	Once		
	years? (Count different majo	r Do	D	[3]	Twice		
	components as different agend			[4]	Three	or more tim	es

	and						
	(job series no.)	(job title	e)			
165.	Are you currently a member of a loc representing DS employees?	al	union		.] Y		
	U ARE A SUPERVISOR (ANY LEVEL), PLEA U ARE NOT A SUPERVISOR, PLEASE GO TO		_		ns 1	66 2	AND 167
166.	How long have you been officially designated a supervisor (any level)		[2] [3]	Less 1 - 2 2 - 5 Over	yea yea	rs rs	/ear
167.	How many employees do you supervise directly (not at second level)?	•	[2] [3] [4]	3 - 5 6 - 9 10 - 21 -	20 30	30	
168.	birthday?	2]	Under 30 30 - 39 40 - 49		[5]	55	- 54 - 59 and ov
169.	Are you male or female?		[1] [2]	Male Femal	•		
170.	Are you Black, White, or Other (e.g American Indian, Eskimo, Aleut, Asi or Pacific Islander)?			Black White Other			

- 172. What is your education level? (Indicate highest grade completed.)
 - [1] Elementary school (grades 1-8)
 - [2] Some high school or some technical training
 - [3] GED (General Educational Development)
 - [4] Graduated from high school and received regular high school diploma
 - [5] High school degree plus technical training or apprenticeship
 - [6] Some college
 - [7] Two-year associate college degree
 - [8] Four-year college degree (B.A., B.S., or other bachelor's degree)
 - [9] Some graduate school
 - [10] Master's degree
 - [11] Doctorate degree (Ph.D., M.D., J.D., etc.)

IF YOU WORK AT MC CLELLAN AFB, PLEASE ANSWER THE FOUR QUESTIONS BELOW.

173. I have been adequately informed about the PACER SHARE demonstration project.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

174. I understand how PACER SHARE will affect me and my work.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

175. I am in favor of the PACER SHARE demonstration project.

Strongly				Strongly
Disagree	Disagree	Undecided	Agree	Agree
[1]	[2]	[3]	[4]	[5]

176. Are there any other issues about PACER SHARE that should be addressed in future surveys?

Appendix C

SUPPLEMENTAL SURVEY RESULTS

This appendix presents supplementary information pertaining to the baseline attitude survey. Table C.1 shows the mean response among nonsupervisors for each question in the questionnaire, by ALC. The ALCs are indicated by the "SITENAME" variable: OC is Oklahoma City, Oklahoma: OO is Ogden, Utah; SA is San Antonio, Texas; SM is Sacramento, California; and WR is Warner-Robins, Georgia. Table C.2 shows the comparable results for supervisors. In Table C.3, the nonsupervisor means for the response scales discussed in Sec. II of the report are presented. Table C.4 presents the analogous results for supervisory personnel.

The ordinary least squares (OLS) regression results are shown in Tables C.5 to C.7. Table C.5 presents results for questions 1-127, which all respondents answered. Table C.6 presents results for the response scales based on these questions. Finally, Table C.7 presents results for questions 128-150, which supervisors above answered, and for the response scales based on these questions. As discussed in Sec. II, the purpose of the regression analyses is to determine the extent to which the mean workforce response at SM-ALC differed from that of the comparison ALCs, controlling for differences in the demographic composition and experience base of their samples and workforces. The following discussion describes the background factors included in the analyses and their purposes.

The "SUPER" variable is coded "1" for supervisors and "0" for nonsupervisors. The coefficient thus indicates the difference in mean response for supervisors relative to nonsupervisors. For example, as can be seen on the first page of Table C.5, the mean response for supervisors across all the ALCs was .15 higher (on the five-point scale) for question 1. The "SACTO" variable is coded "1" for SM-ALC respondents and "0" for all others. It is the key variable, indicating the difference in the mean response for SM-ALC relative to the comparison group. "V152" indicates tenure in DS and is coded as indicated in the questionnaire. A higher value reflects longer time in DS. "V156W" is coded "1" for white-collar job holders and "0" for blue-collar job holders. "V157C" indicates pay levels 1-4 as defined in PACER

SHARE and discussed earlier. Higher values reflect higher pay levels.

"V158" indicates length of time in current pay grade and is coded as indicated in the questionnaire. Higher values reflect longer times.

"V159A" is coded "1" for career category "career" employees and "0" for all others. "V160" indicates length of time worked for current supervisor and is coded as indicated in the questionnaire. Higher values reflect longer times. "V165" is coded "1" for union members and "2" for nonmembers. "V168" reflects the respondent's age and is coded as indicated in the questionnaire. Higher values indicate older respondents. "V169" is coded "1" for males and "2" for females. "V172" reflects education level and is coded as indicated in the questionnaire. Higher values reflect higher education levels. The remaining variables are dummy variables reflecting race and ethnicity. "WHS" is white Hispanic; "BNHS" is black; "OTH" represents all other persons not classified as white non-Hispanic.

Table C.8 presents regression results concerning pretest versus baseline survey attitude differences at SM-ALC. The "ADMIN" variable is coded "1" for the baseline survey respondents and "0" for pretest respondents. The coefficient thus indicates the change in mean response between the two administrations, controlling for possible differences in the composition of the two samples on the other included factors.

Table C.9 highlights the results of the exploratory factor analyses discussed in Sec. II. The factors were generated using the principal factor method and varimax (orthogonal) rotation. Communalities were set equal to the largest absolute correlation in the given column of the correlation matrix. The question numbers shown reflect the questions with absolute loadings of .40 or greater on the rotated factors. The Cronbach Alpha Coefficients for these questions are indicated in the leftmost column.

Finally, Table C.10 presents the percentage distribution of responses across the rating scale categories for questions in the baseline survey.

Table C.1

MEANS FOR ALL VARIABLES, NONSUPERVISORS

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Table C.1--continued

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Table C.1--continued

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Table C.1--continued

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23 8 4.16284987 0.86149043 1.0000000 23 393 8 4.08995852 0.86290171 1.0000000 24 394 7 4.22335025 0.9055818 1.0000000 25 394 7 4.22335025 0.9055818 1.0000000 25 393 8 4.19837059 1.01705841 1.0000000 27 396 1.5 3.01295337 1.0551764 1.0000000 27 387 1.1 1.77002584 0.45356477 1.0000000 28 3.77 2.4 1.77002584 0.45356477 1.00000000 25 377 2.4 1.87267905 0.9551764 1.00000000 2.2 26 377 2.4 1.87267905 0.9551764 1.00000000 2.2 27 3.6 2.6000000 1.44337547 1.00000000 2.2 28 3.6 2.14559585 1.11583352 1.00000000 2.2 29 3.6 3.1	40	700) (896982	.0000000	
22 393 8 4.08905852 0.86290171 1.00000000 24 394 7 4.26649746 0.80237841 1.00000000 25 394 7 4.25786502 0.85387995 1.00000000 27 392 9 4.18320611 0.95405841 1.00000000 27 4.35786502 0.85387995 1.00000000 5. 28 387 1.4 1.71590909 0.45356477 1.00000000 2. 54 88 313 1.71590909 0.45356477 1.00000000 2. 55 37 2.60000000 1.4535647 1.00000000 3. 55 37 2.40000000 1.2433764 1.00000000 3. 56 384 1.7 2.44559585 1.11583352 1.00000000 3. 59 386 1.8 3.1387364 1.00000000 3. 50 387 1.4 3.12659380 1.00000000 3. 51 387 1.4 1.751940 1.12659095 1.00000000 3. 52	• 0	7 6) (841490	.0000000	
23 394 7 4.26649746 0.80237841 1.00000000 24 394 7 4.2235025 0.90565818 1.00000000 25 394 7 4.2235025 0.90565818 1.00000000 26 393 8 4.1832011 0.9540841 1.00000000 52 386 1.6 1.01295337 1.01709127 1.00000000 53 387 1.7700284 0.9540584 1.00000000 2.0000000 54 387 1.7500284 0.0000000 2.0000000 2.0000000 2.0000000 55 377 2.6 1.60000000 1.24335677 1.00000000 2.0000000 1.2237867 1.00000000 1.2237867 1.00000000 1.2237887 1.00000000 1.2237887 1.00000000 1.22365011 1.00000000 2.0000000	• •	000) (862901	.0000000	
24 7 4.22335025 0.96565818 1.0000000 25 394 7 4.35786802 0.96565818 1.0000000 27 392 9 4.19832051 1.0000000 5.1000000 53 386 14 1989395 1.0000000 6.1000000 53 387 1 1.77002584 0.42136067 1.0000000 6.2000000 54 28 377 24 1.77002584 0.42136067 1.00000000 6.2000000 55 377 24 1.77002584 0.42136067 1.00000000 6.2000000 55 377 24 1.7500260 0.99163984 1.00000000 1.20000000 57 384 15 2.6000000 1.44337567 1.00000000 1.20000000 59 386 14 3.77559885 1.11965095 1.00000000 1.20000000 61 387 14 3.77559885 1.11965095 1.00000000 2.2000000 62 387 1.84514436 1.03622424 1.00000000 2.20000000 69 387<	• •	765			802378	.0000000	
25 394 7 4.35786802 0.85387995 1.00000000 5 27 393 8 4.1832641 0.95405841 1.00000000 5 27 392 15 4.19897959 1.015551764 1.00000000 6 53 387 14 1.77002584 0.42136067 1.00000000 2 54 387 1.77002584 0.42136067 1.00000000 2 55 377 2.60000000 0.4535477 1.00000000 2 56 377 2.60000000 0.9918944 1.00000000 6 57 384 17 6.5610417 1.00000000 1.2 57 386 15 2.44559585 1.11583352 1.00000000 1.2 59 387 14 3.7519380 0.54687492 1.00000000 6 51 387 14 3.91214470 1.2436501 1.00000000 2 52 387 2.50000000 1.2436501 1.000	•	394			905658	.0000000	
26 393 8 4.18320611 0.95405841 1.00000000 5 27 392 9 4.19897959 1.01709127 1.00000000 5 53 386 14 1.71590909 0.4213607 1.00000000 2 54 88 376 2.6000000 0.45356477 1.00000000 2 55 377 24 1.87267905 0.99183984 1.00000000 3 56 377 24 1.87267905 0.99183984 1.00000000 3 57 384 17 2.6000000 1.44337567 1.00000000 4 58 377 2.6500000 1.44337567 1.00000000 3 59 384 1.5 2.4455948 1.00000000 4 50 386 1.4455958 1.11583352 1.00000000 4 50 387 1.4 1.7588658 1.13297887 1.00000000 5 51 387 2.0 2.0000000	•	394	•		.853879	.0000000	
27 392 9 4.19897959 1.01709127 1.00000000 4.19897959 53 386 15 3.01295337 1.05551764 1.00000000 2.10000000 54 88 313 1.71502584 0.45356477 1.00000000 2.10000000 55 37 24 1.87267905 0.99163984 1.00000000 3.10000000 57 384 17 2.44559585 1.00000000 3.10000000 3.10000000 59 386 15 2.44559585 1.11583352 1.00000000 4.11583352 1.00000000 4.11583352 1.00000000 4.11583352 1.000000000 4.11583352 1.000000000 4.11583352 1.000000000 4.11583352 1.000000000 4.115858352 1.000000000 4.115858352 1.000000000 4.115858352 1.000000000 4.115858352 1.000000000 2.115858653 1.000000000 2.115858653 1.000000000 2.11586653 1.00000000 2.11586653 1.00000000 2.11586653 1.000000000 2.11586653 1.00000000 3.11586	10	393	•		.954058	.0000000	
52 366 15 3.01295337 1.05551764 1.00000000 2.387 54 88 313 1.71590909 0.45356477 1.00000000 2.556477 55 37 2.60000000 1.44337567 1.00000000 3.7519180 56 37 2.4 1.87267905 0.99183984 1.00000000 3.7519380 57 38 15 2.44559585 1.11583352 1.00000000 9.7519380 59 387 14 3.77519380 0.54687492 1.00000000 9.7519380 60 387 14 3.91214470 1.1365995 1.00000000 9.751940 61 387 14 3.91214470 1.24365011 1.00000000 9.751940 62 381 2.0527494 1.1365995 1.00000000 2.751960 9.31262919 1.00000000 2.751960 69 379 2.2 2.05277045 0.31262919 1.00000000 3.75162919 1.1 71 357 2.05277045	2	392	Ø.		.017091	.0000000	
53 367 14 1.77002584 0.45136067 1.00000000 2.4 54 25 376 2.60000000 1.44337567 1.00000000 3.4 55 377 24 1.8750909 0.45356477 1.00000000 3.4 56 377 24 1.670000000 1.2 1.00000000 1.2 57 384 1.7 6.56510417 2.24386160 1.00000000 1.2 59 386 1.5 2.44559585 1.11583352 1.00000000 1.2 59 386 1.5 3.77519380 0.54687492 1.00000000 6.4 60 387 1.4 3.77519380 0.54687492 1.00000000 6.5 61 387 1.4 3.91214470 1.24357887 1.00000000 6.5 62 381 2.0 2.0000000 1.26374701 1.00000000 2.2 69 381 2.2 2.05277045 0.31262919 1.00000000 3.7	110	386			.055517	.0000000	
54 88 313 1.71590909 0.45356477 1.00000000 2. 55 377 24 1.60000000 1.44337567 1.00000000 6. 56 384 17 6.56510417 2.24386160 1.00000000 12. 57 384 15 2.44559585 1.11583352 1.00000000 12. 59 387 14 3.75519380 0.54687492 1.00000000 4. 60 386 15 3.18652850 1.43597887 1.00000000 6. 61 387 14 3.75519380 0.54687492 1.00000000 6. 61 387 14 3.75519480 1.11965095 1.00000000 6. 62 387 14 1.79586563 1.03922224 1.00000000 2. 63 381 2. 2.5000000 1.20524271 1.00000000 2. 69 379 2. 2.5000000 0.50524277 1.00000000 3. <td< td=""><td>•</td><td>387</td><td>14</td><td></td><td>.421360</td><td>.0000000</td><td></td></td<>	•	387	14		.421360	.0000000	
55 25 376 2.60000000 1.44337567 1.00000000 3.77 56 384 1.87267905 0.99183984 1.00000000 3.10000000 3.244559585 1.11583352 1.00000000 1.24559585 1.11583352 1.00000000 1.24687492 1.00000000 1.24687492 1.00000000 1.24687492 1.00000000 1.24687492 1.00000000 1.00000000 1.00000000 1.00000000 2.21887 1.00000000 1.00000000 2.21887 1.00000000 2.21887 1.00000000 2.21888 1.00000000 2.21888 1.00000000 2.21888 1.00000000 3.2288 <	-	80	~		.453564	.0000000	
56 377 24 1.87267905 0.99183984 1.00000000 3. 57 384 17 6.56510417 2.24386160 1.00000000 12. 58 386 15 2.44559585 1.11583352 1.00000000 4. 59 387 14 3.77519380 0.54687492 1.0000000 4. 60 386 15 3.18652850 1.43297887 1.00000000 6. 61 387 14 3.91214470 1.24365011 1.00000000 5. 63 387 14 1.79586563 1.03922224 1.00000000 2. 64 1.79586563 1.03922224 1.00000000 2. 2. 65 381 20 2.59000000 1.00000000 2. 71 357 2.2 2.05277045 0.31262919 1.00000000 3. 71 351 2.05277045 0.29395552 1.00000000 1. 72 2.2 2.2 2.2 </td <td>5</td> <td>25</td> <td>~</td> <td></td> <td>.443375</td> <td>.0000000</td> <td></td>	5	25	~		.443375	.0000000	
57 384 17 6.56510417 2.24386160 1.00000000 13. 59 386 15 2.44559585 1.11583352 1.00000000 4.0000000 59 387 14 3.1865850 1.43297887 1.00000000 6. 60 387 14 3.91214470 1.24365011 1.00000000 6. 63 387 14 1.79586563 1.0392224 1.00000000 2. 69 381 20 1.84514436 0.36224271 1.00000000 2. 69 379 22 2.50000000 1.205244701 1.00000000 2. 71 357 22 2.05277045 0.31262919 1.00000000 3. 71 357 44 1.90476190 0.29395552 1.00000000 1.1. 72 5.42257218 1.55509847 1.11	5	377	24		.991639	.0000000	m) (
58 386 15 2.44559585 1.11583352 1.00000000 4.519380 0.54687492 1.00000000 9.54687492 1.00000000 9.54687492 1.00000000 9.54687492 1.00000000 9.54687492 1.00000000 9.54687492 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.546887 1.00000000 9.54687 1.00000000 9.54687 1.00000000 9.54688 1.1 1.00000000 9.54688 1.1 1.00000000 1.1<	5	384	11		.243861	.0000000	'n
59 387 14 3.77519380 0.54687492 1.0000000 9 60 386 15 3.18652850 1.43297887 1.00000000 6 61 387 14 3.63307494 1.11965095 1.00000000 6 62 387 14 1.79586563 1.034365011 1.00000000 5 65 381 20 1.84514436 0.3622421 1.00000000 2 68 379 21 2.50000000 1.20574701 1.00000000 2 70 379 22 1.51978892 0.50026867 1.00000000 2 71 357 44 1.90476190 0.29395552 1.0000000 1 72 5.42257218 1.55509847 1.00000000 2 1		386			.115833	.0000000	-
386 15 3.18652850 1.43297887 1.00000000 6. 61 387 14 3.51307494 1.11965095 1.00000000 6. 62 387 14 1.79586563 1.03922224 1.00000000 9. 65 381 20 1.8454436 0.36224271 1.00000000 2. 68 380 21 2.50000000 1.20574701 1.00000000 2. 70 379 22 2.55277045 0.31262919 1.00000000 2. 71 357 44 1.90476190 0.29395552 1.00000000 1. 72 2.05277045 0.29395552 1.00000000 2. 71 381 20 5.42257218 1.55509847 1.00000000 1.	5	387			. 546874	.0000000	-
61 387 14 3.63307494 1.11965095 1.00000000 6. 62 387 14 3.91214470 1.24365011 1.00000000 5. 63 387 14 1.79586563 1.03922224 1.00000000 9. 65 381 20 1.84514436 0.2052771 1.00000000 2. 68 379 21 2.50000000 1.20574701 1.00000000 2. 70 379 22 2.05277045 0.31262919 1.00000000 3. 71 357 44 1.90476190 0.29395552 1.0000000 11. 72 2.05277045 0.29395552 1.0000000 2. 72 381 20 5.42257218 1.55509847 1.0000000 11.	•	386			.432978	.0000000	
62 387 14 3.91214470 1.24365011 1.00000000 5.91214436 63 387 1.04514436 0.36224271 1.00000000 2.00000000 68 380 22 2.50000000 1.20574071 1.00000000 70 379 22 2.05277045 0.31262919 1.00000000 71 357 44 1.90476190 0.29395552 1.0000000 72 381 20 5.42257218 1.55509847 1.0000000	•	387			.119650	0000000	
63 387 14 1.79586563 1.03922224 1.00000000 9. 65 381 20 1.84514436 0.36224271 1.00000000 2. 68 380 21 2.50000000 1.20544701 1.00000000 6. 69 379 22 2.05277045 0.31262919 1.00000000 3. 71 357 44 1.90476190 0.29395552 1.0000000 2. 72 381 20 5.42257218 1.55509847 1.0000000 11.	•	387			.243650	.0000000	
65 381 20 1.84514436 0.36224271 1.0000000 2 68 380 21 2.50000000 1.20574701 1.0000000 6 69 379 22 1.51978892 0.50026867 1.0000000 2 70 379 22 2.05277045 0.31262919 1.0000000 3 71 357 44 1.90476190 0.29395552 1.00000000 2 72 381 20 5.42257218 1.55509847 1.00000000 11	•	387			.039222	.0000000	
68 380 21 2.50000000 1.20574701 1.0000000 6. 69 379 22 1.51978892 0.50026867 1.0000000 2. 70 379 22 2.05277045 0.31262919 1.0000000 3. 71 357 44 1.90476190 0.29395552 1.0000000 2. 72 381 20 5.42257218 1.55509847 1.00000000 11.	•	381			.362242	.0000000	
69 379 22 1.51978892 0.50026867 1.00000000 2.0000000 70 379 22 2.05277045 0.31262919 1.0000000 3.0000000 71 357 44 1.90476190 0.29395552 1.00000000 2.0000000 72 381 20 5.42257218 1.55509847 1.00000000 11.0000000	•	380		. 5000000	. 205747	.0000000	
70 379 22 2.05277045 0.31262919 1.00060000 3.0000000 71 357 44 1.90476190 0.29395552 1.00000000 2.0000000 72 381 20 5.42257218 1.55509847 1.00000000 11.0000000	9	379		. 5197889	. 500268	.0000000	.0000000
71 357 44 1.90476190 0.29395552 1.00000000 2.00000000 72 381 20 5.42257218 1.55509847 1.00000000 11.0000000	~	379		.0527704	. 312629	.0000000	. 0000000
72 381 20 5.42257218 1.55509847 J.00000000 11.00000000	~	357		. 9047619	. 293955	. 0000000	0000000.
	2	381		. 4225721	. 555098	0000000	. 0000000

Table C.1--continued

VARIABLE	Z	N MISSING	HEAN	STANDARD Deviation	MINIMUM	MAXIMUM
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	; ; ; ;	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SITENAUE-00		***************************************	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
(7)	289	12	0.30077121	0.45918397	0	1.00000000
TECH	900	11.	0.79948586	0.40090072	0	1.00000000
RONS DONS	9 0	12	0.15167095	0.35916360	0	1.00000000
S S S S S S S S S S S S S S S S S S S			0 17480720	0.38029123	0	1.00000000
	N (• •	0 30046373	0 AB612585	·c	1.00000000
CNSH	A (0	77.		1210017		1.00000000
RSN6	\$ 00 C	7 .	0.00463640	0.24630134	•	1.00000000
RSN7	70 C	77.	07/100710	7707010	· c	1 00000000
ESNE	7 (P)	77	0.0203030	**************************************	•	1 0000000
888		71	0.64010283	0.100000000		
RSN10	389	12	0.06940874	0.2544/522	O •	
LINSO	389	12	0.06683805	0.25006293	0	1.00000000
C [NSd	389	12	0.11825193	0.32332204	0	1.00000000

Table C.1--continued

VALUE	
2	
MINIMUM	
. 3	
STANDARD DEVIATION	11.125592666923111112559269669299866929999999999999999999999
MEAN STOPMANE BA	22 - 24 - 24 - 24 - 24 - 24 - 24 - 24 -
N KISSING	OHHOOOMAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
2	
VARIABLE	V V V V V V V V V V V V V V V V V V V

VARIABLE	=	N MISSING	HEAN	STANDARD DEVIATION	MINIMUM	MAXIMUM
		1	SITENAME-8A		***************************************	!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
	a	•	_		0000000	00
757		• ~	3.9922279B	0.77790375	1.0000000	5.00000000
797	•	~			.0000000	ğ
722	•	~	٠.		.000000	8
756		~			0000000	Š
V57		~	٦.		.000000	Š
V58	8	~	٦.		0000000	Š
657	•	~	``		000000	9
V60	8	~	٠.		.000000	8
761	•	~	•		0000000	ğ
V62	8	~	٠.		.000000	ğ
V63	•	~	٦.		0000000	8
V64	•	~	-:		0000000	Š
765	8	~	-:		.000000	Š
766	•	~	٠.		000000	ĕ
V67	8	-	٦.		.000000	Š
Vea	•	-	٠.		. 0000000	Š
690	80	. ~	٠.		000000.	Ŝ
070	40	-	•		.0000000	Š
	•	-	٠.		.000000	Š
272	8	-			. 0000000	ğ
100	60		-:		.000000	Š
727	8	~			.000000	3
V75	8	~	•		.000000	Š
V76	8	m	٠.		.000000	Š
VII	8	~	∹:		.0000000	ğ
V78	8	-	٠:		.000000	Š
610	8	m	٠:		000000	9
080	8	m			.000000	8
VBI	8	m	-:		.000000	ğ
V82	8	-	•		.000000	ğ
V83	an (•	∹`			
784	80	•	•			38
V85	8	→ •				
786	30 6	n -				Š
/87	0 0		: -			
992	8	•	; -			ĕ
602	3 Œ	,	٠,		000000	0
167	3 0	•			000000	0
140) Œ	~			.000000	ĕ
160	40	-			.0000000	ŝ
760	65	-			.000000	ĕ
\$6A		•	•		.000000	ŝ
967		-	Ξ.		.000000	š
160	•	S	۳.		.0000000	Š
960	•	~	٦.		.000000	8
664	•	ci	Ξ.		0000000.	Š
V100	8	~	٦.		.000000	8
VIOI	8	~	-:		0000000	8
V102	ă.	~	``.		. 0.300000	8

Table C.1--continued

VARIABLE	2	NIBBING	ИВАН	STANDARD DEVIATION	MINIMOM	MAXIMIM
			SITENAME=SA			
	786	•	3,38082902	1.05807732	1.0000000	
101A	986	.~	2.73316062	1.20882867	1.00000000	5.0000000
3015	386	~	2.71761658	1.25689807	1.0000000	•
9015	386	. ~	3.55181347	1.23736600	1.00000000	-
	270	10	2,79683377	0.95029402	1.0000000	
	378	. 6	2.74603175	0.99283781	1.00000000	•
		:=	2.46684350	1.08891360	1,0000000	-
4109	900	10	2 67282322	1.01760961	1.0000000	5.00000000
7110	בפנ	,,	3.37270341	1.33483304	1.00000000	
*****	,,,		1,12201592	1.31317715	1.00000000	5.00000000
7113 7114	186	7	3.38802083	1.27148368	1,00000000	8.00000000
9114	• c	·	2 97389034	1.36881776	1.00000000	5.00000000
777	, c	, ,	1 69553806	0.46078427	1.0000000	
9174	100	• •	4 25916230	5822514		0
6117	700	~	4 03906250	0.87377525		
777		•	4 17801047	8692702	00000000	0
1217	700	.	• •	0.80103527		
V122	700	1 0 W	10010017.5	0.00100.0		• •
V123	700	9 4	4.0101010	80		9
V124	9 (9 (n u	# 456500000000000000000000000000000000000			• •
V125	7 . 9 (n r	•			
V126	100	- (•		
V127	100	~ 0	•	0 08416311	00000000	4.00000000
7152	200	P 0	-	********		
V153	200		• •	0.1000tF.0	0000000	
V154	3.	A 4	70000000	1 60072002		
V155	676	7	3.404000	1 0087545	0000000	
9617	900	N 1	ď	1247787		11,0000000
/51/	2 6	1	7 403657	0817362	0000000	
8CTA	ה ה ה	7 -	730000000000000000000000000000000000000	0.264264.0		
6517	0 5 6	7.		1687392		
7160	9 / C	• "	2000000	1 2670312	0000000	• 7
Alei Viei	2,0	7.	3.6400000	200000000000000000000000000000000000000		
V162	375	7 1 (4.04205057	202393		•
V163	3/3	5 - (1.54/3333	0.40003004	000000.1	000000
V165	367	P (1.88828338	0.31544755	0000000.1	7.000000
V168	360	20	2.8222222	768/1/2	1.0000000	•
V169	365	7	1.39452055	17681	1.00000000	2.0000000
V170	356	32	2.22471910	0.58145634	1.0000000	3.0000000
V171	346	+ 2	1.30057803	0.45917344	1.00000000	2.0000000
V172	366	22	5.35245902	1.71977443	1.00000000	10.0000000

Table C.1--continued

Variable	2	N MISSING	MEAN	STANDARD DEVIATION	MINIMUM	MAXIMUM
			SITENAME-SA			
RSN1	374	14	0.26203209	0.44032907	0	1.00000000
RSN2	374	14	0.727273	0.44595837	0	1.00000000
RSN3	374	14	0.26737968	0.44318501	0	1.00000000
RSN4	374	14	0.17914439	0.38398687	0	1.00000000
RSNS	374	14	0.35294118	0.47852478	0	1.0000000
RSN6	374	14	0.08823529	0.28401674	0	1.00000000
RSN7	374	14	0.17914439	0.38398687	0	1.00000000
RSNB	374	14	0.03208556	0.17646342	0	1.00000000
RON9	374	14	0.62032086	0.48595712	0	1.00000000
RSN10	374	14	0.03208556	0.17646342	0	1.00000000
RSNII	374	14	0.04010695	0.19647289	0	1.00000000
RSN12	374	7.1	0.14973262	0.35728712	0	1.00000000

Table C.1--continued

MAXIMUM VALUE		000000
MINIMEN	000000000000000000000000000000000000000	
STANDARD DEVIATION	11.09914200 11.105923130 12.295313130 12.2953131356 11.10593131356 11.10593131356 11.10593131356 11.10593131356 11.10593131356 11.1059313131 11.1059313131 11.1059313131 11.10593141 11.1059313131 11.1059313131 11.1059313131 11.1059313131 11.1059313131 11.105931313131 11.105931313131 11.105931313131313131313131313131313131313131	
HEAN	23.10482201338826555555570156555701565557015655570156555701565570156557015655701565570156557015670156	
NI88ING	**************************************	3 6 6 7 7 7 5
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VARIABLE	7	V45 V46 V49 V50 V51

Table C.1--continued

VALUE		000000		000000	000000	0000000		000000	0000000	00000000	0000000		0000000	0000000	0000000	0000000			0000000	0000000	00000000	000000	0000000		0000000	0000000	0000000	0000000	0000000	00000000	0000000	0000000	000000	0000000	00000000	0000000	0000000		000000	0000000	00000000	0000000	0000000	
•		0.	•	 	•	•	•			•	٠		•	• •	5.0	9					•	9		•			in.				5.00	٠	•	. S	•	•	•	•		9		•		•
MINIMUM		1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	0000000	1.00000000			1.00000000	1.0000000		1.00000000	1.00000000	1.00000000	1.0000000	7.0000000	1.00000000	1.00000000		1.00000000		1.00000000	1.00000000	0000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000		1.00000000		0000000	1.00000000	1.0000000	1.0000000	1.00000000	1.0000001		1.000000000	
STANDARD DEVIATION		0.97842826	0.90053661	1.25349455	1.11484229	1.23266172	1.17422393	1 17768242	1.23821635	1.06905886	1.00081132	1.09640257	1 07695001	1,10225460	1.13132951	1.21407851	1.15343014	1.20624331	0.88066069	1.20798714	1.20540560	1.14718872	1.08389076	1.07018391	0.3474400	1.19246103	0.88743692	1.21730832	1.145/3/60	1.27847307	1.03764624	1.11246176	1.1/18299/	1.21817802	1.24925588	0.99181926	1.13988754	1.13852743	7.23844827	0.91245375	1.14342345	1.13455262	0.99866985);;;;;;;;
HEAN	SITENAME=SM	4.02661290	3.79677419	3.41841680	2.76328502	3.51007252	3.11935484	7 56174334	101774194	3.30942788	2.20467365	3.60823910	2.26752619	2 84410339	3.11916264	3.56521739	2.78629032	2.71854839	3.928051/4	2.71394037	3.03634895	2.85495568	3.24697337	2.87692308	7.1017017	2.52860596	2.00403551	2.95080645	3.85460420	2.81920904	2.80983078	2.41176471	3.35990338	3.33930/16 2.85552865	2.55447942	2.57038935	2.46806791	3.17946645	2.7/894/3/	3.66043867	2.77957861	.9741100	3.91329011 1 97475728	•
N MISSING	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11	:		. თ	10	:	11	3=	9	01	13	25	25	9	•	1	=	~ :	101	13	10	12	91,	12	20	12	11	E [12	10	91 91	ي م	77	12	15	7	7	97.	70 20 30	17	15	17	7
3		1240	1240	1230	1242	1241	1240	1240	1259	1241	1241	1238	1241	1761	1242	1242	1240	1240	1237	1239	1238	1241	1239	1235	1238	1241	1239	1240	1238	1239	1241	1241	1242	1239	1239	1236	1237	1237	1235	. v	1234	~	1234	0071
VARIABLE		V\$2	V 53	757	C 20	V57	NSB	657	097	107	V63	797	V65	706	~ &	692	070	110	772	F/S	7/0	776	777	V78	672	282	V82	V83	787	587	V87	887	687	067	160	76A	761	56A	967	797	000	V100	V101	707

Table C.1--continued

MAXIMUM VALUE	!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!	•	•	5.00000000	•	٠	•	٠	•	5.00000000	5.0000000	5.00000000	5.0000000	•	5.0000000	•	•	5.00000000	8.00000000	5.00000000	5.00000000	5.00000000	5.0000000	• 00000000	2.00000000	9.0000000	0.0000000.9	9.0000000	15.0000000	4.0000000	•	•	•	•	•	2.00000000	.0000000	2.00000000	3.00000000	-	11.00000000	5.00000000	•	5.00000000
MINIMUM	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•	•	1.00000000	•	•	•	•	0.0000000	•	•	•	1.00000000	•	•	•	-	•		1.00000000								1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000			
STANDARD DEVIATION	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.09958047	1.36466151	1.27026361	1.30892757	0.92203631	0.96273773	0.99379236	0.97217871	1.43469770	1.36836474	1.32435482	1.38642589	0.48923071	0.72171032	0.96015549	0.94189236	0.93398773	0.90541927	0.97152170	0.94978624	0.96070315	1.18562127	1.03648651	0.48254008	0.52207643	1.29238644	1.03512506	2.13049451	1.02575444	0.76520078	1.54734955	1.22575550	1.32360794	0.99212983	0.42125447	1.24776075	0.49882134	0.58169297	0.32657252	1.54698213	1.22217459	15020955	1.14119875
HEAN	SITENAME=SM -	. 25566343	.92058347	.09797571	.02759740	.48517298	.42317173	.17912901	.46299342	.95234249	.60226354	.87479806	. 70840065	.64906580						22815534		16155089		05867769		72667543	51574074	97512864	40201005	53184450	65754561	08864954	. 52902156	.90697674	64072848			46267361	96208113	87875752	85836910	61916667	64386989	70916667
MISSING) 8 9 9 9 9	s		16	•	7	7	•	· ·		~	7	~	7	~	13	•	•	•	15	•	•	•	. (4)	40	' -) LCT	95	9	~	45	77	45	m	_	53	7	6	7	3	8	~	7	51
2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1236	1234	1235	1232	1214	1217	1217	1216	1238	1237	1238	1236	1231	1238	1238	1240	1239	1239	1236	1238	1238	1227	1210	1211	761	216	1166	1194	1209	1206	1207	1206	1204	1208	1198	1144	1152	1134	966	1165	1200	5611	1200
VARIABLE		2007	V104	V105	V106	V107	V108	V109	V110	7117	VIIS	7116	V117	VIIB	9119	V120	V121	V122	7123	V124	V125	7126	V127	V152	V153	V154	7155	V156	V157	V158	V159	V160	V161	V162	Vi63	V165	V168	V169	V170	V171	V172	V173	V174	V175

Table C.1 -- continued

VARIABLE	2	N MISSING	MEAN	STANDARD DEVIATION	HINIMUM	MAXIMUM
	; ; ; ;		SITENAME=SM			
RONI	1219	32	0.25840853	0.43793938	0	1.00000000
RSN2	1219	32	0.75717801	0.42896436	0	1.00000000
RSN3	1219	95	0.17965546	0.38405777	0	1.00000000
RSNA	1219	32	0.16817063	0.37417125	0	1.00000000
RONS	1219	32	0.41427400	0.49279841	0	1.00000000
RSN6	1219	32	0.05742412	0.23274670	0	1.00000000
RSN7	1219	32	0.20590648	0.40452842	0	1.00000000
RSNB	1219	32	0.04840033	0.21469874	0	1.00000000
6NSE	1219	32	0.61197703	0.48749985	0	1.00000000
RSN10	1219	32	0.03609516	0.18660350	0	1.00000000
RSN	1219	32	0.04183757	0.20030003	0	1.00000000
RSN12	1219	32	0.15996719	0.36672607	0	1.00000000

Table C.1--continued

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Table C.1--continued

HAXIMUM VALUE		
MINIMUM		
STANDARD DEVIATION		1.089947386 1.08984757 1.0898144586 1.089814451 1.089813445 1.088813441 1.088813441 1.088813441 1.088813441 1.08813441 1.088134451 1.088134451 1.088134333 1.0881343451 1.0881343451 1.08813434 1.18657451 1.18657451 1.186814333 1.18681433 1.18681433 1.1868814 1.18681433
KEAN	SITENAM 1750074 1752094 17520994 175209994 17520999999999999999999999999999999999999	2.95899 3.258893 3.02040000 3.020400000 3.0204000000 3.02040000000000000000000000000000000000
N MISSING	**************************************	๚๛๚๚๛๚๛๛๚๚๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛
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VARIABLE	V V V V V V V V V V V V V V V V V V V	V V V V V V V V V V V V V V V V V V V

Table C.1--continued

MAX I MUN VALUE	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5.00000000	. 0000000	. 0000000	. 0000000	. 0000000	.0000000	.0000000	.0000000	.0000000	.000000.	.0000000		. 0000000	.0000000	.000000	. 0000000	٠	5.0000000	. 0000000	. 0000000	. 0000000	.0000000	.000000	.0000000	•	. 0000000	٠.	•	•	2.00000000	•	3.6	٠		•	•	.0000000	3.00000000	9	11.00000000
MINIMUM		1.00000000	-	. 0000000	. 0000000	. 0000000		.0000000	٠.	٦.	1.00000000	٦.	1.0000000	_	1.00000000	1.00000000	1.00000000	000000	1.00000000	•	1.00000000	٠.	1.00000000	1.00000000	. 0000000	1.00000000	•	1.00000000	1.00000000	1.00000000	1.00000000	1.0000000	1.0000000	•	1.00000000	1.00000000	1.00000000	.0000000	00000	000000	1.00000000
STANDARD DEVIATION		1.12927316	.3378650	.2567846	.3078816	.9393007	.0424113	.0799559	. 9991946	. 4274106	3259899	.3216330	. 3993251	.4323581	.6565902	.8836384	.8855710	.9581006	.9164585	.7771854	.8345535	.8581906	.9976266	.9116107	.3477704	4080324	. 1666666	.0702987	.9706150	.0368783	0.57507587	1967//5	. 2194749	3281809	.8079361	.4173071	.3310437	.4992307	. 5217268	.2175	869
HEAN	SITENAME=WR		•	٠.	٣.	۳.	•:	٠.	۳.	۲.	2.50299401							4.06287425	4.21492537	4.46706587	-	•	•	3.29518072	•	•	•	•	•	•	•	•	•	•	•	•	.8089172	.5394321	.6730769	.9503816	.9968354
N MISSING		~	•	1	Ś	•	œ	∞	3	•	7	7	7	•	7	•	®	7	•	-	60	•	6	•	13	297	332	52	16	12	16	12	7	16	15	19	27	24	53	79	25
2	; ; ; ; ; ; ;	_	•	~	•	m		m	~	m	334	~	~	~	~	m	~	m	~	~	~	~	~	•	~	3	S	316	325	329	325	329	329	325	326	322	314	317	312	262	316
VARIABLE	1 1 1 1 1 1	V103	V104	V105	V106	V107	V108	V109	V110	V114	V115	V116	V117	V118	V119	V120	V121	V122	V123	V124	V125	V126	V127	V152	V153	V154	V155	V156	V157	V158	V159	V160	V161	V162	V163	V165	V168	V169	V170	1711	V172

Table C.1--continued

MINIMUM MAXIMUM VALUE VALUE		1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000
STANDARD DEVIATION		0.38673804 0.41200658 0.40332317 0.36534796 0.4201670 0.26538228 0.46536580 0.16336589 0.1542631
HEAN	SITENAME=WR	0.18237082 0.78419482 0.20364742 0.293743234 0.02394355 0.02796353 0.07598784 0.0273562 0.02431611
N MISSING		2222222222
2		#####################################
VARIABLE		R R R R R R R R R R R R R R R R R R R

Table C.2
MEANS FOR ALL VARIABLES, SUPERVISORS

	MAXIMUM	; ; ; ;	5.00000000																																								
	MINIMIN			000000	.000000	. 000000			.00000	.00000	000000		.00000	.00000	.00000		.00000	.00000	. 00000		.00000	.00000	. 00000			.00000	. 00000		. 000000	00000	.00000	.00000	00000	.00000	.00000	.00000	. 00000	000000	000000	000000	.00000	000000	. 00000
SUPERVISORS	STANDARD DEVIATION		0.81533182																									1.10950463															
L VARIABLES,	MEAN	- SITENAME=OC	.0434782	.05/60 6 /	8750000	.8586956	.3913043	.6502/32	8251366	4098360	7978142	.3497267	7377049	2527472	.7704918	. 4066524 	6612021	.9836065	.4863388	.2568306	.1584699	8087431	.0491803	.9617486	17/0618. 76/0618.	5714285	. 5879120	2.92349727 3.62841530	. 6830601	.2404371	3204419	. 5469613	.4419889	4222222	2154696	.9447513	. 2983425	.3888888	5162370	9337016	.0722222	.4143646	.3701¢<7
MEANS FOR ALL	N MISSING																																										
	2		•	8	9 40		•	80 0	D C	9 60	•	•	30 G	9		80 4	8	100		₩ 0	30 G	9	•	•	30 0	9	•		3 40	00	D 4	8	•	20 4	9 60	8	8	8	29 4	9 Œ	8	8	₩ .
	VARIABLE		٧٦	77	5 5	VS.	9/	5	9 0	44 010	VII	V12	V13	\$1A	V16	V17	6 12	V20	V21	V22	V23	V25	V26	V27	V28	67A	V31	V32	V34	V35	V36 V37	V38	V39	070	V41	V43	777	745	V46	\ * * * * * * * * * * * * * * * * * * *	670	V50	V51

Table C.2--continued

VARIABLE	2	N NISSING	FEAN	STANDARD DEVIATION	MINIMOM	MAXIMUM
	1		SITENAME -OC			† † † † †
463	•	G	7		.0000000	0
		•	-	∹	.000000	00000
N54		0	7	• • `	. 0000000	
V55	•	0	•	٦.		
NS6	•	0	•	•		
V57	•	0	•	Ξ.		
NS8	00	•		•		
650	80 (96	•	;`		00000
090		-	•	: `		00000
197	9	> c	•	: -	0000000	00000
797	D 4	> C			0000000	00000
592	D 4	•			.0000000	. 00000
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507	9 G	• •		٠.	.0000000	0000
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990	•	~		٦.	.000000	0000
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		~	•	٦.	.0000000	00000
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727	•	~	٠.	٠.	0000000	.0000
V75	8	7	٦.	٠.	. 0000000	.0000
V76	8	~	₹	•	.0000000	.00000
777	8	7	٠.	٦.	. 0000000	. 00000
V78	8	~	•	٦.	. 0000000	. 00000
6/1	8	7	٦.	٦.	. 0000000	
V80	œ	~	•	•		
VB1	∞ •	m .	•	٠,		
V82	•	, 1	•			
V83	∞ (٠,	٠,	•		
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Table C.2--continued

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	SITENAME=OC		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
		0.78824456	1.00000000	5.00000000
		1.21742981	•	•
		1.07528979	1.0000000	000000
		1.04440.1 0.0440400	•	•
				0000000
		0.93938864 1.00083800		0000000
			000000	000000
		0.135010.1	0000000	000000
		9706/007·T		•
		1.25750730	0000000.	•
1000 1000 1000 1000 1000 1000 1000 100		1.172/8191		0000000
1001 1000 1000 1000 1000 1000 1000 100		1.28649151	0000000 T	•
1001 1000 1000 1000 1000 1000 1000 100		0.48835425	I . 0000000	•
1000 1000 1000 1000 1000 1000 1000 100		0.55196507	3.0000000	5.0000000
1000 1000 1000 1000 1000 1000 1000 100		0.72092416	•	•
1000 1000 1000 1000 1000 1000 1000 100		0.67856144	•	•
1000 1000 1000 1000 1000 1000 1000 100		0.79986946	1.00000000	•
1000 1000 1000 1000 1000 1000 1000 100		0.67230580	•	•
1002 1002 1003 1003 1003 1003 1003 1003		0.80131032	1.0000000	•
1884 1880 1880 1880 1880 1880 1881 1881		0.98510552	1.0000000	5.0000000
1882 1880 1880 1880 1880 1880 1881 1881		0.000000	1.00000000	
1880 1880 1880 1880 1880 1880 1881 1880 1881 1881 1881 40 1881		1 0000014	00000000	
1881 1880 1880 1880 1880 1881 1881 1880 40 1881 1881		1 08222425	1.00000000	0
1800 1800 1800 1800 1800 1801 1801 1801		1 12755675	9	2.00000000
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180 180 180 180 180 180 180 180 180 180		1.01006104		5.0000000
180 180 180 180 180 180 180 180 180 180		1.11046730	000000	000000000
180 180 180 180 180 181 181 180 180 180		6.1930361.1		20000000
180 180 180 180 180 181 181 180 180 181 181		0.3372020		0000000
180 180 180 180 181 181 180 180 180 40 181 181 180 40 144		1.14055450		•
180 190 180 180 180 180 180 180 180 40 181 181 180 190 190 190 190 190 190 190 190 190 19		1.15049400		000000
180 180 180 180 180 180 180 180 180 40 40 144		1.00521003		•
179 180 180 181 181 180 180 180 180 40 40 144		1.03902730 1.0390275		•
180 180 180 180 180 180 180 180 40 40 144		1 0560500		20000000
180 181 181 181 180 180 180 181 181 40 40 144		1.00630437		•
180 181 181 180 180 180 180 181 181 40 40 174		1.0709755		000000
181 180 180 180 180 180 181 181 181 40 40 174		1.03363646	000000	•
181 180 180 180 180 180 181 181 180 40 144 174		1.6067/0.1	00000	20000000
181 180 180 180 180 180 181 181 180 40 144 115	. 248618/8	0.94613312		•
180 180 180 180 180 181 181 180 40 144 115	. 32596685	0.95542436		•
180 180 180 181 181 181 180 40 144 177	. 49723757	0.85390807	1.000000	
180 180 181 181 181 180 49 144 177	. 8388888	1.16352330		? <
180 181 181 181 180 40 144 177	. 1111111	0.97006722	•	•
180 181 181 180 40 177	. 50000000	0.97166562		.0000000
181 3 2. 181 3 3 3. 180 4 1. 40 144 1.	. 50000000	0.95426125	•	3.000000
181 3 3. 3. 4. 1. 4. 1. 4. 1. 1. 7. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.	.87292818	1.16922897	1.0000000	5.0000000
180 4 1. 40 144 1. 7 177 3.	.81215470	0.55584400	1.00000000	4.000000
40 144 1.	. 78868889	0.40923541	1.00000000	2.0000000
7 177 3.	. 80000000	0.40509575	1.00000000	2.0000000
	.57142857	1.39727626	1.00000000	5.00000000
6 168 16 2.	.76190476	1.93684135	1.00000000	5.00000000
6 6	.42372891	2.68118480	1.00000000	15.00000000

Table C.2--continued

MAXIMUM VALUE		4.00000000	5.00000000	6.0000000	6.00000000	8.00000000	4.00000000	2.00000000	4.00000000	9.00000006	6.0000000	2.00000000	3.00000000	2.00000000	10.00000000
MINIMEN		1.00000000	1.00000000	1.0000000	2.00000000	1.0000000	1.0000000	1.00000000	1.0000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000	1.00000000
STANDARD		1.06929924	0.60826111	1.48875466	1.02317629	1.11860230	0.69374120	0.12908715	1.05204731	1.18776227	1.14619018	0.44126489	0.38878251	0.13691408	1.81544438
HEAN	SITENAME-OC	2.75138122	3.78453039	4.01657459	4.54748603	4.03910615	1.28176796	1.98314607	3.17816092	4.82954545	3.42372081	1.26256983	1.92178771	1.98101266	5.73743017
N MISSING		m	~	(4)	wi	ı vo	· (41	•	10	969	7	ď	· vn	26	'n
2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	181	181	181	179	179	181	178	174	176	177	179	179	158	179
VARIABLE	1	V158	V159	V160	V161	V162	V163	V165	V166	V167	V168	69 LA	V170	1717	V172

Table C.2--continued

MAXIMUM VALUE	1.00000000 1.000000000 1.000000000 1.00000000
MINIME	0000000000
STANDARD DEVIATION	0.42056832 0.4312273 0.37862568 0.33477348 0.36865888 0.24020217 0.24020217 0.25013963 0.25013963
MEAN 11 ENAME=0C	0.22777778 0.78333333 0.1722222 0.1277778 0.3888889 0.166667 0.1666667 0.06111111 0.05000000 0.0666667
NI99ING	*********
Z	1180 1180 1180 1180 1180 1180
VARIABLE	RSN1 RSN2 RSN3 RSN4 RSN6 RSN6 RSN1 RSN10 RSN10 RSN10

Table C.2--continued

MAXIMUM	
MININCH	
STANDARD Deviation	
MEAN STERNAMESCO	2.90066225 2.1589434795 2.1589434795 2.1589434795 2.1589434795 2.1589434795 2.1589434795 2.1589434795 2.1589434795 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15894391 2.15866667 2.15866667 2.158943333 2.15894391 2
MISSING	
2	1861 1861 1861 1861 1861 1861 1861 1861
VARIABLE	V V V V V V V V V V V V V V V V V V V

Table C.2--continued

VARIABLE	2	N MISSING	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE
		1 1 1 1 1 1	SITENAME-00			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
752	151	1	3.64238411	1.01550888	1.00000000	5.00000000
753	151	-	4.18543046	0.61540202	1.0000000	
154	151	~		0.84852814	1.00000000	
V55	151	⊶,		1.02092889	000000000000000000000000000000000000000	
.56	161	-4 -	3.19801323	1.00934633		
75	151			0.86995471	1.0000000	
900	151	٠.		1.07066029	1,00000000	
600	151	•		0.98572594	1.0000000	
195	151	•		0.93822433	1.0000000	
162	151	. —	3.99337748	0.84456449	1.00000000	5.00000000
163	151	~		0.83027696	1.0000000	
194	151	-		1.22368098	1.0000000	
165	151			0.91511709	1.00000000	
99/	151			0.99055139	0000000.1	
167	150	~• (0.833/4039	1.0000000	
894	150	~	3.65333333	0.64554470		
69/	051	~ <		0.000000	200000	
2	061	~		7.754000 T		
	200	→ (1.04004090 0.4012036		
		• •		0.00130	1.0000000	•
27.	200	• •	3.7533333	0.95493537	1.00000000	
• C	90	• ~	3.6666667	1.00779956	1.00000000	
90	150	.~	3.9066667	0.83823614	1.00000000	5.00000000
ננו	150	~	3.7333333	0.96701760	1.0000000	
178	150	~	3.14666667	1.10754985	1.00000000	
611	150	~	2.26666667	1.00779956	1.00000000	
780	150	~	4.3466667	0.59060504	7.0000000	5.00000000
781	150	~	2.98666667	1.16427047	0000000.1	
782	051	~	2.2333333	50/204/6.0	0000000.T	
59.	001	~ (1.1044190		•
900	200	• ~	2.4200000	1.28109643	1.0000000	5.00000000
987	150	. ~		1.01991358	1.0000000	
787	150	7		1.10730743		5.00000000
788	150	7	3.31333333	1.06900610	1.00000000	
789	150	7		0.98526050	1.00000000	
06/	150	~1		0.82467538	2.00000000	
791	150	~ 0		1.00426384	•	
192	150	~ 0		1.099/050/	•	
56.	120	7		0.00200		2000000
7 65	001	4 C		0.04/39363		
901	051	• ~	573333	0827919	• -	
797	150	• ~	.0006666	5850103	.0000000	0000000
86/	151	-	0860	04524	0000000	
66/	151		.1986755	np94638	•	5.0000000
7100	151	- -	40.7	15/20.0		000000
101	151	- ~	2.71333333	628 628	1.0000000	5.0000000
707) 1	•	999944	100101.		111111111

Table C.2--continued

MAXIMUM VARUB	
MINIMEM	
STANDARD DEVIATION	0
MEAN	3.756 3.756 3.756 3.756 3.756 3.756 3.756 3.756 4.352 3.755 4.352 3.755 4.355 4.
NISSING	
3	
9	

Table C.2--continued

V158 148 148 148 V159 148 148 148 V160 148 148			DEVIATION	VALUE	VALUE	
158 148 159 148 160 148 161		SITENAME=00		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
159 140 160 140 161	•	2.50000000	1.12787803	1.00000000	4.00000000	
160 148	•	3.87837838	0.47958890	1.00000000	₹.00000000	
161	•	3.68243243	1.40474009	1.00000000	0.00000009	
	•	4.75000000	0.83197168	3.00000000	6.0000000	
148	-	3.83108108	1.15109243	1.00000000	5.00000000	
163	•	1.42567568	0.74770594	1.00000000	₹.00000000	
165	'n	1.94557823	0.22762361	1.00000000	2.00000000	
	-	2.95945946	1.11805454	1.00000000	4.00000000	
	'n	4.62585034	1.12998293	1.00000000	7.00000000	
	•	3.0000000	0.99654576	1.00000000	6.0000000	
	•	1.32191781	0.46881996	1.00000000	2.00000000	
	•	2.07534247	0.28972321	1.00000000	3.00000000	
171 141	11	1.91489362	0.28003474	1.00000000	2.0000000	
	eri	5.97959184	1.81118817	2.00000000	11.00000000	

Table C.2--continued

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Table C.2--continued

VARIABLE	2	N MISSING	MEAN	STANDARD	MINIMUM	MAXIMUM VALUE
	! ! ! ! !	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SITENAME=SA	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! !
7	178	0	3.96067416	1.01046703	1.00000000	5.00000000
V2	177	(2.57627119	1.30366480	1.0000000	5.00000000
۲3 : ۲3	1 / 00	-	بَ مَ	1.08450769	1.00000000	5.00000000
4	1 / 0	9 0	2.87640449	1.15293999		0000000
7 9 2	178	0		1.25548375	0	000000
25	177		2.39548023	1.10863446	1.00000000	0000000
. 60	175	•	3.10285714	1.25521572	1.00000000	
0.5	176	7	3.14204545	1.12490981	1.0000000	
VIO	175	m	4.40000000	0.68648698	1.00000000	3.0000000
VII	176	~	3.75568182	0.99281510	1.00000000	
V12	176	~•	3.29545455	1.0/606/88	0000000.T	
V13	176	~	3.05681818	1.24061038		2.0000000
	176	~ (3.65909091	1.10172289		5.0000000
VIS	176	•	3.32386384	0 000000		0000000
V16	175	∾ (3.90285/14	1 12671226	0000000	5.00000000
VI7	9/1	٧.	3.60441413	1 031 14044	1,0000000	5.00000000
	9/1	~ ~	3.33441413	1 13860457	1,00000000	0000000
617	6/1	~ c	3.33142031 2.0324364	1,32242153	000000001	5.00000000
V20	9/1	•	#0000000000000000000000000000000000000	1 17549382	1 00000000	5.0000000
127	9/1	• •	3.31430000	1.17117712	1.00000000	5.00000000
777	270	•	3.15000304	1.19862316	1.00000000	5.00000000
	176	• ~	3.06818182	1.35474155	1.00000000	0000000
***	177	•	3.97175141	0.88823995	1.00000000	5.00000000
227	111	•	3.19774011	1.26598663	1.00000000	2.00000000
220	176	. ~	3.17613636	1.28627874	1.00000000	2.00000000
000	177			0.78983820	1.00000000	5.00000000
02A	177		•	1.19093908	1.00000000	000000
V30	177	-	005649	1.11582100	1.00000000	5.00000000
Val	111	-		1.18105987	1.00000000	5.0000000
V32	177	~		1.15166635	1.0000000	0000000
V33	111			7552526.0		0000000
V34	177	-		1.14036166	000000	5 00000000
V35	177	- • •		1.11039740		2.00000000
736	177			1.05592831	1.0000000	5.00000000
757	170	→ ⊂		1.07482104	1.00000000	5.00000000
000	178	• •	. (4)	1.07462908		5.00000000
040	177	-	.1694915	1.13045459	1.00000000	5.00000000
V41	178	0	۳.	1.02070236	1.00000000	5.00000000
V42	178	0	٦.	0.86843181	1.00000000	5.00000000
V43	178	0	٠.	1.08591158	1.00000000	5.00000000
770	178	0		0.77952680	1.0000000	2.0000000
V45	178	o (4719101	0.92167727	1.00000000	•
V46	178	0	.1179775	1.10602477	T.0000000	•
747	178	90	3.16292135	1016197		
048	178	- 0	1608/07.			
749	178	-		04/07/6.		
050	9/1		0.303300.0	1 02380751		5.0000000
V5I	0/1	•				

Table C.2--continued

VARIABLE	22.	N MISSING	HEAN	STANDARD DEVIATION	MINIMUM	MAXIMUM VALUE
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1		SITENAME=SA			
V52	177		.2994350	1.17533831	1.00000000	5.00000000
V53	178	0	. 3146067	0.63948259	1.00000000	
757	178	96	4.21910112	0.89080379	1.00000000	5.00000000 6.000000000000000000000000000
555	177	-	6//K/10.	1.103/4090	1.00000000	5.00000000
05A	177	• ~	.8531073	1.20175249	1.00000000	5.00000000
V58	178	0	.966292	1.03552097	1.00000000	
65A	178	0	.7134831	1.21754509		5.00000000
090	177	-		1.21276065	000000	5.00000000
V61	177	-			1.0000000	
V62	178	0	4.03370787	0.83631473	1.00000000	5.00000000
V63	176	~ .		1.02380751	1.0000000	5.0000000
190	111	→ (1.12304/39		000000
502	170	n c		1 10923422	1.0000000	
994	178	• •		1.00028562	1.00000000	5.0000000
199A	178	• •		0.98772058	1.00000000	5.00000000
690	178	0		0.99704381	1.00000000	5.00000000
V70	178	0			1.00000000	5.00000000
V11	178	0		1.10504863	1.00000000	5.00000000
V72	178	0	4.35393258	0.61388016	1.00000000	5.0000000
V73	178	ο.	3.79775281	0.87242470	1.00000000	5.00000000
7/1	177	~ •			1.0000000	5.00000000 5.00000000000000000000000000
V75	178	ο,		1.01610531		S. 00000000
V76	111	→ «	ï			3.000000
V77	8/1	> c	•		1.0000000	2.000000
10 C	9/1	-	3.4/191011 2.6202124B	1.07431093		5.0000000
A 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	170	-	•		1.0000000	
780	178	٦ C	3 28651685		1.00000000	
782	178	• •	: 7		1.00000000	
CB3	177	-4	` :	1894287		5.00000000
V84	176	7	٦.	1.21536430	1.00000000	5.0000000
V85	178	0	``	1.21336691	1.00000000	0000000
V86	178	0	4.08988764	0.94648263	1.0000000	000000
V8.7	178	o •	.9550561	1.16357245	1.00000000	
V88	178	> (. 5348314	1.03951326	1.0000000	3.0000000
582	9/1	-	3.8033/0/9	1.02545357		
790	177	-	•	1 02401192	1.0000000	
160	178	4 0	•	1.15034929	1.00000000	5.00000000
160	176	~		0.94077890	0	000000
767	177	-	3.36158192	1.13031260	0000000	5.00000000
V95	178	0	•	1.01835189	1.00000000	5.00000000
96/	178	0	•	1.14831952	1.0000000	5.00000000
797	177	→ •	•	0.61666276	1.0000000	5.0000000
960	178)	3.00000000	1.08403932	1.0000000	3.0000000
0010	178	4 6		0.97504246	1.00000000	5.00000000
V101	177		.8700565	1.17263132	1.0000000	5.00000000
V102	178	0	•	1.25715119	1.00000000	

Table C.2--continued

178 0.0000000 0.0000000 0.0000000 0.0000000 0.00000000	VARIABLE	2	N MISSING	HEAN	STANDARD DEVIATION	MINIMUM	MAXIMUM
178 178	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			SITENAME=8A	1	, , , , , , , , , , , , , , , , , , , ,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
17.00000000 1.00000000 1.00000000 1.00000000 1.00000000 1.00000000 1.00000000 1.00000000 1.00000000 1.00000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.000000000 1.00000000 1.00000000 1.000000000 1.000000000 1.00000000 1.0000000000	103	7	0	.7303370	.9830661	.0000000	.0000
176 2 2.4829545 1.14467824 1.00000000 2.00000000 1.00000000 2.7846991 0.9971874 1.00000000 2.00000000 1.00000000 2.7846991 0.9971874 1.00000000 2.00000000 2.00000000 1.00000000 2.8424871 1.00000000 2.00000000 2.00000000 2.8424871 1.00000000 2.000000000 2.0000000000		. ~	0	. 6966292	.2658441	.0000000	.000000
178 0.9551885 1.00000000 5.00000000 1.0000000000	0	-	~	. 4829545	.3048237	.0000000	.0000000
176 2. 2. 78405991 0.9271864 1.00000000 5.0000000 176 1.00000000 5.00000000 176 1.00000000 5.00000000 176 1.00000000 5.00000000 5.00000000 1.00000000 5.000000000 5.00000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.0000000000	0	~	0	.7865168	.1246785	.0000000	
176 2 2 2 2 2 2 2 2 2	o	-	~	. 7840909	.9251886	.0000000	. 0000000
176 176	0	~	7	.8636363	.9877167	.000000.	. 0000000
17	0	~	~	.6079545	.0900822	.0000000	.0000000
176 176 177	۰,	-	~	.8342857	.9773124	.0000000	.0000000
17	• -		~	.7443181	.2409542	.0000000	.0000000
1	- ۱	. ~	~	.6818181	.2832588	.0000000	.0000000
17	- ۱	٠,		7514124	.2410180	.0000000	.0000000
1	- ۱	٠,	۰,	8531073	4384745	.0000000	.0000000
17. 1. 1. 1. 1. 1. 1. 1.	- ۱	٠,	•	5197740	5010261	.0000000	.0000000
17	٠,	- ۲	• ~	3011363	6720534	.0000000	.0000000
177 1 4 27118644 0 77287777 2 00000000 5 000000000 5 00000000	→ C	- r	•-	2090395	. B162606	.0000000	.0000000
17	40	- 6	4 ~~	3672316	7728707	.0000000	.0000000
24 1727277 0.67573913 2.0000000 5.000 25 177 1 4.31073446 0.8254176 2.00000000 5.000 26 177 1 4.22594303 0.8826937 1.00000000 5.000 27 178 4 2.2594303 0.9861297 1.00000000 5.000 29 174 4 2.758630 1.1979928 1.00000000 5.000 29 172 6 2.7758620 1.00000000 5.000 30 172 6 2.7758620 1.00000000 5.000 31 172 6 2.7758614 1.00000000 5.000 31 172 6 2.7034837 1.00000000 5.000 32 172 6 2.7034837 1.00000000 5.000 34 172 8 1.752442 1.1724806 1.00000000 5.000 34 171 3.1452442 1.7124816 1.00000000 5.000 34	40	٠,	• ~	2711864	7110453	0000000	.0000000
25 177 1 4.2954344 0.86254176 2.0000000 5.000 26 177 1 4.29543503 0.8826937 2.0000000 5.00 26 177 1 4.2259887 0.96812979 1.0000000 5.00 28 177 4 2.7586207 1.2027922 1.0000000 5.00 30 172 6 2.0326336 1.0499228 1.0000000 5.00 31 172 6 2.0326336 1.0499228 1.0000000 5.00 31 172 6 2.0326336 1.174414 1.0000000 5.00 31 172 6 2.034887 1.1754814 1.0000000 5.00 33 172 6 2.134887 1.1500888 1.0000000 5.00 34 172 6 3.402345 1.171446155 1.0000000 5.00 34 171 7 3.547638 1.17114605 1.00000000 5.00 34 <t< td=""><td>46</td><td>- ^</td><td>• ~</td><td>4772727</td><td>6757391</td><td>.0000000</td><td>.0000000</td></t<>	46	- ^	• ~	4772727	6757391	.0000000	.0000000
177 1 4.23944503 0.88269327 1.00000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.000000000 5.0000000000	7 4	٠,	• ~	3107344	8254117	.0000000	.0000000
177 1	,	•	• ,	2994350	.8826932	.0000000	.0000000
177 178 179		٠,		2316384	8101024	.0000000	.0000000
174 4 2.77586207 1.20273928 1.00000000 5.000 174 6 2.77586207 1.20273922 1.00000000 5.000 172 6 2.77255814 1.14775414 1.000000000 5.000 172 6 3.4302256 1.15003888 1.00000000 5.000 173 6 3.43022256 1.15003888 1.00000000 5.000 171 7 3.647642 1.17798806 1.00000000 5.000 171 7 3.4152046 1.0440555 1.00000000 5.000 171 7 3.4152046 1.04465125 1.00000000 5.000 171 7 3.4152046 1.04465125 1.00000000 5.000 171 7 3.415204 1.1789636 1.00000000 5.000 172 6 3.416538 1.1789636 1.00000000 5.000 173 6 3.416538 1.1789636 1.00000000 5.000 174 7 2.357215 0.9556195 1.00000000 5.000 175 6 2.7790637 1.2465108 1.00000000 5.000 175 6 2.7790637 1.0465416 1.00000000 5.000 175 6 3.3139535 1.25681875 1.00000000 5.000 175 6 3.3139535 1.25681875 1.00000000 5.000 175 7 3.4853801 0.91454629 1.00000000 5.000 175 7 3.26900585 1.25681875 1.00000000 2.000 175 8 8 8 8 8 8 8 8 8	2.5	٠,	, ,	.2259887	.9681297	.0000000	.0000000
172 6 2.77586207 1.20273922 1.00000000 5.00000000 1.000000000 5.00000000 1.000000000 5.0000000000000000000000000		. ~	0	.1292134	.1979928	.0000000	.0000000
172 6 2.09302326 1.04099580 1.00000000 5.00000000000000000000000000	. 6	-	₩	.7758620	.2027392	.0000000	.0000000
172 6 2.7325814 1.14375414 1.00000000 5.000000000 1.72 1.28390714 1.000000000 5.0000000000000000000000000	30	~	9	.0930232	.0499558	.0000000	.0000000
172 6 2.70348837 1.28390374 1.00000000 5.000 172 6 3.43023256 1.150000000 5.000 170 6 3.43023256 1.1712255 1.00000000 5.000 171 7 3.08470588 1.1711225 1.00000000 5.000 171 7 3.08487050 1.04465155 1.00000000 5.000 171 7 3.81286550 1.04692122 1.00000000 5.000 171 7 3.81286550 1.074663128 1.00000000 5.000 171 7 3.3274658 1.11582428 1.00000000 5.000 172 6 3.19166047 1.14623361 1.00000000 5.000 172 6 3.4302326 0.95560195 1.00000000 5.000 172 6 2.34302326 0.96687979 1.00000000 5.000 171 7 2.3567255 0.95560195 1.00000000 5.000 172 6 2.77906977	31	~	9	.7325581	.1437541	. 0000000	
172 6 3.43022256 1.15003888 1.00000000 5.00000000 1.000000000 5.00000000 1.000000000 5.0000000000000000000000000	32	~	9	. 7034883	.2839037	.0000000	.0000000.
172 6 3.1976442 1.17298806 1.00000000 5.000 170 7 3.08470588 1.17112255 1.00000000 5.000 171 7 3.08126550 1.0465155 1.00000000 5.000 171 7 3.48126550 1.07824728 1.00000000 5.000 171 7 2.32748538 1.11882420 1.00000000 5.000 172 6 3.19186465 0.9668797 1.00000000 5.000 172 6 3.4186465 0.9668797 1.00000000 5.000 172 6 3.4186465 0.96560195 1.00000000 5.000 172 6 2.34033236 0.95560195 1.00000000 5.000 171 7 2.35672515 0.95560195 1.00000000 5.000 171 6 2.34303236 0.96560195 1.00000000 5.000 171 7 3.74853801 0.91454629 1.00000000 5.000 172 6 <	33	1	9	.4302325	.1500388	. 0000000	. 000000
5 170 8 3.56470588 1.17112255 1.00000000 5.000 171 7 3.41824135 1.108460555 1.00000000 5.000 171 7 3.41824550 1.07924728 1.00000000 5.000 171 7 3.38126550 1.07924728 1.00000000 5.000 171 7 3.381266550 1.07924728 1.00000000 5.000 171 7 3.381266550 1.07924728 1.00000000 5.000 172 6 3.19186047 1.11623361 1.00000000 5.000 172 6 3.41860465 0.9688779 1.00000000 5.000 172 6 2.34572315 0.9568779 1.00000000 5.000 172 6 2.97093023 1.24453108 1.00000000 5.000 171 6 2.77466441 1.06404461 1.00000000 5.000 172 6 2.7746641 1.00000000 5.000 170 1.77601751	34	-	9	.1976744	1729880	. 0000000.	. 0000000
171	35	_	6 0 (.5647058	. 1711225	. 000000	000000.
171 7 3.4930468 1.04465155 1.00000000 5.000 171 7 3.54970760 1.04692122 1.00000000 5.000 171 7 3.38011696 1.07924728 1.00000000 5.000 171 7 2.32748538 1.1158242 1.00000000 5.000 172 6 3.19186047 1.14623361 1.00000000 5.000 172 6 3.41860465 0.95560195 1.00000000 5.000 172 6 2.34302326 0.95560195 1.00000000 5.000 172 6 2.34302326 0.96640195 1.00000000 5.000 172 6 2.7790697 1.046905175 1.00000000 5.000 172 6 2.7790697 1.08905175 1.00000000 5.000 172 6 2.7790697 1.00000000 5.000 172 6 3.3139535 1.25681875 1.00000000 2.000 170 1.97368421 0.15222142	36	~	7	.0818713	1084005	. 0000000.	
171	37	-	7	.4152046	.0446515		
171	38	~	~ (0101666	7176980.		
171 7 3.3801139 1.11582420 1.0000000 2 172 6 3.41860465 0.96687979 1.00000000 4 172 6 3.43672515 0.96687979 1.00000000 5 172 6 2.34302326 0.986773853 1.00000000 6 2.34302326 0.98773853 1.00000000 5. 171 6 2.77906977 1.0640461 1.00000000 5. 171 6 2.77906977 1.0640461 1.00000000 5. 172 6 3.2690585 1.08905175 1.00000000 5. 172 6 3.3139535 1.25681875 1.00000000 2. 172 6 1.76744186 0.15222142 1.00000000 2. 172 6 1.7744186 0.15222142 1.00000000 2. 170 8 2.64117647 1.91708569 1.00000000 2. 5 9.22674419 2.69085192 4.00000000 15.	39	- (- (. 8128055	7/8/6/0.		
172	9	- (٠,	.30011006.	.1/6963t		000000
172 172 173		٠,	~ 4	. 34 / 40 J	3830611.		0000000
44 171 7 2.35672515 0.95560195 1.00000000 5.0 44 172 6 2.34302326 0.88773853 1.00000000 5.0 45 172 6 2.97093023 1.24453108 1.00000000 5.0 47 172 6 2.77906977 1.06404461 1.00000000 5.0 49 171 7 3.74853801 0.91454629 1.00000000 5.0 49 171 7 3.74853801 0.91454629 1.000000000 5.0 50 172 6 3.33139535 1.25681875 1.000000000 5.0 52 172 6 3.51162791 0.77601751 2.00000000 2.0 53 140 1.97368421 0.1522142 1.00000000 2.0 54 170 2.00000000 2.0 2.00000000 2.0 56 172 4.00000000 15.0 57 2.64117647 1.91708569 4.00000000 15.0 57 2.69085192 4.00000000 15.0	4.	٦,	3 4	4186046	9668797	0000000	.0000000
45 172 6 2.34302326 0.88773853 1.00000000 5.0 45 172 6 2.97093023 1.24453108 1.00000000 5.0 48 172 6 2.77906977 1.06404461 1.00000000 5.0 49 171 7 3.2490585 1.08905175 1.00000000 5.0 50 172 6 3.3139535 1.25681875 1.00000000 5.0 52 172 6 3.51162791 0.77601751 2.00000000 6.0 53 172 6 1.76744186 0.42369631 1.00000000 2.0 53 170 1.97368421 0.1522142 1.00000000 2.0 54 170 2.00000000 2.0 2.00000000 2.0 56 170 2.64117647 1.91708569 1.00000000 15.0 57 172 4.00000000 15.0 15.0	•		, ~	3567251	9556019	0000000	.0000000
172 6 2.97093023 1.24453108 1.00000000 5.000 171 7 3.74853801 0.91454629 1.00000000 5.000 172 6 2.77906977 1.06404461 1.00000000 5.000 172 6 3.3139535 1.25681875 1.00000000 5.000 172 6 1.76744186 0.42369631 1.00000000 4.000 4 177 2.00000000 2.000 2.000 5 170 1.97368421 1.00000000 2.000 6 1.77 2.00000000 2.000 2.000 5 1.70 8 2.64117647 1.91708569 1.00000000 15.000 7 1.72 6 9.22674419 2.69085192 4.00000000 15.000			- 16	3430232	8877385	.0000000	.0000000
171 7 3.74853801 0.91454629 1.00000000 5.000 172 6 2.77906977 1.06404461 1.00000000 5.000 172 6 3.33139535 1.25681875 1.00000000 5.000 5.000 172 6 3.51162791 0.77601751 2.00000000 4.000 4.000 1.97368421 0.15222142 1.00000000 2.0000	45	٠,	.	9709302	2445310	.0000000	.0000000
172 6 2.77906977 1.06404461 1.00000000 5.000 171 7 3.2690685 1.08905175 1.00000000 5.000 2 172 6 3.3139535 1.25681875 1.00000000 5.000 3 172 6 1.76744186 0.42369631 1.00000000 2.000 4 1 177 2.00000000 2.000 2.000 5 170 8 2.64117647 1.91708569 1.00000000 2.000 7 172 6 9.22674419 2.69085192 4.00000000 15.000	7	. ~	7	7485380	9145462	.0000000	.0000000
171 7 3.26900585 1.08905175 1.00000000 5.000 172 6 3.3139535 1.25681875 1.00000000 5.000 3 172 6 1.76744186 0.42369631 1.00000000 2.000 4 38 140 1.97368421 0.1522142 1.00000000 2.000 5 170 8 2.64117647 1.91708569 1.00000000 2.000 7 172 6 9.22674419 2.69085192 4.00000000 15.000	· a	٠,		1790697	.0640446	.0000000	.0000000
172 6 3.3139535 1.25681875 1.00000000 5.000 172 6 3.51162791 0.77601751 2.00000000 4.000 3 172 6 1.76744186 0.42369631 1.00000000 2.000 4 38 140 1.97368421 0.1522142 1.00000000 2.000 5 1 177 2.00000000 2.000 2.000 6 170 8 2.64117647 1.91708569 1.00000000 6.000 7 172 6 9.22674419 2.69085192 4.00000000 15.000	9	٠,		2690058	.0890517	.0000000	.0000000
172 6 3.51162791 0.77601751 2.00000000 4.000 3 172 6 1.76744186 0.42369631 1.00000000 2.000 4 38 140 1.97368421 0.1522142 1.00000000 2.000 5 1 177 2.00000000 2.000 2.000 6 170 8 2.64117647 1.91708569 1.00000000 6.000 7 172 6 9.22674419 2.69085192 4.00000000 15.000	20		• •	.3313953	.2568187	.0000000	.0000000
3 172 6 1.76744186 0.42369631 1.00000000 2.000 4 38 140 1.97368421 0.1522142 1.0000000 2.000 5 170 2.00000000 2.000 2.0000 2.0000 6 170 8 2.64117647 1.91708569 1.00000000 6.0000 7 172 6 9.22674419 2.69085192 4.00000000 15.000	52	~	9	.5116279	.7760175	.0000000	.0000000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	53.	7	9	.7674418	.4236963	.0000000	.0000000
5 17 2.00000000 . 4.00000000 6 1.00000000 6.000000 7 1.91708569 1.00000000 6.00000 7 1.91708569 1.00000000 15.00000 7 1.91708569 4.00000000 15.00000 7 1.00000000 15.00000 7 1.00000000 15.00000 7 1.00000000 15.00000 7 1.00000000 15.00000 7 1.000000000 15.00000 7 1.000000000 15.00000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.000000000 7 1.0000000000	54	•	4	.9736842	.1522214	.000000.	.0000000
6 170 8 2.64117647 1.91708569 1.00000000 6.0000007 172 6 9.22674419 2.69085192 4.00000000 15.0000	55		7	.0000000		. 0000000.	
57 172 6 9.22674419 2.69085192 4.00000000 15.0000	S	~	જ	.6411764	.9170856	0000000.	
	S		•	. 226 /441	. 69089.	, 000000	

Table C.2--continued

VARIABLE	3	N MISSING	ИВАИ	STANDARD DEVIATION	MINIMUM	MAXIMUM
	1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SITENAME=SA			† ; ; ; ;
9317	121	7	2.48538012	1.01955426	1.00000000	4.00000000
0517	172	•	3.81395349	0.67558297	1.0000000	9.0000000
0910	121	,	3.444444	1.67019235	1.00000000	6.0000000
1917	121		4.35672515	1.19124198	2.00000000	000000009
1917	121		3,73099415	1.26404051	1.00000000	5.00000000
2017	171		1,67836257	1.01549739	1.00000000	4.00000000
7917	170	• •	1.97647059	0.15202543	1.00000000	2.00000000
5915	891	9	2.89880952	1.07580846	1.00000000	4.00000000
2915	9 9	01	4.38690476	1.08845655	2.00000000	7.00000000
945	167		3.27544910	1.12830329	1.00000000	6.00000000
0917	2 2		1.25000000	0.43430721	1.00000000	2.00000000
2012	167		2.08982036	0.60942742	1.00000000	3.00000000
מינה	150	6	1.42767296	0.49630431	1.00000000	2.00000000
V172	167	=======================================	6.05988024	1.78244653	1.00000000	10.0000000

Table C.2--continued

Variable	z	N MISSING	MEAN	STANDARD DEVIATION	MINIMUM	MAXIMUM VALUE
			SITENAME=SA			
(N)d	175	M	0.29714286	0.45831131	0	1.00000000
CNSO	175) (r)	0.7600000	0.42830862	0	1.00000000
220	175) (न	0.18285714	0.38765854	0	1.00000000
770	175	, ~	0.07428571	0.26298776	0	1.00000000
5N50	175) (**	0.41142857	0.49350461	0	1.00000000
9700	175) (m	0.13714286	0.34498519	0	1.00000000
720	175) M	0.15428571	0.36225892	0	1.00000000
620	175) (eq	0.08571429	0.28074496	0	1.00000000
922	175) (T	0.63428571	0.48301190	0	1.00000000
CLASC	175	m	0.0400000	0.19652147	0	1.00000000
נומטם	175	1 6	0.04571429	0.20946409	0	1.00000000
RSN12	175	. m	0.1200000	0.32589400	0	1.00000000

Table C.2--continued

VARIABLE	2	N MISSING	ИБАЛИ	STANDARD DEVIATION	MINIMOM	MAXIMUM
	1	1 8 1 1 1 1 1 1	SITENAME = SM	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
7	166	0	3.97590361	0.98443528	1.00000000	.0000000
V2	166	0	2.33132530	1.18775854	1.00000000	5.0000000
V3	166	0	3.0000000	1.11735619	1.0000000	
**	166	0	3.62048193	1.1/831508	1.000000	5.00000000
\$ <u>\</u>	991	>		1 22259667	1 0000000	
, Ae	997	-		1 14705832	1,0000000	0000000
۲A وو	691	- C	2 92582927	1.29444768	1.00000000	
D 9	7 Y Y	•		1.17286391	1.00000000	5.00000000
55	16.5	•		0.86600407	1.00000000	5.00000000
(T)	165	ı	3.40606061	1.11474032	1.00000000	.0000000
V12	165	-	•	1.14898972	1.00000000	5.00000000
V13	165	-		1.05705667	1.00000000	000000
V14	165			1.18371557	1.0000000	2.0000000
V15	165			1.22223790	7.0000000	
V16	165	 4 ,	3.87272727	1.04659742	7.000000	3.000000
V17	165	 1 •		1.18143436		
V18	165			70678001.1		200000
V19	165	 4 ,		19169791.1	7.	
V20	165	- -1 •		1.33644180		2000000
V21	401	→.		1.433/0303	0000000	
V22	101			1 14350895	1.00000000	0000000
£23	COT	-		1.33924227	1.00000000	5.00000000
424 	100	4 -	42000	0 98585712	00000000	5.00000000
575	100	-4	3696969	1,31234403	1.00000000	
97.0	100	•	7333	1.28373186	1,00000000	5.00000000
777	165	•	3.60000000	1.07521977	1.00000000	5.00000000
970	165	• •	2.02424242	0.93019481	1.00000000	٠
057	165	. ~	2.969697	1.20681117	1.00000000	5.00000000
V31	165	-	3,45454545	1.11778606	1.00000000	.0000000
V32	164	~		1.18471991	1.00000000	5.00000000
V33	165	,-4	۳.	1.18782939	1.00000000	•
V34	165	_	7	1.14950422	1.00000000	3.00000000
V35	165	~ .	2.575758	1.25984666	7.0000000	
V36	165	~ •	3.15/5/5/6	1.1/663546	1.000000	5 00000000
m (991	> C	3.03421007	1.16/0611	1.0000000	0000000
×38	991	> C	1144	1.0352423	1,00000000	5.00000000
727	994	.	2 57228916	1.09719347	1,0000000	•
V41	166	•	3.23493976	1.11147554	1.00000000	.0000000
V42	165	-	•		1.00000000	5.00000000
V43	166	0	. 78915	1.01390479	1.00000000	•
777	166	0	7		1.00000000	. 00000000.
V45	165	~	4909090	1.03368971	1.00000000	000000.
V46	166	0	2.52409639	1.09932104	1.0000000	5.0000000
747	165	- '	. 2121212		1.0000000	٠
0 7 /1	791	~ -		0.1201053	1.00000000	5.00000000
692	097	~			1	
050	190	• ~	2.58787879	1.11523747	1.00000000	0
704	;	1				

Table C.2--continued

VARIABLE	3	N MISSING	KEYN	STANDARD DEVIATION	MINIMUM	MAXIMUM VALUE
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		SITENAME=SM			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
6316	371	-	8181818	٦,	.00000	.00000
767	9	•	23636	Ξ.	8	5.00000000
450	9	-	.8060606	٦.	.00000	.00000
755	•	~	.4121212	•	.00000	. 00000
V56	9	~	3212121	٦.		
V57	•	, p.	.1151515	•		
V58	9	~	. 6363636	•		
V59	•	. →,	. 2060606	Ξ.		
090	•	~ •	15/5/5/.	;		
V61	9	-	5757575			
762	•	~ ~	6617166.			000000
V63	۰ م		71717.			00000
797	0 4	→ -	. 8000000.		00000	.00000
50X:	9 4	٠.	1202021		000000	.00000
992	9 4	• •	5337423		.00000	.00000
707	9 4	•	1801681		. 00000	.00000
902	9 4	·	1963190		.00000	.00000
	ď	•	8527607		. 000000	. 00000
	9) (P)	7975460	٦.	.00000	00000
7/2	9	. (*)	1595092	¬.	.00000	00000
	•		.6932515	•	00000.	00000
7/2	•	· (**)	.5153374	٦.	00000	.00000
V75	9	~	. 5398773	•	.000000	. 00000
V76	9	m ·	.3680981	•	.00000	
717	9	~	. 4049079	•		
V78	ø,	, pop	7026066.	•		
677	ب ھ	7 0	.0/40400. 2/26590	. `	00000	000000
780	0 4	n •	0802469	•	.00000	.00000
TRA	9 4	• ~	3435582	: -,	.00000	.00000
707	S G	•	0000000	•	.00000	000000
787	9	· 673	.4110429	•	00000	000000
V85	9	m	.6073619	•	. 000000	.000000
V86	9	m	.6687116	•		
V87	•	- P	0030660	•		00000
V88	9	C.	0000000. 60000000	• -		00000
687	9	~ ~	8036808		00000	.00000
062	9 4	•	4110429		.00000	.00000
167	3 4	, (~1	7975460		.00000	.00000
	9	•	.8209876	٦.	.00000	00000
760	•	.	.2331188	•	.00000	.00000
262	9	~	.7300613	•	.00000	.00000
960	9	7	. 3024691	•	. 00000	
767	9	♥ (.0493827	∹`		
867	9	⊶.	. 2666666	-∵		
60A	9					000000
V100	9 4	-1 ,-		•	00000	00000
V101	162	1 6	2.432926B3	1.17818149	.00000	.00000
70 1 0	•	•				

Table C.2--continued

VALÚE		.5.00000000
VALUE		1.000000000
Standard Deviation	100 # 10	.839270
MEAN	1. 1200000000000000000000000000000000000	•
MISSING		•
2	00000000000000000000000000000000000000	154
VARIABLE	VVI 22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	V157

Table C.2--continued

VARIABLE	2	N MISSING	HEAN	STANDARD DEVIATION	MINIMUM	MAXIMIN
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	;		SITENAME=8M	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	97.	,	2 48427673	1.06054289	1.0000000	€.00000000
9672	667	- «	3.82500000	0.87989422	1.00000000	9.0000000
6128	091) (3.27044025	1.39022598	1.00000000	6.0000000
0014	191	٠ ي	4.38509317	1.09008031	1.00000000	6.0000000
1914	191	'n	3.38509317	1.36958986	1.00000000	5.00000000
7014	191	n w	1.44720497	0.90069849	1.00000000	€.00000000
6176	797	, -	1.93589744	0.24572440	1.00000000	2.00000000
5074	16.2	- t	2.73202614	1.12394123	1.00000000	₹.00000000
997	163	71	4.30263158	1.12785017	1.00000000	7.00000000
7077	100	9 pm 9 pm	3.15483871	1.13470595	1.00000000	6.00000000
9912	15.1	12	1,39610390	0.49068221	1.0000000	2.00000000
2010	151) (M	1.96732026	0.50547399	1.00000000	3.00000000
277	146	000	1.91780822	0.27560214	1.00000000	2.00000000
1112	151	20	6.22727273	1.80964275	2.00000000	11.00000000
2/1/2	162	7	2.95679012	1.29666924	1.00000000	5.00000000
277	162	•	2.91358025	1.20245640	1.00000000	5.00000000
V175	162	•	3.36419753	1.18351079	1.00000000	5.00000000

Table C.2--continued

N MINIMUM MAXIMUM VALUE		0	•				0 1.0000000	0	•	0	0	50 1.00000000	00000001 0
STANDARD		0.466668	0.4713862	0.3161049	0.3510189	0.501550	0.30827108	0.409419	0.242111	0.5007756	0.2179805	0.2304465	DOBARAGO
MEAN	SITENAME-SM	0.31677019	0.67080745	0.11180124	0.14285714	0.50310559	0.10559006	0.21118012	0.06211180	0.52795031	0.04968944	0.05590062	0.1001.0
N MISSING		•	· srī	·	· vn	·	, vo	•	ı vo) v) vn	•	
Ż	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	161	161	191	161	191	161	161	161	191	191	161	
VARIABLE	1 1 1	(NSA)	ESN2	200	PNS C	5250	928	P.S.V.7	e No	0780	0178	RSKII	CLNOC

Table C.2--continued

	142173999999999999999999999999999999999999	2322681 03322681 1064529561 107025275 107025275 107025275 107025275 107025275 10702525 107025	1. 000000000000000000000000000000000000	5.000000000000000000000000000000000000
	043479 043956825 19256825 19256825 19256825 19256825 19256825 19256825 19256825 19256825 19256825 1925682 192682 1926	1945 1945 1945 1946		
	66956522 173391304 132603304 132603304 132603304 132603300 132617320 132603609 136603609 136603609 136603 136603 1	1922 1922 1922 1922 1922 1922 1939		
પહોં એ જે જે	7.591.304 31.391.304 31.391.304 31.391.304 31.391.304 31.391.391 31.391.39 32.21.391.39 32.21.391.39 32.21.391.39 33.33.33.39	00000000000000000000000000000000000000		
ૡૺ <i>૱ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ૽ઌ</i> ઌૺઌ૽ઌ૽	34826083 13 13 13 13 13 13 13 13 13 13 13 13 13	78242 708642 708666 0939672 1012129 1012129 231122 231229 63129 631131 641131 641131		
୕ ୷୴୴୴୴୴୴୴୴୴୴୴୴୴୴୴୴୴୷୴୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷	31304348 83478261 824782609 82608696 14782609 14782609 14782609 14739130 12739	7086 7086 7089 7089 7089 7089 7089 7089 8089 8089		
	2521/2020 2521/2020 26086696 26086696 261086696 2610887 26107391 2610887 2610887 2610887 2610887 2610888 261088 2610888 2610888 2610888 2610888 2610888 2610888 261088 261088 261088 261088 2610888 26	00121000000000000000000000000000000000		
	347826699 6086956096 6086956095 10482608698 14748260833 147482609 139513099 139513099 139513099 139513099 139513099 139513099 139513099 139513099 1395130 1395130 1395	012129 1095129 1095129 1753502 1753502 175350 17726 17		
ଳ ଳ ଳ ଳ ଳ ଲା ଲ ଲ ଲ ଲ ଲ ଲ ଲ ଲ ଲ ଲ ଲ ଲ ଲ ଲ	025008 00608695 006956695 147026693 147026693 147026693 14702699 1770299 1770299 177029 177029 177029 177029 177029 177029 177029 177029 177029 17702	109502 109502 1730502 1730534 17310534 1731057 173506 1731057 1731057 1731057 1731057 1731057 1731057 1731057		
୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩ ୩	00095655 64266087 147826087 747826083 747826083 74782609 1395130433 70434783 7085955 7105263 713043478 71305088 71305088 71305088	8520 9096 9096 9096 9096 9096 9096 9096 90		
୨. ୩. ୩. ୩. ୩. ୩. ୩. ୩. ୩. ୩. ୩. ୩. ୩. ୩.	70/48/40 70/48/	241131 271131 2711334 909616 8269616 871268 704506 641131 641131		
	747024 768695609 74739130 74739130 74739130 74739130 74739130 74739130 747391 7	01000000000000000000000000000000000000		
ଳ ରାଜ୍ଞ ନ ରାଜ୍ଞ ନ ରାଜ୍ଞ ରାଜ୍ଞ ରାଜ୍ଞ ନ	66695652 74782609 74782609 13951304330 13951304330 1395130435 1105263	909616 826979 858284 351087 837968 837960 6219873 641131	000000000000000000000000000000000000000	
લે જ જ જે જ	74782609 41739130 39513739130 104347391 11 70434783 11 73043478 10 64035088 11 7304348 11 7304348 11 7304348 11	826979 858284 871288 8371288 637960 621873 641131 694452		
	41739130 2521739130 25217391 204347435 11 42105263 11 66086957 66035088 11 64035088 11 64035088 11 64035088	858254 351087 351087 704506 223873 641131		
	29130435 20130435 20130435 2013043478 2013043478 252173991 241304391 271304348 11304348	677248 677248 704506 641131 69452		
	70434783 80869565 62105263 173043478 86086957 64035088 17304348 17304348	637960 704506 223873 694151	.0000000.	000000000000000000000000000000000000000
	80869565 0 42105263 1 73043478 1 86086957 0 55217391 1 64035088 1	704506 223873 641131 694452		000000000000000000000000000000000000000
	42105263 1 73043478 1 86086957 0 25217391 1 64035088 1	223873 641131 694452	.0000000	0000000
	7304348 1 64035088 1 71304348 1	694452	,,,,,,,,,	.0000000
~~~~	25217391 1 64035088 1 71304348 1	01000	.0000000	
~ ~ ~ ~ ~	64035088 1 71304348 1	60066	.0000000	.0000000
m (4) m	71304348 1	014288	0000000.	0000000
* m		500690		
	50434783 50434783	14/301		0000000
٠. ۳	6666667 0	903258	.0000000	. 0000000
.e	42105263 1	994376	.0000000	. 0000000
7	30434783 1	929976	. 0000000	0000000.
m	20175439	406946	. 0000000	
m c	36842105 1	720215		
2 6	40930366 00869566	418385		0000000
	64347826	167670	0000000	.0000000
4	17391304 0	862367	.0000000	.0000000
m	73913043 1	487979	.0000000	.0000000
7	24347826 0	615955	.0000000	. 0000000
2	33913043 0	409511	.0000000	. 0000000
m	04347826 1	457487	. 0000000	
7	356521/4 I	5/2316		
7 6	720126.13	92.13	0000000	0000000
~	42982456	41449	0000000	.0000000
5.	46086957	022671	. 0000000	.0000000

Table C.2--continued

		SITENAME-WR			
	0	3.61739130	1.11278542	1.00000000	5.00000000
115	0	4.17391304	0.59619951	1.0000000	
	•		1.19131103	1.00000000	5.00000000
4 -	• ~		1.02097244	1.00000000	5.00000000
-	0	2.73043478	1.15714212	000000	5.00000000
_	0		0.92774835	1.0000000	2000000
<b>—</b>	<b>~</b>		1.19018916		2000000
<b>~</b>	٥.		1.1404/903	•	2000000
	<		1.16160.1		000000
<b>—</b> .	<b>3</b> (		0 92205786	•	0000000
	<b>&gt;</b> C		1,12539509	000000	0000000
	<b>,</b>		0.99306710	1.00000000	5.00000000
	• •		1.12492054	•	
	0		0.91658172	1.00000000	5.00000000
			0.97984660	1.00000000	000000
	0		1.03611373	1.00000000	0000000
	0		1.01791729	1.00000000	
	0		1.03279556	1.00000000	20000000
	0	•	0.65333738	7.0000000	
	0	•	0.88912405	7.0000000	
	0	•	0.302/06.0	000000	
	9 6	•	1 02053664	00000000	0000000
	•	•	0.98020064		0000000
	•		1.00053380		0000000
		. ` .	0.93438428		2.00000000
	0	•	0.67334564	1.00000000	0000000
	0	• •	1.09272611	1.00000000	0000000
	0	٠;	0.87946312	1.00000000	5.00000000
	0	•	1.10969653	1.0000000	20000000
	0	•	1.11921221		
	9		0.04/64030	0000000	0000000
	<b>&gt;</b> c	•	1 07725657	0000000	000000
112	> <		1.02023763		0000000
115	•		0.76258823		5.00000000
115	•		0.83314262		5.00000000
115	0		0.88439303	1.00000000	0000000
115	0	.4956521	0.99449284	1.00000000	5.0000000
115	0		0.99372555	1.00000000	5.00000000
115	0		1.08333187	1.00000000	5.00000000
115	0	. 6608695	0.99018833	1.00000000	3.0000000
115	0	. 5565217	V0100/4.0	1.0000000	
115	0 (	9304347	1 03473033	T.000000	
115	<b>&gt;</b> c	3.01/39130	1.03434336	00000000	00000000
112	<b>-</b>	5178617	0.87441819		5.00000000
777	•	2434782	1 14394903		0000000

Table C.2--continued

MAXIMIM	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.000000	0	000000	. 00000	. 000000	.000000	. 00000	. 00000						000000	.0000000	0000000	.000000	.0000000	.0000000	.0000000	.0000000	.000000	. 0000000			90	000000	. 000000	.000000	•	.000000	.000000		0000000	.000000	.0000000	.0000000	. 0000000	.0000000			0000000	.0000000	.0000000	0000000	38	
MINIMUM		1.00000000	.0000	.0000	0000	0000	.000	. 0000	.0000	.0000	0000	3000	900			0000	0000	0000	.0000	.0000	.0000	.000	0000	0000.	•	0000.				.000	.000	000	.000.	1.0000000	000	0000	.000	.000	000	000.				.00000	.0000000	. 0000000	3.00000000	
STANDARD DEVIATION		0.92081614																																													1.9020424/ 2.72068547	
MEAN	SITENAPE=WR	634782	3.14782609												4.31430000	4 2046 4286	4.23404460	4.31858407	4 . 41 592920	4.23893805	4.26548673																							72727			2.50476190 9.12612613	
N MISSING		c	• •	0	0	~	<b>~</b>	-	<b>→</b>	m	m	~	m (	<b>~</b>	c.	<b>.</b>	<b>,</b>	• ~	• ~	. ~	7	8	0	-	-4	<b>,</b>	<b>4</b> ,	<b>⊸</b>	<b>-</b>	<b>-</b>	•	~		~ -	<b>-</b>	•	-		7	<b>~</b> 4	4 <i>,</i>	⊶ ‹	7 (	'n	84	113	10	
2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-	115	-	_	_	~	_	~	-	~		<b>~</b>	┛,	→.	٠,	٦.	- ب	- ۱	- ۱	-	-	-	~	114	114	114	٠,	C 7 7 7	71.	711	113		113	114	114	114	-	113	~	┛.	┥,	- ا	110	ے ا		105	
VARIABLE	1 1 1 1 1	2000	2010	2010	V106	V107	V108	V109	0110	V114	V115	V116	V117	V118	V119	V120	V121	7777	7177	V125	V126	V127	V128	V129	V130	V131	V132	V133	V134	V135	7170	V138	V1 39	V140	V141	V142	7710	V145	V146	V147	V148	V149	V150	V152 V153	V154	V155	V156	

Table C.2--continued

VARIABLE	2	N MISSING	HEAN	STANDARD DEVIATION	MINIMUM	MAXIMUM VALUE
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	; ; ; ; ; ;	SITENAME=WR	1 1 1		
V) 58	112	•	2.78571429	1.08576847	1.00000000	4.00000000
65(7	112	, en	3.63392857	0.86987144	1.00000000	4.00000000
V160	112	m	3.66964286	1.73147020	1.00000000	00000000.9
V161	112	m	4.87500000	0.99661590	2.00000000	6.0000000
V162	112	m	3.43750000	1.43809966	1.00000000	5.00000000
V163	112	m	1.28571429	0.63570308	1.00000000	4.00000000
V165	112	m	1.97321429	0.16218227	1.00000000	2.00000000
V166	110	·	2.97272727	1.09593989	1.00000000	4.00000000
V167	109	•	4.67889908	1.26110426	1.00000000	7.00000000
V168	106	· o•	3.33018868	1.07545515	1.00000000	000000009
V169	109	φ.	1.31192661	0.46541992	1.00000000	2.00000000
V170	108	-	1.75925926	0.45075991	1.00000000	3.00000000
1717	91	24	1.96703297	0.17953950	1.00000000	2.00000000
V172	110	Ś	5.32727273	1.71934002	2.00000000	10.00000000

Table C.2--continued

3 0.2410/143	
0.27678571 0.08928571 0.08928571 0.04464286 0.55357143 0.0000000000	

Table C.3

MEANS FOR SCALES, NONSUPERVISORS

<b>X 3</b> 1	62555555555555555555555555555555555555	000000000000000000000000000000000000000
PIAX INCH VALUE		wwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwww
MINIMUM VALUE	10000000000000000000000000000000000	1.25000000 1.000000000 1.000000000 1.00000000
STANDARD DEVIATION	0.5262012 0.91262012 0.91262213 0.92662213 0.90611561 1.06648227 0.90611561 0.912690000 0.112690000 0.126900000 0.126900000 0.1269000000000000000000000000000000000000	0.7359703 0.98775130 0.98775130 0.98101332 0.75630052 1.75630052 1.75630052 0.7556604 0.70556604 0.70556604 0.70556604 0.70556604 0.70556604 0.70556604 0.70556604 0.70556604 0.705005673 0.867373 0.8673162 0.8673167
MEAN SITEMANG-OC	2.5018933 2.501889 2.7554688 3.204559 3.204559 3.204559 3.204559 3.204568 2.705108 2.705108 2.705108 2.705108 2.501875887 2.501875887 2.501875887 2.501875887	2971939 2971939 2971939 2706266 2716350 2716350 2716350 2716350 2716350 2716350 2716350 2716350 2716350 2716350 2716350 2716350 2716350
n Missing		
2		
VARIABLE	PHO2 PHO3B PHO3B PHO64 PHO66 PHO66 PHO7 PHO9 PHO9 PHO9 PHO9 PHO9 PHO9 PHO9 PHO9	PM02 PM03B PM03B PM04 PM04 PM06 PM10 PM10 PM11 PM11 PM13 PM13 PM13B PM13B PM13B PM13B PM13B PM13B PM13B PM13B PM13B PM13B

Table C.3--continued

VARIABLE	2	n Missing	MEAN	STANDARD DEVIATION	MINIMEM	MAXIMUM VALUB
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SITENAME=SA			* * * * * * * * * * * * * * * * * * * *
PH02	382	•	3.26243455	0.77633711		5.00000000
PM03B	381		3.65966754	0.86481449	1.0000000	•
	707	• ~	4.37882765	0.70605213		
PM06	379	• 👁	3.28012313	0.86807516		•
PM07	384	•	3.23046875	0.93555880	1.00000000	2.00000000
PMOB	383	ın t	2.55091384	1.05323881		•
PMIO	186 196 196	~ 6	4.2027391 3.48021308	0.85198082	1.00000000	5.00000000
PM12	386	~	3.80440415	0.90737600		5.00000000
PKI	382	•	2.73232984	0.83547215		4.7500000
PHIS	378	ខ្ល	2.76366843	0.73399805		6.6333333 6.0000000000000000000000000000
PM17	303	^ :	2.53524804	0.36979803	•	4.5555556
	7 C	<b>.</b>	2.85639687	1.13730395		5.00000000
PM21R	9 60	<b>.</b> 101	2.92080070	0.83644769	1.00000000	4.6666667
PM23	384	•	2.59505208	1.16220111		2.00000000
PH31B	381	_	3.04811899	1.00423960		2.0000000
PAYDETRM	377	1	. 2926613	1.14859191	•	5.0000000
UNIONSAT	375	m (	.6602666	0.81529164	1.0000000	3000000
ORGINACE	375		3.11224490	0.87314986	.00000	000000
	•	ì	•			
	1 1 1 1 1 1 1 1 1 1 1		SITENAME=SM			
PM02	1223	98	2.98405560	0.78898362	1.00000000	5.00000000
PM03B	1217	76	3.30457409	0.92815473	7.0000000	
PHO	1229	77	2.6102522¢	1.00193889	1.0000000	0000000 S
PHOSE	1230	c ye	7.91042524	0.90917947	00000000	5.0000000
PM07	1223	78	2.94092396	0.92399114	1.00000000	5.00000000
PMO8	1229	22	3.05736371	1.10252370	1.00000000	5.0000000
PM10	1237	7	4.03839935	0.81874827	1.0000000	5.0000000
PH11	1225	92	2.94312925	1.03028497	000000.T	5.000000 5.000000
PM12	1235	27	2.55505341	0.79701149	1.0000000	5.00000000
PM15	1210	3	2.29187328	0.66670325	1.0000000	4.66666667
PH17	1227	24	2.36471068	0.89635931	1.00000000	2.00000000
PM18D	1194	57	2.22268751	0.69046483	1.0000000	4.5555556
PM19	1231	200	2.45410236	1.11079580	1.00000000	5.0000000 5.00000000
PM21B	1229	7.7	2.58/2/903	1.04011286	•	5.00000000
FR43	1228	22	2.55021716	0.95791784	.0000000	5.00000000
PAYDETRM	1236	15	2.81040992	1.23231101	000000	5.00000000
UNIONSAT	1205	9:	2.39402490	0.79229941		3.000000 3.0000000 3.00000000
SUPVINIT	1202 1219	32	2.76643619	0.89520382	1.0000000	5.00000000

Table C.3--continued

VARIABLE	*	N MISSING	HEAN	STANDARD	MINIMIN	MAXIMUM
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			SITENAME=WR	*	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
P#02	336	ø	3.17465119	0.72284676	1.00000000	5.00000000
PM03B	336	<b>'</b>	3.31051587	0.91340226	1.0000000	5.0000000
P404	337	<b>~</b> 6	2.88427300 4.45080321	0.94489015	1.00000000	5.00000000
PROSE	766		3.17415170	0.87098746	1.0000000	5.00000000
	334		3.11377246		1.0000000	4.75000000
	333	•	2.82882883	1.06029554	1.00000000	2.00000000
DING	332	•	4.09262048	0.79074026	1.25000000	5.0000000
PMII	335	•	3.22288557	0.93612018	1.00000000	2.00000000
PM12	340	-	3.42647059	1.02283913	1.00000000	5.0000000
FINA	335	•	2.67313433	0.79685611	1.00000000	4.75000000
PMIS	332	•	2.49899598	0.65472615	1.00000000	4.3333333
Pari 7	338	<b>m</b>	2.19970414	•	1.00000000	5.0000000
PRIBO	330	11	2.21346801	0.67926715	1.00000000	1.111111
PATS	336	w	2.56845238	1.11893552	1.00000000	2.00000000
PM218	336	m	2.87278107	0.78892897	1.00000000	2.0000000
PM23	338	m	2.01331361	0.99283799	1.00000000	2.00000000
PKSIB	333	•	2.9099091	0.97211380	1.00000000	2.00000000
PAYDETEM	334	-	2.66367265	1.19628123	3.00000000	2.00000000
UNICHSAT	330	11	2.55878788	0.81266479	1.00000000	2.0000000
ORGINVOL	326	15	3.73926380	0.52824430	1.45454545	2.00000000
BUPVNUNT	334	1	2.94653550	0.83850093	1.00000000	4.57142857

able C.4

MEANS FOR SCALES, SUPERVISORS

VARIABLE	3	N MISSING	ИВАН	STANDARD DEVIATION	MINIMUM	MAXIMUM VALUE
***************************************			SITEMANG=OC			
PM02	102	~	•	•	•	•
PM0 3B	100	•	3.80740741	0.64964829	. 3333333	5.00000000
P#04	181	~	•	•	•	
PMOSB	182	~	•		1.00000000	•
PM06	177	-	•	۲.	•	•
PM07	162	~	3.63598901	0.71225179	•	•
PM09	102	~	_	•	1.00000000	•
PM10	181	~	4.19337017		•	•
PHII	102	~	3.94871795		•	.0000000
PM12	101	•	4.07065217			.0000000
PM14	100	-	3.28472222		•	•
PM15	178	•	2.97940075	.7486418	•	99999999.
PM17	182	~	•	0.88355822	•	.0000000
PM18D	101	~	•	0.73323391		•
PM19	191	m	3.26243094	.0508846	.0000000	.0000000
PM21B	102	~	3.67216117		•	5.00000000
PM2 3	183	_	•	.0186146	9	•
PM26	178	•	•	.6901263	.000000	4.25000000
PH27	179	··	.601955	.7019121	•	4.50000000
PM28D	178	•	2.88764045	.7495113		4.80000000
PM30	178	•	3.02808989	.6123011	ŗ	. 5000000
PM31B	162	~	3.48534799	.8384368	•	
PAYDETRA	182	~	•		٩.	•
UNIONSAT	177	-	2.58192090	.7670121	.0000000	Ō
ORGINVOL	178	•	4.08937692	.3759440	060606	00000
SUPVICET	111	7	3.52865214	0.78624023	1.42857143	2.00000000

Table C.4--continued

VARIABLE	3	n Missing	HEAN	STANDARD DEVIATION	MINIMEM	MAXIMEN
•			BITENAME-00	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
P#02	150	~	3.70166667	0.72335016	1.25000000	.0000000
Pet03m	150	~	3.8844444	0.68431524		5.0000000
PHOA	150	~	•	٠.	1.00000000	
PHOSB	147	S	4.27891156	•	•	5.00000000
PHO6	140	•	•	٠.	•	
PH607	151	~	•	٦.	.0000000	0000000.
PHOS	150	~	2.50333333	٦.	.0000000	.0000000
P410	146	•	•	₹		. 0000000
PHILI	150	~			. 3333333	0000000
PHC1 2	151	-			.0000000	•
PM1.4	149	~			. 5000000	.0000000
PM15	140	•		0.74605029		4.6666667
PH17	150	~	2.3833333	0.80355057	. 0000000	.0000000
PHIBD	150	~		0.70162540		ההההה.
PM19	150	~		1.13573243		.0000000
PM21B	150	~				.0000000
PH23	151	~		٦	.0000000	5.0000000
PM26	147	S			.0000000	.000000
PN27	117	<b>•</b>		₹	.0000000	2.00000000
PM28D	117	S	. 70884	٦.	. 2000000	-
PM30	147	s		5	.2500000	5.00000000
PM31B	150	~	. 3800000	₹	1.3333333	2.0000000
PAYDETRM	146	-	۳.	₹	.000000	2.00000000
UNIONSAT	148	<b>-</b>	٦.	0.80689595	.000000	4.40000000
ORGINVOL	140	•	4.06203931	.4404157	2.727273	.0000000
BURNINE	150	~	•	0.82534167	.2857142	5.00000000

Table C.4--continued

VARIABLE	2	N MISSING	MYDA	STANDARD DEVIATION	MINIMEM	MAXIMEM
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		SITINAME-SA			
P102	176	a	3.63494318	0.77729421	1.25000000	5.00000000
P1603B	176	~ (	3.878787	0.76375317	1.0000000	0000000.V
1004	2.5	~ -		0.97360873	2 222223	20000000
	771	- ▼	3.62739464	0.02445551	1.1666667	5.00000000
	176	• ~	3.71448864	0.74148713	1.0000000	2.00000000
	176	) (4	2.36647727	1.11895925	1.00000000	2.00000000
	176	~	4.33664773	0.61465959	2.25000000	5.00000000
	111	-	4.06214689	0.72945231	1.00000000	2.00000000
200	178	•	4.09269663	0.86918530	1.00000000	8.00000000
	111	H	3.19350282	0.78628163	1.00000000	5.00000000
2134	175	m	3.06285714	0.77364493	1.00000000	S.00000000
Pari 7	177	· =	2.83050847	1.01945633	1.00000000	5.00000000
	172	•	2.97803618	0.77973750	1.00000000	5.00000000
	175	M	3.19142857	1.10077596	1.00000000	5.00000000
PM21B	177	e ged	3.64030132	0.81529440	1.00000000	2.00000000
PM23	175	· M	3.11714286	1.19949360	1.0000000	5.00000000
PM26	170	•	2.94264706	0.71077218	1.00000000	5.00000000
PM27	171		2.83479532	0.90755155	1.00000000	2.00000000
Petzen	171	7	3.07836257	0.70872687	1.0000000	4.40000000
PK30	170	•	3.07794118	0.72670338	1.00000000	<b>5.00000000</b>
PM31B	176	co	3.57196970	0.86695799	1.00000000	5.00000000
PATTERN	176	a	3.72537879	1.11370674	1.0000000	5.0000000
TATOROLL I	175	) <b>(</b> 71	2,72228571	0.75773060	1.0000000	4.20000000
CESTWOL	172	•	4.13054968	0.43316525	2.63636364	5.00000000
BUPVACIAT	175	n	3.52653061	0.80679398	1.28571429	2.00000000

Table C.4--continued

VARIABLE	3	N MISSING	MEAN	STANDARD DEVIATION	MINIMUM	MAXIMEN
			SITENAME-SM	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
PM02	162	•	3.29012346	0.83865908	1.25000000	5.00000000
PHO 38	164	~	3.76219512	0.73824830	1.0000000	5.00000000
PMOA	163	•	2.70552147	0.99027690	1.0000000	5.00000000
PROSE	164	~	4.03455285	0.80862672	2.0000000	5.00000000
P#06	160	•	3.34791667	0.83036947	1.0000000	5.00000000
PM07	164	~	3.30792683	0.92286795	1.0000000	5.0000000
PMOR	162	-	2.60493827	1.21255351	1,00000000	5.00000000
PM10	164	~	4.24695122	0.70926591	2.00000000	5.00000000
PM11	162	•	3.62757202	0.91787389	1.0000000	5.00000000
PHOLIZ	165	-	3.72121212	0.98827195	1.0000000	5.00000000
PHIA	161	101	2.98602484	0.78821815	1.0000000	5.0000000
PM15	160	•	2.46666667	0.64773971	1.16666667	4.00000000
PH17	163	~	2.72085890	0.95758531	1.0000000	5.00000000
PHIBD	162	-	2.63648834	0.74273050	1.00000000	4.2222222
PHIS	160	•	3.01250000	1.18288370	1.0000000	5.00000000
PH21B	163	~	3.34355828	0.87756937	1.0000000	5.00000000
PM23	165	-	2.75757576	1.17857663	1.0000000	5.00000000
PM26	157	<b>O</b>	2.44108280	0.75592750	1.0000000	4.50000000
PH27	157	•	2.25000000	0.77418278	1.00000000	€.00000000
PM28D	154	12	2.56103896	0.73139777	1.00000000	4.60000000
PM30	157	•	2.56608280	0.68954540	1.0000000	4.50000000
PM31B	162	•	2.92386831	1.01423593	1.00000000	5.00000000
PAYDETRM	164	~	3.25609756	1.34483666	1.00000000	5.00000000
UNIONISAT	162	~	2.53580247	0.75844048	1.00000000	4.20000000
ORGINAOL	158	•	4.08630610	0.49695578	2.636364	5.00000000
SUPVACUE	164	~	3.26916376	0.61356803	1.14285714	5.00000000

Table C.4--continued

VARIABLE	2	NISSING	MEAN BITENANG=WR	STANDARD DEVIATION	MINIMINA	MAXIMIN
2402 2403 2404	1115	0 11 01	3.60217391 3.74853801 2.98695652	0.75284231 0.67189894 0.93062154	1.00000000 2.00000000 1.00000000	5.00000000 5.00000000000000000000000000
00.00 00.00 00.00 00.00	1115 1115 115	N-00 F	4.300/8488 3.73245614 3.61086957 2.22179913 4.3369103	0.69787514 0.74353301 0.9402856 0.72140565	1.1666667 1.00000000 1.00000000	8
18 <b>7</b> 81		100M+	3.91791101 3.91791101 3.21460177 2.91666667	0.75582323 0.76928548 0.74766546 0.75819028	1.0000000000000000000000000000000000000	5.0000000 5.00000000 4.50000000
PM17 PM16D PM19 PM218	1115 1115 1115 1115 1115 1115 1115 111	9- <b>9</b> -9-9-	2.5260858 2.75243665 3.10000000 3.59420290 2.71735130	0.485544 0.73376452 0.79199529 1.0619628	1.00000000 1.000000000 1.00000000000000	4.33000000 5.00000000 5.00000000
PM26 PM27 PM26D PM31B PMYDETRM UNIONSAT ORGINVOL		488888 4888	2.26125163 2.26125163 2.92382600 2.92382600 3.56167136 2.63654762 3.64264762 3.50751880	0.75196814 0.75181617 0.64437801 0.77803095 1.12851687 0.79123371 0.41873650	11.200000000000000000000000000000000000	4.0000000 4.25000000 5.00000000 4.60000000 5.00000000 6.1128571

Table C.5
RECRESSION RESULTS FOR ALL VARIABLES, ALL EMPLOYEES

0.0027 0.0027 0.0098		PROBY T1 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 00001 000
66.1	23.6 23.6 23.6 23.6 23.6 23.6 23.6 23.6	# RATIO # SQUARE # SQ
3656.2 3545 1.031368 STANDARD	0.157711 0.047767 0.037026 0.032941 0.012981 0.012980 0.012980 0.012980 0.011490 0.0501194 0.0501196	### ### ### ### #### #################
33E DFE MSE PARAMETER	ESTIMATE 3.726185 -0.018969 -0.024623 -0.002249533 -0.0037595 -0.019826 -0.019821 -0.019821 -0.019821 -0.019821 -0.019821	BSR DFE MSE MSE MSE DFE MSE 2.242430 0.1393085 -0.1393147 0.297288 0.109254 0.099147 0.297288 0.009013651 -0.00694572 0.00694572 0.053120 -0.00694572 0.053058 0.053058 0.053058 0.053058
	<b>a</b> AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	
MODEL: MODELO! DEP VAR: VI	VARIABLE SUPERCEPT SACTO SACTO VI 55 W VI 56 W VI 59 W VI 60 W	MODEL: MODELO! DEP VAR: V2 VARIABLE INTERCEPT SUPER SUPER SUPER VISS VISS VISS VISS VISS VISS VISS VIS

Table C.5--continued

	_			
6.51 0.0001 0.0268	PROBY	00000000000000000000000000000000000000	0.0001 0.1218 0.1218 16.55 0.0001	
P RATIO PROBPE R-SQUARE	T BATIO	21.7 -4.18469 -2.6009 -2.6009 -2.18420 -2.28410 -2.3186	. 695 . 695 . 547 	T RATIO 18 8.850 -3.53840 -0.9960 -1.09960 -1.09960 -1.099844 -0.09844 -0.09882
3647.33 3545 1.02666	STANDARD	0.04573 0.04573 0.0123913 0.0123913 0.0123913 0.012056 0.012066 0.012066 0.012066	999 5	ETT. 1
156 170 170	Parameter Estinate	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-0.251006 -0.250334 -0.126136 -0.126156 -0.126156 -0.126156	PARAMETER ESTIMATE 3.512291 0.1580469 -0.1580469 0.106191 -0.046890 0.001277 -0.012277 -0.012277 -0.013838 -0.01462516 -0.01468516
<b>a</b>	2			<u> </u>
MODEL: MODELO1	VARIABLE	INTERCEPT SACTO V155W V156W V156W V156W V159A V165 V165 V165	WHS BNWHS OTH MODEL: MODELO DEP VAR: V4	AAKI TARAH T

Table C.5--continued

17.89 0.0001 0.0704	PROB> [#]	0.00001 0.00001 0.00001 0.00001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001	5.50 0.0001 0.0227	PROB>   T	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
F RATIO PROB>F R-SQUARE	T RATIO	14.8194 7.1789 -6.5937 -0.4109 5.7161 -2.3078 -1.3454 -1.3454 -2.5564 -2.5564 -3.9543 -3.9543 -3.9543 -3.9543	F RATIO PROB>F R-SQUARE	T RATIO	19.8803 1.9703 1.9703 1.0863 -1.7496 -2.7496 -1.8692 -1.5653 -1.5653 -1.4738 -2.3931
4475.008 3545 1.262344	STANDARD	0.055645 0.052445 0.0525380 0.0525380 0.0525380 0.052533 0.055533 0.0556533 0.0556533	5324.826 3545 1.502067	STANDARD ERROR	0.190327 0.057646 0.057646 0.057686 0.056331 0.016530 0.060313 0.060313
338 DFR <b>HSR</b>	Parameter Estimate	2.585570 0.379377 -0.210093 0.02565 -0.050956 -0.050956 0.066148 0.066148 0.066148 0.014238 -0.114238 -0.215054	888 170 188 188	Parameter Estimate	3.783748 0.113579 0.081389 0.087086 -0.087080 0.045020 0.045020 0.02819 -0.096608 -0.096608
107	å	<b>мимимимимими</b>	.01	DF	напанананана
MODEL: MODEL01 DEP VAR: V5	VARIABLE	INTERCEPT SUPER SACTO V152 V155W V157C V159A V169 V169 V169 V172 WHS SHHS OTH	MODEL: MODELO! DEP VAR: V6	VARIABLE	INTERCEPT SUPER SACTO V152 V156 V158 V159 V160 V165 V165

Table C.5--continued

	SS DER	3666.146 3545 1.034174	F RATIO PROBSF R-SQUARE	52.06 0.0001 0.1805
DF ES	Parameter Estimate	STANDARD	T RATIO	PROB>[T]
	3.628617		22.9768	0.0001
	327656		8.8374	0.0001
	04795		-4.9136	0.0001
	60264		-8.0233	0.0001
	65256		1.4183	0.1562
o	54967		-0.0459	0.9634
	37617		-2.4240	0.0154
	99001		-0.2409	0.8096
	31523		2.1397	0.0102
	19784	0.051264	3.5070	0.0005
į				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	336	5155.903	F RATIO	0.0001
	MSE	1.454416	R-SQUARE	0.1121
PARAMETER DF ESTIMATE	ETER VATE	STANDARD ERROR	T RATIO	PROB>   T
1 2.25	3016		12.0300	0.0001
•	5 5 3 7		-4.2380	
	5783		0.9464	•
•	2682		10.6671	
•	5347		-5.2889	
9	1505		-0.0472	•
	6817 4278		-2.5665 2.2625	
	4982		2.9876	
	8650		2.2319	•
1 -0.07	-0.071677	0.013645	-5.2530	0.0001
	1019		-6.2674	
	6227		•	•

Table C.5--continued

HODEL: NO	HODET 01		33E DFR	4		0.0001
DEP VAR: V9			HSE.	1.279111	R-SQUARE	•
VARIABLE		Š	Paracter Estinate	STANDARD ERROR	T RATIO	PROB> [T]
INTERCEPT		٦.	3.56.526	•	970	•
SOPEK SACTO		- ا	-0.187092		537	? 0
152		• ~	-0.020462		900	7
156W		-	-0.116557	•	514	9
157C		<b>~</b>	0.0004555242	•	217	÷.
158		⊣.	-0.0014522	•	000	. c
V159A		٦-	10/05/10-0-	•		פי פ
165		•	-0.00122848		022	•
168		<b>~</b>	-0.011871	•	587	٦.
169		~	-0.079249	•	705	•
172		~	-0.062753	•	20	٠,
<b>3</b>		<b>;-4</b> (	0.163862	•	332	9,
BINHS		<b>~</b>	-0.00620967 -0.066885	0.057012	-0.1440	0.4618
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	-		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		f
HODEL: HO	HODET01		M	2951.564	F RATIO	
DEP VAR: V10	0		NSM NSM	3345 0.832599	R-SQUARE	0.0737
			PARAMETER	STANDARD		
VARIABLE		DE	ESTIMATE	ERROR	T RATIO	PROB>   T
INTERCEPT		-	3.591044		.342	0
SUPER		-	0.294901		. 871	٠,
SACTO		٦,	-0.134671		048	••
V152		٦.	0.014986		177.	•
7631			0.031338		765	: 0
V158		٠,	-0.046147		573	
159A		-	-0.014936		356	•
V160		-	-0.00904152		.833	٦.
165		-			. 169	₩.
168		<b>~</b>	0.081040		.820	9,
691		٦.	-0.027008		07.	• •
V172		<b>-</b>	-0.011770	0.010324	-1.1400	0.2343
		- ۲	0.123440		345	? "
Series Series		٠.	-0.154001		100	٠.
•		)	i			

Table C.5--continued

MODEL: MODEL01 DEP VAR: V11		88 89 M	4311.314 3545 1.216168	F RATIO PROB>F R-SQUARE	18.50 0.0001 0.0726
VARIABLE	ğ	Parameter Estimate	STANDARD ERROR	T RATIO	PROB> [T]
INTERCEPT SUPER SACTO V152 V156		.37262 .37262 .12570 .02980		.015 .126 .126 .080	9995
V157C V158 V159A V160 V168		0.061224 -0.051413 -0.101468 0.107359 0.107358	0.035177 0.021672 0.0301660 0.013118 0.054270	1.7404 -2.3723 -2.0029 2.1542 1.9782 5.1698	0.0819 0.0177 0.0453 0.0313 0.0680
V169 V172 WHS BMHS		.19652 .02812 .01815 .12424 .13973		253	92601
MODEL: MODEL01 DEP VAR: V12		SSE	4857.176 3545 1.370148	F RATIO PROB>F R-SQUARE	8.92 0.0001 0.0364
VARIABLE	ÐĒ	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>  T
INTERCEPT SUPER SACTO V152		2.519364 0.256513 -0.218188 0.009697936	.05505 .04267 .02644	. 859 . 659 . 112	0001
VISON VISON VISON VIGO			.03733 .02300 .05377 .05377	. 997 . 268 . 453	788 788 745
V168 V169 V172 WHS BNHS		-0.00140976 0.011759 0.120012 -0.017100 0.052125 -0.086500	0.057604 0.017862 0.018096 0.013244 0.057834 0.059006	-0.0245 0.6583 2.4953 -1.2912 0.9013 -1.4659 0.4659	0.9805 0.5104 0.1967 0.3675 0.1428 0.6413

Table C.5--continued

MODEL	HODETO1		388	4389.919	F RATIO	23.13 0.0001	
DEP VAR:	V13		MSM	1.238341	R-SQUARE	0.0891	
VARIABLE		à	Parameter Estimate	STANDARD	T RATIO	PROB>[T]	
INTERCEPT	•	<b>~</b>	679	=:	21.2904	0.0001	
SCPER		~-	m :	90	-6.1606 -2508	0.0001	
24CTC			101	6	4.0191	0.0001	
V156W		۰.	111	3	-2.4360	0.0149	
V157C			101	<u> </u>	-5.1096	0.0001	
V158		<b>,</b>	919	5	1509.0	0.364	
V159A		<b>→</b> -	201.0	<u> </u>	1.3304	0.0400	
2912		- ٠	161	0	-2.9449	0.0033	
V168		•	0	0	-2.5943	0.0095	
V169		-	17	9	3.1130	0.0019	
V172		-	.033	9	2.6443	0.0082	
ZH2		4	.051	5	-0.9356	0.3495	
BAHIS		-	. 164	9	2.9235	0.0035	
OF.H		-	6413	8	0.0717	0.9428	
 	, 		1 1 1 1 1 1 1 1 1 1	 			
HODEL:	HODET01		800	5207.563	F RATIO	14.25	
			DFE		PROB>F	0.0001	
DEP VAR:	V14		HSH	1.468988	R-SQUARE	9900.	
			PARAMETER	STANDARD			
VARIABLE		DF	ESTIMATE	ERROR	T RATIO	PROB>  T	
TOROGENI		-	51585	18	679	0.0001	
SUPER		-	36853	.0	197	0.0001	
SACTO		-		ś	.953	0.0001	
V152		-	11388	9	507	0.6121	
AJ SEW		_	33994	2	.068	0.9454	
V157C		<b></b> 4 .	5015	<u> </u>	.297	0.1946	
V158		<b>,</b>	04076	36	117	0.08/0	
V159A		⊣.	98786	į.	?;	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	
V160		<b>-</b>	20050	5 6	120	0.00	
610		٦,	00170	9	216	0.0267	
9910		- •	60770	9	. 885	0.3760	
V172		· ~	0.04878	5	.557	0.0004	
WHS		-	-0.010858	0.059884	-0.1813	0.8561	
BUTHS		~ .		9,8	.292	0.1963	
¥		-	. 1680.	Ŝ	ם ח	P767.0	

Table C.5--continued

21.31 0.0001 0.0827 PROB>[T]	0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.5316 0.0001 0.5558	PROB>   17.65 0.0001 0.0001 0.0001 0.0001 0.189 0.3185 0.013 0.013 0.0019 0.0008 0.0008 0.0008
FROB>F PROB>F R-SQUARE F RATIO	16. 16. 17. 17. 17. 17. 17. 17. 17. 17	FRATIO PROBNE R-SQUARE 17.9592 17.9592 17.1635 17.1635 17.9598 17.9968 17.9968 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976 17.9976
4975.045 3545 1.403398 STANDARD KRROR	0.183969 0.055720 0.043190 0.026761 0.0248533 0.03428 0.054420 0.054420 0.058298 0.013404 0.013404 0.013404 0.059718	4058.017 3545 1.144716 3545 1.144716 0.16151 0.050324 0.034128 0.043851 0.043851 0.043851 0.012727 0.012727 0.012727 0.012727 0.0123934 0.053863
SSE DFE MSE MSE FARANCTER ESTIMATE	3.041051 0.4139981 0.0547229 0.1263564 0.106229 0.010229 0.010229 0.070822 0.197229 0.056089	SSE DEE DEE DEE ESTIMATE 2.983947 0.18213430 0.006317141 0.222201 0.222201 0.222201 0.0237619 0.037619 0.037619 0.037619 0.0177961 0.177961 0.0177961
č	ппппппппппппппппппппппппппппппппппппппп	g dedecedededed
MODEL: MODELO1 DEP VAR: V15 VARIABLE	INTERCEPT SUPER SACTO VISSW VISSW VISSW VISS VISS VISS VISS V	MODEL: MODELO1 DEP VAR: V16 VARIABLE INTERCEPT SUPER SACTO V155 V156 V157 V158 V158 V168 V168 V168 V168 V168 V168 V168 V16

Table C.5--continued

HODEL: HODELO1	10	388	4451.596	F RATIO	18.59
DEP VAR: V17		<b>1831</b>	73	R-SQUARE	6
VARIABLE	å	Parameter Estinate	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT	~		.17402	15.8289	9
SUPER	<b>~</b>	0.049388	0.052708	0.9370	0.3466
MACTO VISS		2 9	02531	9990.0-	976
VISEW	••	0.39977	.04592	•	8
V157C	<b>~</b>	2	.03574	<b>~</b> :	93
V158	<b></b> -	9	.0220.	-1.4979	
V159A	<b>→</b> -	35	01111	1.9290	180
VI65	•	9	.05514	4.7580	8
V168	-	2	.01710	0.2866	774
V169	<b>~</b>	2	.04604	ο.	3
V172	<b>~</b> •	0.02048	.01267	<b>−.</b> .	25
	<b>→</b> -	0.11551 0.35526	00000	2000.7-	<u></u>
OTH O	<b></b>	200	.09004	•	
• • • • • • • • • • • • • • • • • • •		9 9 1 1 1 1 1 1	• • • • • • • • • • • • • • • • • • •	! ; ; ! ! ! !	
MODEL: MODEL01	5	100	9	FRATIO	7
DEP VAR: VIB		NSE SE	1.330228	R-SQUARE	9
		PARAMETER	STANDARD		
VARIABLE	ĐĒ	ESTIMATE	ERROR	T RATIO	PROB>[T]
INTERCEPT	~	. 5059	17910	66.	9
SCPER	⊶,	. 2689	.05424		
SACTO	-4 -	8787.0 004600	10770°	7.	
751A	٠.	0.3049	.04727	6.45	9
V157C	-	.0801	.03679	.17	.029
V158	⊶.	0.0339	.02266	2.	134
V159A V160	<b>→</b> -	0205	01370	1.50	133
V165	•	.0768	.05675	.35	175
V168	~	.0648	.01760	.68	89
V169	<b></b> -	2000	704/39	200	100
7/ TA	<b>-</b>	2300	.05698	4.03	200
BARIS	<b>.</b>	0.144611	0.058140	2.4873	0.0129
H.S	◄	9650.	00760.		ATC:

Table C.5--continued

HODEL: MODELO1	107	200	5542.521	F RATIO	12.64
DEP VAR: V19		HSH	17	R-SQUARE	9
VARIABLE	å	Parameter Estimate	STANDARD	T RATIO	PROB> [T]
	•			,	
INTERCEPT	⊶ ,	2	11861.	1///1	
SUPER	→ -	0.431.09	0.038813	• •	
	٠,	FT - 0		35	
757	<b>→</b> •	֡֓֞֟֓֓֓֓֓֓֟֟֓֓֓֓֟֟	17070.	710.	
A120	→,	3	<b>*71c0</b> .	N/7.	
V157C	<b>,</b>	7	89660.	1.289	
V158	~	2	.02457	9.6.E	
V159A	⊶.	3	.05744	0.615	
V160	<b>~</b> 4 :	Ξ.	.01487	900	
V165	<b>~</b>	3	.06153	. 422	
V168	<b></b>	Ξ:	.01908	2.301	
V169	<b></b>	3	.05137	199.2	
V172	-	2	.01414	.610	
275 275	-	Ζ.	.06178	203	
	-	2	.06303	=======================================	
<b>#</b> 5	-	2	.10047	. 228	
; ; ; ; ; ; ; ; ;					
HODEL: HODEL01	101	100	4605,464	FRATIO	44.48
		2 2	2000	PROBY F	1000.0
DEP VAR: V20			_	R-SQUAKE	•
		PARAMETER	STANDARD		
VARIABLE	30	ESTIMATE	ERROR	T RATIO	PROB>  T
TUPPOCEDE	-	•	17700	579	•
SUPER	• ~	•	.05361	588	
SACTO	-	٠,	.04155	. 293	•
V152	-	õ	.02574	.372	•
M95 [A	-	Ξ.	.04671	.872	•
V157C	-	"	.03635	9.961	•
V158	-	6	.02239	416	•
V159A	~ ·	-0.051861	0.052360	ο,	0.3220
V160	<b>~</b>	٠.	.01355	ָרָי פּיי	•
V165	<b>~</b> •	Ξ,	.05609	1	•
V168	<b></b> ,-	•	66/10.	3.744	•
V109	→	•	20010	251	•
7/1/ 6H3	<b>-</b>		05631	2.421	
BAHS	• ~		.05745	731	
OTH.	-	0.114120	.09159	1.2460	0.2129

Table C.5--continued

HODEL:	MODEL 01		100	5351.395	F RATIO	18.30	
DEED VAR:	V21			1.509561	R-SQUARE	0.0719	
VARIABLE		2	Parameter Estimate	STANDARD	T RATIO	PROB> [T]	
INTERCEPT			.04058	70	15.9359	0.0001	
STOLE		·	32398	9.0	-7.2327	0.0001	
M951A		4	223	0.050356	4.4289	0.0001	
V150		·	0.10060	,0,	-4.1666	0.0001	
V159A V160			.04581	•	3.1347	0.0017	
V165		<b></b> -	.16006	90	2.6473 1.5068	0.0061	
69[7		, , , ,	0.11752		-2.3280	0.000	
Z			.06037		-0.9945	0.3200	
BURHS OFF			1 <b>8</b> 559 17005		-2.9965 1.7224	0.0027	
MODEL	HODET01		14 S	4260.25	F RATIO	17.09	
DEP VAR:	V22		NSE	1.201763	R-SQUARE	0.0674	
VARIABLE		<b>9</b> 0	PARA! TER ESTIMATE	STANDARD ERROR	T RATIO	PROB>   T	
INTERCEPT	e.,	٦.	.27378			•	
SACTO			34047				
V152		<b></b>	.02500 .41238				
V157C			022772			•	
V159A		٠.,	0.028733	0.050359	0.5706	0.5683	
V160 V165		<b></b>	.15641		9		
V168		<b></b> -	.08811			• •	
V172			.02070				
SH3		<b></b> -	.02733				
OTH.			.13587				

Table C.5--continued

HODEL: HODELO?		388	4651,746	FRATIO PROB>F	19.55
DEP VAR: V23		HSM.	1.312199	R-SQUARE	0.0764
VARIABLE	<u>a</u>	Parameter Estinate	STANDARD ERROR	T RATIO	PROB>[T]
INTERCEPT	~	3.189550	0.177891	17.9298	0.0001
SACTO		-0.083813	.04176	-2.0068	10.
V152	-4-	-0.058156	0.025877	7	024
V150W	<b>-</b>	0.100567	.03654	2.7523	.005
V158	-	7	.02251	-3.7144	966
V159A		0.00499942	.03262 .01362	1.3665	.171
V165	• •		.05637		.027
V168	<b>~</b> -		01748	-3.1429	
V169	<b>-</b> -	-0.054980	.01296	, •	000
SES.	-	0.081272	.05659	~ (	.151
BMHS	<b></b>	-0.159777	.09205	-2.7669	. 572
					* * * * * * * * * * * * * * * * * * * *
MODEL: MODELO3	-	188	5122.188	F RATIO	31.00
DEP VAR: V24		NSK NSK	1.444905	R-SQUARE	,
		PARAMETER	STANDARD		
VARIABLE	O.	ESTIMATE	ERROR	T RATIO	PROB> [T]
INTERCEPT		.72881	18667	14.6184	•
SUPER		67490	.05653	11.9371	•
SACTO	<b>-</b>	22/03	02715	-6.8367	
75TA		0.20075	.04926	4.0749	
V157C		.18753	.03834	4.8911	•
V158	<b></b> -	. II680 15428	.05521	-2.7941	
7 1 2 4 V 1 5 V V 1 5 V V V V V V V V V V V V V	<b>→</b>	0.01664	.01429	1.1643	
V165	-	.04696	.05915	0.7939	-
V168	<b>~</b> •	0.01004	.01834	-0.54/5	
V169	<b>→</b> ←	69980	.01360	-6.3746	
WHS	, 🛶 ,	0.24242	.05939	4.0818	0.0001
BNR S		59.	0.096593	0.0062	

Table C.5--continued

Manager - Landon (1)	5		3957.351	F RATIO	11.43	
HUNEL HOUSE	<b>.</b>	Mo	3545	PROB>F	0.0001	
DEP VAR: V25		<b>MSM</b>	1.116319	R-SQUARE	0.0461	
VARIABLE	à	Parameter Estinate	STANDARD	T RATIO	PROB>[T]	
INTERCEPT	<b>~</b> ,	3.642357	0.164078	22.1990	0.0001	
SACTO	<b></b>	-0.115578	0.03850	-3.0004	0.0027	
V152	<b></b> 1	0.058566	0.023867	1.2890	0.1975	
V157C	4 ,-4 ,	0.109132	0.033702	3.2381	0.0012	
V159A		-0.096051	0.048536	-1.9790	0.0479	
0910		0.019790	0.012568 0.051995	1.5747	0.0727	
V168	• •	0.005254573	0.016123	0.3259	0.7445	
V169 V172	<b></b>	-0.025004	0.011954	-2.0916	0.0365	
SEES		0.154288	0.052203	2.9555 -2.5244	0.0031	
	•	-0.029780	0.084903	-0.3506	0.7258	

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HODEL: HODELO1 DEP VAR: V26		SSE DPE NSR	4993.169 3518 1.419320	F RATIO PROB>F R-SQUARE	17.11 0.0001 0.0680	
VARIABLE	à	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T	
INTERCEPT SUPER			.05624	22.3557 -0.6867	0.0001	
V152 V156W			02701	-0.3510 2.0067	0.7256	
V150 V150 V159A		0.095818 -0.046657 -0.045076	0.023502	4.0770 -0.8493 -3.1687	0.0001	
V165 V165 V166			05885	-0.3835	0.0014	
V172 V172 WHS		0.02604	01353	1.9248	000	
BNHS OTH		0.270030 -0.098530	.09609		0.0001	
13		#86 #86 #86 #86	73	F RATIO PROB>F	32.06	
DEP VAR: V27	ě	PARAMETER POSTINATE	; Ē.	N-SQUAKE	5051.0	
INTERCEPT	; -	3.002169		•	0.0001	
SUPER		0.498424		9.0993		
V152 V156W	<b></b>	-0.068633		5.1624		
V15/C V158 V159A		-0.167251	0.022886	4.6834 -7.3080 -1.6923	0.0001	
V160 V165		-0.00978726 0.075589		-0.7065 1.3189		
V168 V169		-0.032662 -0.049838		-1.8379 -1.0415		
V172 WHS	, , , , , , , , , , , , , , , , , , ,	-0.062940 0.316070		-4.7768 5.4931		
BNHS OTH		-0.019982 0.115202		-0.3404 1.2310		

Table C.5--continued

19.77 0.0001 0.0777	PROB> [T]		<i></i> .	000000000000000000000000000000000000000	19.15 0.0001 0.0755	PROB>   T	0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001
F RATIO PROB>F R-SQUARE	T RATIO	22.1247 8.6321 -6.7475 -0.7683		1.9700 0.0053 -2.0938 -3.8883 6.1794 5.6073 1.4760	F RATIO PROB>F R-SQUARE	T RATIO	13.1614 3.5280 -7.1289 -0.2309 -0.9571 -0.0305 -0.0305 -0.0305 -0.0305 -0.0305 -0.0305 -0.0305 -0.0305 -0.0305 -0.0305 -0.0305
4054.066 3518 1.152378	STANDARD ERROR			0.053029 0.016444 0.012192 0.053321 0.065321	3313.76 3518 0.941944	STANDARD ERROR	0.151294 0.0458224 0.035194 0.0319929 0.0191076 0.011589 0.011667 0.011023 0.048136 0.048136
252 273 167	Parameter Estimate	3.702401 0.437513 -0.265088	-0.0218974 -0.0218974 -0.012890 -0.040586 -0.030928	0.104469 -0.092406 -0.092406 0.329002 0.329002 0.127809	800 870 800 800 800	Parameter Estimate	1.991236 0.161666 -0.253214 -0.00508098 0.188510 0.18425 -0.138630 -0.018660 -0.018660 -0.04763 0.067763 0.067163 0.067163
	Ď					DF	пенесенененене
MODEL: MODELO1 DEP VAR: V28	VARIABLE	INTERCEPT SUPER SACTO	V156 V156 V159 V159A V160	V165 V169 V172 WHS BNHS OTH	HODEL: HODELO1 DEP VAR: V29	VARIABLE	INTERCEPT SUPER SACTO V152 V1564 V1564 V1594 V159 V165 V169 V172 WHS BNHS

Table C.5--continued

HODEL:	HODET 01		382	4043.538 3518	F RATIO PROB>F	19.79
DEP VAR:	V30		200	1.149386	R-SQUARE	•
VARIABLE		ā	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT		<b>~</b>	2.907219	0.167125	17.3955	0.0001
SUPER		-4 -	-0.106817	0.030236	;;	
346.10		- ٠	• •	0.024311		•
V1 S6W				0.044107	۲.	•
V157C			•	0.034328	7,	٠
V158		-1	•	0.021149	7	•
V159A		<b>~</b> .	•	0.049437	٠,	•
V160		٦.	j٠	108710.0	-	•
V165		⊶.	•	0.03530	:-	•
Vies		٦.	•	0.0160.0		•
V169		٠,	•	0.012176		
7/1/2		٠,	•	0.053173	•	
		<b>-</b> , -	•	0.54250	•	•
		<b>-</b>		0.086479	۳.	
			•	* * * * * * * * * * * * * * * * * * * *		
MODEL	MODETO1		200	5243.683	F RATIO	10.10
			DFE		PROB>F	35
DEP VAR:	V31		HSM.	1.490587	K-SQUAKE	5
			PARAMETER	STANDARD		•
VARIABLE		DE	ESTIMATE	ERROR	T RATIO	PROB>   T
TUTPROTECT		-	3.724722	.19	.570	.000
SUPER			0.309452	.05	.368	8
SACTO		-	-0.222986	9	4.990	8
V152			-0.018202	.0	.657	510
W156W		_	0.192153	.0	3.825	90.
V157C		-	-0.017677	5	707.0	400
V158		<b>~</b>	-0.069521	20.	ממני ז	
V159A		<b>,,</b>	-0.097368	5.5	760	
V160		<b>-</b>	-0.023214		2.079	037
7100		<b>-</b>	030690	5	641	1001
69[A		•	-0.126500	0.	.512	.012
V172		· ~	-0.040973	9	.954	.003
WHS		-	0.023158	0.060553	0.3824	0.7022
BNHS		<b>~</b> ·	0.014037	9	727.	766
E E		-	-0.029399	5	. 470	

Table C.5--continued

HODEL:	HODET 01		386	4248.687	F RATIO	22.85	
DEP VARI	V32		MSM	1.207700	R-SQUARE	•	
VARIABLE		DF	Parameter Estimate	STANDARD	T RATIO	PROB>   T	
INTERCEPT	<b>1</b> 4	-	2.425694	17131	14.1595	0.0001	
SCPER		<b></b>	0.164504	0.040219	-7.1541		
V) 52		•	-0.067263	.02492	2.699	•	
V156W		-	-0.031032	.04521	.686	•	
V157C		-	0.202110	.03518	5.743	•	
V158		⊶,	0.001940	79170.	֭֭֚֚֚֚֚֚֚֓֝֝֡֜֜֝֝֜֝֟֝֝֡֟֝֝֡֡֡֝֩֡֡֝֡֩֝֡֡֡֡֝֩֡֡֡֡֡֝֩֡֡֡֡֡֡֡֡֡֡	•	
V159A		٦.	0.011650	01312	0.887		
2917		•	0.250542	.05428	.615	•	
V168		-	0.090357	.01683	. 367	•	
V169		-	-0.066891	.04532	1.475	•	
V172		→	-0.084083	.01248	25.	•	
SES		<b>-</b>	0.116546	.05450	1.15E	•	
		<b></b>	-0.122/62	08864	.073		
	;	. !					
MODEL	MODEL01		M S S	4795.707	F RATIO	39.03	
DEP VAR	V33		NSK	1.363191	R-SQUARE	0.1427	
VARIABLE		DF	Parameter Estimate	STANDARD	T RATIO	PROB>   T	
FOAUGAWNI	ę.	-	2,509257		13.7866		
SUPER		٠,	0.321560		5.8332	•	
SACTO		-	-0.347364		-8.1294	•	
V152		<b></b>	0.030225		1.1416		
V156W		~ ,	0.083802		7 2250	٠	
V157C		۰,	0.270450		5.6971	• •	
VI58		٠,	0.058723		, ,		
V159A		•	, .		1.0481	•	
V165		-	0.215432		3.7352	•	
V168		-	0.132756		,-,	•	
V169		٦,	-0.136042		-2.8250	•	
V172		<b>→</b> -	0.003368	0.013260	3.1086	0.0019	
BNHS		•	-0.202752		-3.4318	•	
OTH.		-	-0.078582		-0.8344	•	

Table C.5--continued

BTANDARD  BIRGR  0.185612 0.065218 0.065218 0.063576 0.063576 0.063576 0.063576 0.0538987 0.0538987 0.0538987 0.0538987 0.0538987 0.0538987 0.0538989 0.0538987 0.0538989 0.0538989 0.0538989 0.0538989 0.0538989 0.0538989 0.05380898 0.0580898 0.058686 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.0586868 0.05868899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899 0.0588899	MODEL	MODEL 01		11 a	4987.604	F RATIO	26.79	
PARAMETER STANDARD T RATIO FR C 12.959116 0.185612 15.9425 16.43625 0.055618 7.8911 7.0.302669 1.0.43625 0.055618 7.8911 7.0.302669 1.0.43625 0.048987 5.6878 1.0.00876681 0.027000 5.3247 5.9458 1.0.00876681 0.027000 5.03489 1.0.30412 0.023489 1.0.30412 1.0.0087681 1.0.0087681 1.0.0087681 1.0.008768 1.0.6634 1.0.008761 1.0.008762 1.0.6834 1.0.008762 1.0.6834 1.0.008762 1.0.6040 1.0.008762 1.0.6040 1.0.008762 1.0.6040 1.0.008762 1.0.6040 1.0.00878 1.0.00878 1.0.00478	VAR	V34		35W		R-SQUARE	0.1025	
1	VARIABLE		DF	Parameter Estimate	STANDARD ERROR		PROB>[T]	
-0.302669	INTERCEP' SUPER	<b>t</b> +		2.959116	0.185612	15.9425		
0.218625 0.048987 5.6878     0.148728 0.038426 3.9010     0.036423 0.033489 -4.4108     0.036423 0.054906 -0.6634     0.036423 0.054819 3.7858     0.034562 0.018239 3.7858     0.034562 0.018239 3.7858     0.034562 0.018233 -4.2166     0.034562 0.013523 -4.2166     0.034562 0.013523 -4.2166     0.034562 0.013523 -4.2166     0.0346291 0.059055 2.00640     0.03462 0.059055 2.00640     0.044715 0.059055 -0.0434     0.054609 0.056068 6.8807     0.0348795 0.043460 -12.3071     0.0348795 0.058662 1.6128     0.0348795 0.058662 1.6128     0.0348795 0.058662 1.6128     0.0348795 0.058662 1.6128     0.0348795 0.058662 1.6128     0.0348795 0.058887 -3.5439     0.0348797 0.034887 -3.5439     0.022559 0.058887 0.05771     0.022559 0.056089 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.058887 0.05771     0.022559 0.050899 0.057789     0.022559 0.050899 0.057789     0.022559 0.050899 0.050897     0.022559 0.050899 0.050897     0.022559 0.050899 0.050897     0.022559 0.050899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0.054860 0.054899     0	SACTO			. 0	0.043576	-6.9458 -0.3247		
1	V156W			0.278625	0.048987	5.6878 3.9010		
1	V158			-0.103603	0.023489	-4.4108 -0.6634		
0.222677 0.058819 3.7858     0.034562 0.0186239 1.8949     0.034562 0.013523 -4.2166     0.0357022 0.013523 -4.2166     0.018473 0.059055 2.00624     0.018473 0.059055 -0.06340     1 -0.036393 0.056045 -0.0634     1 -0.0416991 0.096045 -0.0634     1 -0.044715 0.0185116 16.0953     1 -0.044715 0.018656 -3.0431     1 -0.044715 0.018662 1.6128     1 -0.03446995 0.014179 1.0995     1 -0.03446995 0.014179 1.0995     1 -0.044609 0.014179 1.5285     1 -0.044865 0.014887 -1.5285     1 -0.044865 0.014887 -1.5285     1 -0.044869 0.0034499 0.055489     1 -0.034449 0.065489 0.055480     1 -0.044669 0.0654899 0.055480     1 -0.044669 0.0654899 0.055480     1 -0.044669 0.0654899 0.055480     1 -0.044669 0.0654899 0.055480     1 -0.044669 0.0654899 0.065480     1 -0.044669 0.0654899 0.065480     1 -0.044669 0.0654899 0.065480     1 -0.044669 0.0654899 0.065480     1 -0.044669 0.0654899 0.065480     1 -0.044669 0.0654899 0.065480     1 -0.044669 0.0654899 0.065480     1 -0.044669 0.065480 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.065480     1 -0.064860 0.0654	V159A V160		<b>→</b> ⊶	Ö	0.014217	-0.6831		
-0.133517 0.049110 -2.7187     -0.057022 0.013523 -4.2166     -0.018673 0.060251 -0.6040     -0.018673 0.060251 -0.0434     -0.00416991 0.096045 -0.0434     -0.00416991 0.096045 -0.0434     -0.00416991 0.096045 -0.0434     -0.00416991 0.096045     -0.00416991 0.096045     -0.00416931 0.056068     -0.014148 0.048956 -3.0431     -0.0385788 0.053426 -3.0431     -0.0383896 0.038024     -0.0383896 0.038024     -0.0383896 0.038426     -0.044795 0.023426     -0.044595 0.023426     -0.044595 0.014179     -0.044595 0.014179     -0.044596 0.0188190     -0.044596 0.0188190     -0.044596 0.0188190     -0.044596 0.0188190     -0.044596 0.0188979     -0.044596 0.0188979     -0.0445979 0.060890     -0.022599 0.0528897     -0.022599 0.0558897     -0.022599 0.0558897     -0.022599 0.0558897     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.095789     -0.064860 0.0	V165 V168			0.222677 0.034562	0.058819 0.018239	3.7858 1.8949		
O.118473	V169			-0.133517	0.049110	-2.7187	•	
-0.036393   0.060251   -0.6040     -0.00416991   0.096045   -0.00434     -0.00416991   0.096045   -0.00434     DFE	WHS			0.118473	0.059055	2.0062		
LR: WODELO1  DFE 3518  RATIO  3518  R-SQUARE  1.410170  R-SQUARE  PARAMETER STANDARD  SLE DF ESTIMATE ERROR T RATIO PR  1 0.385788 0.056068 6.6807  1 -0.534862 0.043460 -1.6606  1 -0.044715 0.026928 -1.6006  1 0.083896 0.038024 2.2064  1 0.083896 0.038024 2.2064  1 0.083896 0.018190 1.0995  1 0.09550 0.018190 2.7227  1 0.049526 0.018190 2.7227  1 0.049526 0.018190 2.7227  1 0.022559 0.058897 0.38330  1 0.022559 0.058897 0.5400  1 0.022559 0.0658897 0.6771	BNHB OTH			Ö	0.060251 0.096045	-0.6040		
DFE DFE PROBEF  NASE 1.410170 R-SQUARE  PARAMETER STANDARD T RATIO PR  SLE DF ESTIMATE ERROR T RATIO PR  1 0.385788 0.056068 6.68071 1 -0.534862 0.043460 -12.3071 1 -0.044715 0.026928 -13.7099 1 0.083296 0.038024 2.2064 1 0.083896 0.038024 2.2064 1 0.083896 0.034865 -3.0431 1 0.045590 0.054759 -3.0431 1 0.049526 0.014179 1.0995 1 0.049656 0.014879 -1.5285 1 0.022559 0.058897 0.3830 1 0.022559 0.058897 0.3830 1 0.022559 0.058897 0.3830 1 0.022559 0.058897 0.5400 1 0.054860 0.055789 -0.5771	HODEL	MODETO1		<b>4</b> 000	4960.977		26.79	
PARAMETER STANDARD T RATIO PROE ESTIMATE ERROR T RATIO PROE CONTROL T RA	VAR	V35		DFE		PROB>F R-SQUARE	0.0001	
1 2.979505 0.185116 16.0953 0.056068 6.6807 0.055068 6.6807 0.055068 6.6807 0.055068 0.055068 0.055068 0.055068 0.026928 -12.3071 0.0081248 0.026928 -1.5606 0.038024 0.1301 0.0083895 0.023426 0.1301 0.015590 0.054759 -3.0431 0.015590 0.054759 0.1301 0.04955 0.014179 1.0995 0.014179 1.0995 0.014865 0.018190 2.7227 0.004956 0.013487 -3.5439 0.0032459 0.056897 0.5400 0.5400 0.054860 0.055789 -0.5771 0.0064860 0.095789 -0.5771	VARIABLE		DF	Parameter Estimate	STANDARD ERROR		PROB>[T	
1 -0.534862 0.043460 -12.3071 0.0447185 0.026928 -1.6606 0.0181248 0.048856 -3.7099 0.0181248 0.038024 2.2064 0.0181896 0.038024 2.2064 0.015638 0.053426 0.1301 0.015590 0.014179 1.0995 0.016638 0.014179 1.0995 1.015638 0.014179 1.0995 1.015638 0.014179 1.0995 1.015862 1.015862 1.015862 1.015862 1.015862 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.015865 1.058897 -1.5285 1.015865 1.0058897 1.03830 0.058400 1.058400 1.058400 1.0564860 1.056789 -0.6771 0.056789	INTERCEP	t.	~	2.979505		16.0953	•	
1     -0.044715     0.026928     -1.6606     0.048856       1     -0.181248     0.048856     -3.7099     0.018024       1     0.083896     0.023426     0.1301     0.01301       1     -0.166688     0.054759     -3.0431     0.01810       1     0.094609     0.054759     -3.0431     0.01810       1     0.049526     0.018190     2.7227     0.018190       1     -0.047797     0.018190     -1.5285     0.018190       1     0.022559     0.058897     -3.5439     0.3830       1     0.022559     0.060090     0.5400     0.06771	SOFER			0.363/86 -0.534862		-12.3071		
1 0.003048795 0.023426 2.2064 0.03048795 0.023426 0.1301 0.003048795 0.023426 0.1301 0.0166638 0.054759 -3.0431 0.0094609 0.058662 1.6128 0.014865 0.018190 2.7227 0.013487 -3.5439 0.0032459 0.064860 0.0658897 0.3830 0.0032480 0.064860 0.095789 -0.6771 0.0000000000000000000000000000000000	V152			-0.044715		-1.6606	•	
1 0.003048795 0.023426 0.1331 0.1301 1 0.015598 0.014179 1.0995 0.014179 1.0995 0.014179 1.0995 0.014179 1.0995 0.014179 1.0995 0.014199 1.0995 0.014199 1.0995 0.014199 1.0995 0.014199 1.0995 0.014199 1.0995 0.013487 -1.5285 0.013487 -3.5439 0.013249 0.0568897 0.3830 0.0132480 0.056989 -0.5471 0.000090	V157C					2.2064		
1 0.015590 0.014179 1.0995 0.004609 0.058662 1.6128 0.0049526 0.018190 2.7227 0.018190 2.7227 0.004865 0.048979 -1.5285 0.0022559 0.05887 -3.5439 0.005090 0.3830 0.0054860 0.095789 -0.5771 0.005789 -0.5771 0.005789	V158		<b></b>	٠. ١		0.1301	•	
1 0.094609 0.058662 1.6128 0.018190 2.7227 0.018190 2.7227 0.018190 2.7227 0.018190 2.7227 0.018190 2.7227 0.018190 2.7227 0.018190 2.15285 0.018187 2.35439 0.018187 2.35439 0.018187 0.3830 0.018187 0.38480 0.0181887 0.38400 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.01818880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880 0.0181880	V160		• •	0.015590		1.0995		
1 -0.074865 0.048979 -1.5285 0. 1 -0.047797 0.013487 -3.5439 0. 1 0.022559 0.058897 0.3830 0. 1 0.032449 0.060090 0.5400 0.	V165 V168			0.094609		1.6128		
1 0.02559 0.058997 0.3830 0.000000 0.5400 0.000000 0.5400 0.064860 0.095789 -0.6771 0.000000	V169			-0.074865		-1.5285	•	
1 0.032449 0.060090 0.5400 0. 1 -0.064860 0.095789 -0.6771 0.	VI / Z		<b></b>	0.022559		0.3830		
	BNHS		<b></b>	0.032449 -0.064860		0.5400		

Table C.5--continued

MODEL: MODELO3		100	4250.254	F RATIO	22.29
DEP VAR. V36		4 18 N	1.200145	R-SQUARE	, 0
VARIABLE	ă	Parameter Estimate	STANDARD	T RATIO	PROB>[T]
INTERCEPT			•	10.9496	0.0001
SACTO		0		16.5003	9
V152 V156W				1.1060	<u> </u>
V157C		0	•	0.4959	9.7
V159A	٠.	į	0.050685	-2.31	0.00
V160 V165				1.2160	•
V168	· ·		•	4.3137	Ġ٠
V169 V173			•	1.1361	10
KHS	••			2.2956	9
BINHS OTH		0.1 <b>8</b> 3965 0.016059	0.055620 0.088662	3.3076 0.1811	7.5
	!	1			76 91
MODEL: MODELO	_		3518	PROB>F	0.0001
DEP VAR: V37		ASM	1.252290	R-SQUARE	0.0776
VARIABLE	DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT	н.	•		16.0332	0.0001
SUPER		•		-5.3945	9
V152	-	0		-1.4069	~;
V156W	<b>,</b>	•		2.9136	
V158	•			1.3751	<b></b> .
V159A	<b></b> -	•		-3.0173 -1.3992	9.5
V165	٠.	ö		-1.4465	: =:
V168	<b>-</b> -	•		3.6245	
V172				-2.7527	9.0
WHS		0.328223	0.055502 0.056627	5.9137 8.1754	0.0001
HA	· <del>~</del>			3.0842	•

Table C.5--continued

~ <b>~</b>		P	· ·
9.97 0.0001 0.0408 PROB> T	0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001	PROBY   18.57 PROBY   7   0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001	
FRATIO FROBSF R-SQUARE T RATIO	21.06.00.00.00.00.00.00.00.00.00.00.00.00.	F RATIO PROBATIO T SQUARE 13.9919 -0.3419 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2574 -1.2	.0
3895.654 3518 1.107349 STANDARD ERROR	0.164040 0.049684 0.0238684 0.023862 0.023862 0.020759 0.018525 0.051986 0.052191 0.052191 0.052191	4233.662 1.203429 1.203429 2.31808 0.045132 0.045132 0.045132 0.054191 0.050586 0.013099 0.013099 0.012459	.05551 .0 <b>6848</b>
SSE DFE MSK PARAMETER ESTIMATE	3.455176 0.000604766 0.000604764 0.0007615 -0.027515 -0.027367 -0.089091 -0.069012 -0.069012 -0.1797155 -0.1797155	SSE DFE PARAMETER 3.010987 0.199324 0.179324 0.0585054 0.015031 0.012091 0.012091 0.012091 0.012091 0.012091	-0.043573 -0.096675
ı Dı	- THEFTERMENT   	<u> </u>	
MODELO1  V38	<b>*</b>	MODELO1: V39	
MODEL: DEP VAR: VARIABLE	INTERCEPT SUPER SACTO V153 V156 V159 V169 V172 WHS WHS WHS	A CE ORBE	BNHS OTH

Table C.5--continued

DEP VAR: V40 VARIABLE D			1.07 <b>8996</b>	H-BOUAKE	
۵					1
	8	Parameter Estimate	STANDARD	T BAT10	PROB>   T
	<b>~</b> -	2.460744	0.161927	15.1967	0.0001
	٠,	-0.362929	93	-9.5469	0.0001
	_	-0.067762	.023	-2.8768	0.0070
	٦.	0.057814	20.	1.3528	700
	<b>-</b>	0.199704	250	6.004 4.004	1000
	٦.	-0.000200		-2.5521	0.0107
	•-	-0.00645943	5	-0.5208	0.6025
	-		.051	1.9007	0.0574
	_	0.100443	20.	6.3126	0.0001
	_	-0.141676	.042	-3.3068	0.0010
	<b>-</b>	-0.060009	5	-5.0866	0.0001
	٦,	0.132006	150.	2.5623	*010.0
	_	•	.052	-0.4950	0.620
	<b>~</b>	-0.00126385	. 083	-0.0151	
MODEL 01		T C	4230,102	P BATIO	34.02
		DFE		PROB>F	0.0001
V41		HSE	1.202417	R-SQUARE	0.1267
		PARAMETER	STANDARD		
ā	ğ	ESTIMATE	ERROR	T RATIO	PROB>   T
•	_	3.758924		21.9901	0.0001
		0.764907		14.7742	0.0001
		-0.063888		-1.5920	0.1115
	. –	0.015165		0.6099	0.5420
	_	-0.101815	•	-2.2569	0.0241
. •	_	-0.054467	•	-1.5513	0.1209
- '	_	-0.00102009	•	-0.0472	0.9624
	ᇽ,	-0.114236	•	2667.7-	0.0239
	<b>,</b>	-0.00966588	•	785/-0-	
•	٠,	-0.19854.0-	•	- 3.0010	2000
	٠,	-0.004/3334	•	A 5.5.8	1000
	٠,	0.016170	•	1.2984	0.1942
		0.250024	0.054386	4.5973	0.0001
•	_	0.226873	•	4.0887	0.0001
•	_	0.153891	•	1.7398	0.0820

Table C.5--continued

HODEL:	HODET01		200	3015.368	F RATIO	18.86	
VAR	V42			0.057131	R-SQUARE	0.0744	
VARIABLE		ğ	Parameter Estimate	STANDARD	T RATIO	PROB>[T]	
INTERCEPT SUPER			3.701074	0.144322	25.6446 5.9040	0.0001	
<b>SACTO</b> V152			-0.017406		-0.158 -0.1528 0.0555	0.000	
			0.117957		3.9791	0.000	
_		-	0.079212		1.8554	0.0636	
			-0.046369		-1.0581	0.2901	
			0.045192		-2.9204	0.0038	
			0.043270 -0.207600		4.1151	0.0001	
			-0.307224		-6.5579 -3.2892	0.0001 0.0010	
HODEL	HODET01	:	<b>M</b> 500 0	4790.504	F RATIO	11.74	
VAR: V	V43		MSK	1.361712	R-SQUARE	0.0477	
VARIABLE		DE	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T	
INTERCEPT			3.897180	0.181908	21.4240	0.0001	
		٠,	-0.105392	0.042706	-2.4678	0.0136	
			-0.074637	0.048009	-2.8206 2.6316	0.0085	
		-	0.009796798	0.037365	0.2622	0.7932	
V159A		٠		0.053810	-1.0902	0.2757	
			0.007067076 0.106782	0.013934	1.6524	0.0641	
		<b></b>	-0.010322	0.017875	-0.5774	0.5637	
			-0.035658	0.013253	-2.6905	0.0072	
		٠.,	-0.259415	0.059049	-4.3932	0.000	
		<b>-</b>	219649.0-	C	h>71.71	1100.0	

Table C.5--continued

2.91 0001 0522	<u>=</u>	0001 0033 0019	0016 0001 0003 5453	00000000000000000000000000000000000000	14.22 .0001 .0571	<u> </u>	00001 00001 00001 2033	.0530 .0001 .0001 .4787 .277
000	PROB>   T	6666	66666		"oo	PROB>   T		
FRATIO PROB>F R-SQUARE	T BATIO	<b>8</b> 6 6	က်လ်ဝုံက်ဝုံ	90000	F RATIO PROB>F R-SQUARE	T RATIO		40000
2276.217 3518 0.647020	STANDARD		9.		3397.57 3518 0.965767	STANDARD		0.045317 0.01734 0.018054 0.018055 0.040533 0.04014
35E 0FE	PARN TTER RST::/ATE	3.547093 0.111576 -0.091640 -0.023266	,00404	i	SSE DFE MSE	Parameter Estimate	3.172755 -0.071229 -0.175580 -0.091029 -0.197680 -0.041586	-0.00286039 -0.341319 -0.341319 0.084980 -0.00796744 -0.00796704
	à		<b> </b>			Ö		
MODELO1	M	ŧ.			MODELO1	<b>N</b>	<b>t</b>	
HODEL: DEP VAR:	VARIABLE	INTERCEPT SUPER SACTO V152	V156W V156W V159A	V168 V169 V172 WHS BAHS OTH	MODEL: DEP VAR:	VARIABLE	INTERCEPT SUPER SACTO VI 52 VI 55W VI 57C	V159A V160 V168 V172 WHS

Table C.5--continued

HODEL:	HODET 01		# # # # # # # # # # # # # # # # # # #	4112.05	F RATIO	18.43	
DEP VAR:	97/		MOM	1.168860	R-SQUARE	0.0728	
VARIABLE			Parameter Estimate	STANDARD	T RATIO	PROB>   T	
INTERCEPT	E+		3.061561	0.168535	90	0.0001	
SACTO V152			-0.3317 <b>48</b> -0.066902	0.039567 0.024516	. 384 . 728		
V156W		-	0.108979	0.044480	450	•	
V158		4 ,		0.021328	020		
V159A V160			-0.202102 0.009 <b>8</b> 56208	0.049854 0.012909	. 053 . 763		
V165		-	0.116473	0.053407	.180	•	
0169 V169			-0.069407	0.044592	. 556		
V172		<b></b>	-0.067732 0.240348	0.012279	. 516 . 482		
			0.010132	0.054708	185		
					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
HODEL:	MODET 01		100	5503.29	F RATIO		
DEP VAR:	747		NSE	1.564324	R-SQUARE	0.0277	
VARIABLE		DE	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T	
INTERCEPT		~•	3.253142	7,	16.6852	•	
SOPER			0.043122	ب	-2.1794		
V152		<b>,</b>	0.101630	٠.	3.5834	•	
V1558			0.0004034413	ب د	0.0101		
V158		<b>~</b> •		9,	0.7770	•	
V159A V160			-0.026148	•	-1.7509		
V165		٦,	-0.129631	9,	-2.0981	•	
V168 V169		<b>-</b> -	0.03216		1.5502		
V172		-	-0.00414987	90	-0.2921	• •	
BNHS		٠.	-0.210973	0.063290	-3.3335	000	
H.		-	BA0109.0-	7	P111.0:	•	

Table C.5--continued

<b>Pa</b>
ESTIMATE
3.002117
0.0136
_
-0.1306
0.0533
-0.1.59
0.3115
0.2661
SSE DFE NSE
Parameter Estimate
3.7728
-
•
-0.008485
-0.02765 0.00854921
0.005591219
-0.2383

Table C.5--continued

MODEL	HODET 01		100 100 100 100 100 100 100 100 100 100	4506.149	F RATIO PROB>F	22.00 0.0001	
DEEP VARI	VSO		1181	1.280884	R-SQUARE	0.0857	
VARIABLE		Đ	Paraueter Estinate	STANDARD	T RATIO	PROB>   T	
INTERCEP	<b>6</b> 4		3.032801	0.176426	17.1902	0.0001	
SACTO		٠.	-0.363042	0.041420	-8.7650	0.0001	
V152			0.155586	0.046562	3.3415	0000	
V157C		<b>-</b>	0.007586762	0.036239	0.2094	0.0342	
<b>6158</b>			-0.122776	0.052189	-2.3525	0.0187	
V160		-	0.030996	0.013514	2.2937	0.0219	
V165			0.128631	0.033908	4.2957	0.0001	
V169		-	-0.133125	0.046680	-2.8519	0.0044	
V172		<b></b> -	-0.049805	0.012854	-3.8747	0.0007	
		-	-0.047426	0.057269	-0.6261	0.4077	
5		-	0.012261	0.091292	0.1343	0.6932	

Table C.5--continued

JOH 17800M	107ECO	358 1130	4475.976	F RATIO	6.02
DEP VARI VSI		MSK	1.273031	R-SQUARE	•
VARIABLE	2	Parameter Estinate	STANDARD ERROR	T RATIO	PROB> [ 1
INTERCEPT	-	2.926449		16.6338	0.0001
		0.242371	0.053287	1.5578	0.1194
V152	•~	0.040922		1.5990	0.1099
V156W	<b>~</b> ~	0.060779		1.4853	0.1376
VIS /C				-1.2493	0.2116
V159A	-4-	-0.010001		-0.2075	0.223
	<b>-</b>			-1.4865	0.1367
V160	-			-3.4715	0.0003
6914	<b>~</b> ,			2.4615	0.0139
	<b>-</b>	-0.056514		-1.0096	0.3127
1	. ~	_		-3.6913	0.0007
5	-	-0.0: \$60		-0.2813	0.1/65
ON 178CON	107200		3564.41	P RATIO	17.96
DEP VAR: VS2	~	750 180	1.013769	R-SQUARE	0.0712
	,	PARAMETER	STANDARD		
VARIABLE	ă	ESTIMATE		T KATIO	i i lacua
INTERCEPT	~	4.063677	0.157000	25.8832	0.0001
	<b></b> .	-0.322314	0.047552	2.4146	0.0001
	<b>→</b>	0.05000	0.022838	3.5386	0.0004
41 S 6 W		-0.046833	0.041435	-1.1303	0.2584
V157C	<b>~</b> •	-0.067110	0.032249	2.7944	0.0052
V 1 5 0		0.023181	0.046442	0.4991	0.6177
V160	. ~	-0.00527028	0.012026	-0.4382	0.6612
V165	-	-0.109354	0.049752	-2.1980	0.0280
191A	<b>-</b>	-0.133616	0.015428	0.7063	0.4800
V169		0.036125	0.011439	3.1582	0.0016
2 T T	· ~	-0.242002	0.049951	-4.8624	0.0001
	, p.,	0.053761	0.050964	1.0549	0.6434
₹	→	-0.03/616	> P • • • • • • • • • • • • • • • • • •	)	)

Table C.5--continued

MODEL: MODEL01	6	100	2213.957	F RATIO	15.12	
DEP VAR: VS3			0.629681	R-SQUARE	0.0606	
VARIABLE	ă	PARAMETER ESTIMATE	STANDARD ERROR	T RATIO	PROB>   T	
INTERCEPT	-4-	12028	0.123735	•	0.0001	
SACTO		-0.082707	0.029049	-2.0471	0.004	
V152 V1565	<b>~</b> -	01532 07305	0.017999		0.3945	
V157C	· ~	00512	0.025416		0.0008	
V158	<b>~</b> ~	12520	0.015656	•	0.0001	
V159A V160	-	01024	0.009477690		0.2798	
V165	٦.	04362	0.039210	•	0.2660	
99TA	<b></b>		0.032739		0.004	
V172	••	14043	0.009014973		0.4284	
	,d ·	0.02729	0	•	0.4882	
		92 4 3 9 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0.040165		0.0262	
	•					
MODEL: MODELO	.01	198	3731.332	F RATIO	27.62	
DEP VAR: VS4			5	R-SCVARE	0.1054	
VARIABLE	ğ	Parameter Estimate	STANDARD ERROR	T RATIO	PROB> [T	
INTERCEPT	-	3.549326	•	.095	•	
SUPER	<b>-</b>	0.230631	•	4.740	•	
VIS2	<b>-</b>	0.029240		251		
V1 56W		-0.073314		. 729	•	
V157C	<b>~</b> -	0.182796	•	.540	•	
V159A	<b>-</b>	-0.111936		2.355	• •	
V160	-	-0.0013753	•	.111	•	
V165	<b></b> -	0.143762	•	.82 <b>4</b>	•	
99[7	<b>-</b>	-0.101416		. 386		
V172		-0.068843		5.882	•	
25	<b>~</b> •	0.2.9474	-	4.490	•	
<b>DATE</b> OTH		-0.201123	0.083121	-1.0124	0.0156	

Table C.5 -- continued

MODEL	MODET 01		388	5014.014	F RATIO PROB>F	36.53	
DEP VAR:	V5.5			1.426056	R-SQUARE	0.1348	
VARIABLE		2	PARACTER ESTINATE	STANDARD	T BATIO	PROB>   T	
INTERCEPT	t	,-4 e	2.146084	.18620	11.5252	0.0001	
			-0.253965	0.043716	-5.8094	• •	
V152		<b></b>	0.021451	.02708	6.0304		
V157C			0.243899	03824	•	•	
V158			0.003304789	.05358	0.0600		
V160 V160		4	0.03220	.01426	2.2580	•	
V165		<b>~</b> -	0.215437	.05900	1.5548		
691A			-0.176087	.04926	<b>.</b> .	•	
V172		٦,	0.03977	.01356	7	•	
SH3		<b>~-</b>	-0.018303	.05944	-3.1655		
2 Z		-	-0.033151	.09635	•	• (	
!		!				60	
MODEL	MODEL01		1900 1900	3516	PROB>F	0.0001	
DEP VAR	V56		HSH.	1.158000	R-SQUARE	0.0751	
91041		6	PARAMETER	STANDARD	T RATIO	PROB>[T]	
VAKIABLE		5				-	
INTERCEPT	ŀ	~	3.113423	.16779	18.5546	0.0001	
SUPER		<b></b>	0.441479	78050	-2.4605	.013	
V152		4 ~	0.019552	.02440	0.8010	. 423	
M95 [A		-	0.015982	.04428	0.3609	. 18 	
V157C		٦.	č	03446	0.0085	210.	
V158		٠,	5	.04963	~	.007	
V160		· ~	-0.017186	.01285	-1.3371	.181	
V165		-	0.025807	.05317	0.4853	70.	
V168		<b>~</b>	0.021390	0.016488	-5.7532	100	
V172		-	-0.017914	01222		.142	
MHS		٦.	0.272682	.05338	5.1077	280	
		<b>-</b>	0.058239	.08682	-0.6838	492	
5		•					

Table C.5--continued

	HODEFO!		188 188 188 188 188 188 188 188 188 188	5044.677	F RATIO	14.82	
DEP VAR	VS7		480 W3E	1.434777	R-SQUARE	0.0895	
VARIABLE		<b>06</b>	Parameter Estimate	STANDARD ERROR	T RATIO	PROB> [T]	
INTERCEPT SUPER	-		3.664392	0.186777	19.6191	0.0001	
SACTO V152			0.112360		2.5624 0.5576		
7156W			-0.015747		- 3. 3610	• •	
V158 V159A		·	0.056661	0.023636	2.3972		
160 160 160			-0.206468		-3.4863		
168 169 169			0.023699		0.4796	• •	
V172			0.037557		2.7599 0.5215		
BNIHS OTH			0.052334		0.8632 0.9613		
HODEL:	HODET01		11 to 0	4043.176	F RATIO	32.55	
DEP VAR:	V58		HSE	1.149936	R-SQUARE	0.1219	
VARIABLE		DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>[T]	
INTERCEPT		~	3.025206	0.167212	18.0920	0.0001	
SUPER		<b>-</b>	0.2510/4	0.039256	-6.4285	0.0001	
V152		, <b></b> ,	0.025333	0.024323	1.0415	0.2977	
156W			0.154562	0.034346	6.7541	0.0003	
158		<b>.</b>	-0.110528	0.021160	w c	0.0001	
159 <b>A</b> 160			0.002142252	0.012808	0.1673	0.8672	
V165		<b></b> -	0.170974	0.052988	3.2267	0.0013	
69T		<b>-</b>	-0.070543	0.044242	-1.5945	0.1109	
V172			-0.061143	0.012183	-5.0189	0.0001	
BNHS		٠	-0.203347	0.054279	-3.7464	0.000	
H.		-	-0.1 1717	0.086524	-1.4067	0.1596	

Table C.5 -- continued

EDEL:	HODET01		200	3845.857	F RATIO	17.35
DEP VAR	V59		100	1.093816	R-SQUARE	0.0689
VARIABLE		ă	Paraketer Estinate	STANDARD	T PATIO	PROB> [T]
INTERCEPT SUPER	•		1.974424 0.257100	0.163081	12.1070 5.2051 -5.7446	0.0001
20CTU V152 V156W			-0.03364	0.023722	-0.9967 -0.8237 4.5528	0.3190 0.4102 0.0001
150 150 160 160			-0.000485437 -0.054079 0.013072	0.020637 0.048241 0.012492	-0.0235 -1.1210 1.0464	0.0000000000000000000000000000000000000
V168 V168 V169			0.043006 0.086223 -0.062822 -0.063809	0.051679 0.016025 0.043149 0.011882	0.8322 5.3805 -1.4559 -4.3436	0.0001 0.1455 0.0001
WHIS OTH OTH	-		0.144087 0.043336 0.108728	0.051886 0.052938 0.084387	2.7770 0.8186 1.2884	0.0055 0.4131 0.1977
MODEL: DEP VAR:	MODELO1 V60		838 DFE MSE	4712.823 3516 1.340393	F RATIO PROB>F R-SQUARE	6.94 0.0001 0.0268
VARIABLE		DE	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>[T]
Intercept Super	•		2.324129	0.180529	12.8740 2.5960 1.3489	0.0001
SACTO V152 V156W			0.039112	0.047645	1.4894	0.1365
157C 158 159A			0.085430 -0.070826 -0.100276	0.037082 0.022845 0.053402	2.3038 -3.1002 -1.8777	0.0213 0.06019 0.0605
V165 V165 V168			-0.074948 0.1 0070 0.044817 0.105746	0.013828 0.057208 0.017740 0.047766	-1.8042 1.7492 2.5264 2.2139	0.0713 0.0803 0.0116 0.0269
V172 WHS BNHS OTH			-0.048922 0.337141 0.086578 -0.027832	0.013153 0.057437 0.058601 0.093415	-3.7195 5.8697 1.4774 -0.2979	0.0002 0.0001 0.1397 0.7658

Table C.5--continued

HODEL:	HODZCON		388	4928.306	F RATIO	18.22
DEP VAR:	V61		18 N		R-SQUARE	•
VARIABLE		D.	Paraketer Estimate	STANDARD ERROR	T RATIO	PROB> T
INTERCEPT		٦.	3.299060	0.184610	17.8704	0.000
SOPER		<b>-</b>	1.44 <i>(</i>	.04334	191	
V152		·	018	.02685	268	. 788
V156W		-	1460	.04872	818	96
V157C		<b>-</b>		.03792	300	170
# C T A		<b>-</b> -	807	05461	1.260	207
4757A		•	584	.01414	0.279	.779
V165		-	804	.05850	675	.093
V168		-	286	.01814	709	. 178
V169		-	932	.04884	2.034	.042
V172		, ب	1328	.01345	187	200
SHS		⊶.	768	.05873	100.7	700.
BNHS		<b>-</b> 4 -	777	. U3992	4 . A	156
H 15		• !				
MODEL	MODEL01		<b>388</b>	3404.527	P RATIO	27.78
			DFE	351	PROB>F	8
DEP VAR	V62		MSE	0.968295	R-SQUARE	. 10
			PARAMETER	STANDARD		
VARIABLE		DE	ESTIMATE	ERROR	T RATIO	PROB> T
INTERCEPT		-	.55387	.15343	16.6442	0.0001
SUPER		-	.36387	.04647	839	0.0001
SACTO		-	.17243	.03602	786	0.0001
V152		-	.03092	.02232	382	0.1660
V1 56W		-	.02003	.04049	7,	6020.0
V157C		٦.	0.12968	.03151	11.	100.0
V158		٠,	77100	12410.	0.00	0470
V159A		٦,	76160.0	01175	280	0.7795
2917		٠,	0.19880	.04862	088	0.0001
V168		·	.08842	.01507	864	0.0001
V169		-	.01463	.04059	360	0.7184
V1.72		<b>~</b> -	0.047930	00	4.2875	0.0001
SHW S		<b>-</b>	17468	04980	507	0.0005
orn Orn		٠,	43906	.07939	530	0.0001

Table C.5--continued

DEP VAR: V63  NSE CAR: V63  VARIABLE DF ESTIMATE STANDARD VARIABLE DF ESTIMATE STANDARD SUCTO			())
PARAMETER	0.977111	R-SQUARE	0.0493
EPT 1 2.903658 1 0.024931 1 0.024931 1 0.01323585 1 0.012323585 1 0.012779 1 0.01407572 1 0.01407938 1 0.01407938 1 0.01407938 1 0.01407938 1 0.01407938 1 0.016997 1 0.253747 1 0.253747 1 0.253747 1 0.253747 1 0.253747 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016997 1 0.016987 1 0.016987 1 0.017877	TANDARD ERROR	T RATIO	PROB>   T
1	.154136	18.8383	0.0001
1	.036186	-6.6287 0.1572	0.0001
1 -0.072779   1 -0.072779   1 -0.00707572   1 -0.00707572   1 -0.00707572   1 -0.00707572   1 -0.00707572   1 -0.0070706   1   0.0070706   1   0.0070706   1   0.0070706   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1   0.0070707   1	.040679	-0.7294	0.4658
MODELO1 1 0.001407938 1 0.001407938 1 0.001407938 1 0.001407938 1 0.001407938 1 0.263747 1 0.263747 1 0.263747 1 0.263747 1 0.263747 1 0.263747 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001883104 1 0.00188310	031660	-2.2988	0.0216
HODELO I 0.011292 0.001311 0.001407938 0.001407938 0.001407938 0.001407938 0.0016997 0.263747 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.016997 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.0169937 0.01699	045595	-1.7481	0.0805
I 0.001407938 1 0.001407938 1 0.055080 1 0.255080 1 0.255080 1 0.255080 1 0.255080 1 0.255080 1 0.255080 1 0.255080 1 0.255080 1 0.2571MATE 2.938049 1 0.0524798 1 0.0524798 1 0.0524150 1 0.001883104 1 0.001883104 1 0.001883104 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470 1 0.0018470	.011806	0.9565	0.3389
1	015146	0.0930	0.9259
I -0.055080  I 0.263747  I 0.235660  I 0.235660  I 0.16997  EST IMATE  ESTIMATE  I 0.194710  I 0.0194710  I 0.025186  I 0.025186  I 0.001883104  I 0.001883104  I 0.001883104  I 0.001863104  I 0.00186416  I 0.00186410	040782	-1.9735	0.0485
BET 0.263747 0.263747 0.235660 1 0.235660 1 0.235660 1 0.235660 1 0.255660 1 0.255660 1 0.255660 1 0.257960 1 0.254150 1 0.001883104 1 0.001883104 1 0.001883104 1 0.001863104 1 0.001863104 1 0.001863104 1 0.001863104 1 0.001863104 1 0.001863104 1 0.001863104 1 0.00186416 1 0.00185788 1 0.00186416 1 0.00185788 1 0.00186416 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.00185788 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1 0.0018578 1	.011230		0.0001
RE MODELO1 SSE DEE NSE DEE NSE DEE NSE DEE SETIMATE SETIM	049040		0.000
RE MODELO1 SSE DEE DEE DEE DEE DEE BLE MSE 1 1 2.938049 1 0.194710 1 0.194710 1 0.194710 1 0.194710 1 0.024150 1 0.025186 1 0.0125186 1 0.003646416 1 0.0035788 1 0.0035788 1 0.0035788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.00735788 1 0.0073578 1 0.00735788 1 0.	.079758	0.2131	0.8313
DEE MSE   DEE   DE		F RATIO	41.21
AR: V64 BLE DF ESTIMATE  1 2.938049 1 2.938049 1 0.194710 1 0.524798 1 0.025186 1 0.0125186 1 0.003646416 1 0.00735788 1 0.00735788 1 0.003546416 1 0.00735788	3516	PROB>F	0.0001
PARAMETER  BLE DF ESTIMATE  1 2.938049  1 0.194710  1 0.524798  1 0.01883104  1 0.01883104  1 0.01883104  1 0.013646416  1 0.003646416  1 0.0035788  1 0.0035788	.146002	R-SQUARE	•
2.938049 1 0.194710 1 0.524798 1 0.0514798 1 0.01883104 1 0.01883104 1 0.01883104 1 0.01883104 1 0.013846416 1 0.00354816 1 0.00357988	STANDARD	T RATIO	PROB>   T
1 0.0035488 0 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.184710 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.18470 0.1	366331	0003 11	.000
1 0.00125786 1 0.025186 1 0.025186 1 0.001883104 1 0.003646416 1 0.003546416 1 0.003546416 1 0.0035788 1 0.0035788	050558	3.8512	0.0001
1 0.025186 0 0.441934 1 0.025186 0 0.254150 0 0.001883104 0 0.001883104 0 0.001583104 0 0.001583104 0 0.001583104 0 0.001583104 0 0.001583104 0 0.001583104 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.00158310 0 0.0	039189	13.3914	0.0001
1 0.041934 1 0.001883104 1 0.001883104 1 0.0137902 1 0.013648 1 0.00364616 1 0.0035788 1 0.00785788	.024282	1.0372	0.2997
1 0.024150 1 0.001883104 1 -0.0137902 1 -0.073937 1 0.003646416 1 -0.00725788 1 -0.00725788	044055	10.0314	0.0001
1 0.001883104 1 -0.037902 1 -0.073937 1 0.003646416 1 0.00725788 1 -0.00725788	034287	-6.5374	0.0001
1 -0.13.902 1 -0.012088 1 -0.073937 1 0.00366416 1 0.389914 1 -0.00725788	021124	0.0891	0.9290
1 -0.073937 1 0.003646416 1 0.00725788 1 -0.0725788	012786	-0.9454	0.3445
1 0.003646416 (1 0.389914 (1 0.00725788 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0.0078470 (1 0	052897	-1.3977	0.1623
1 0.389914 ( 1 -0.00725788 ( 1 -0.078470 (	016403	0.2223	0.8241
1 -0.00725788 ( 1 -0.078470 (	.044166	8.8283	0.0001
0/48/0.0-	012162	-0.5968	0.5507
) 12500K	053109	-1.4//5	0.0311
-0.105757	086376	• -	0.2209

Table C.5 -- continued

DEP VAR: V65 VARIABLE SUPER SUPER SUPER SUPER SUPER V152 V156 V159 V159 V165	Ã		0.856348	R-SQUARE	0.0428	
VARIABLE SUPER SUPER 9ACTO V152 V158 V158 V158 V160	30					
1MTERCEPT 30PER 3ACTO V152 V156 V156 V156 V160		PAKAMETEK ESTIMATE	STANDARD ERROR	T BATIO	PROB> [ T	
9ACTO V152 V156W V159A V160 V165	44	2.824045	.04370	19.5711	99	
V157C V158 V159A V160		-0.175429 -0.122514 -0.046483	. 033 <b>8</b> 7 . 02099 . 03 <b>8</b> 08	-5.1785 -5.6368 -1.2206	504	
V160 V165	) A A A	• •	.02963 .01826 .04268	3.7925 -0.8934 -3.0510	0.000	
V168		0.0005889376 0.025057 0.010023	.01105 .04572 .01417 .03817	0.5480 0.7068 -0.4746	,,,,,	
V172 WH3 BNH3 BNH9 OTH	1 <b>44</b> 44		0.010513 0.046910 0.076640	-2.2052 0.8789 0.9856 -0.9856	0.0275 0.3795 0.3244	
MODEL: MODELO1 DEP VAR: V66	101	388 DF8 MS8	4037.142 3516 1.148220	F RATIO PROB>F R-SQUARE	49.92 0.0001 0.1756	
VARIABLE	DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB> (T	
INTERCEPT SUPER		. 44378		14.6258 15.1737 -8.1353		
V152 V156W V157C	1 <i></i>	.06878 .07886 .17705		-2.8299 1.7885 5.1588		
V159A V160	aaa.	.04608 .03862 .02156		-2.1796 -0.7815 -1.6848		
V165 V168 V169 V172 WHS BNHS OTH	deedee	0.055739 0.055739 -0.022654 -0.031627 -0.312383 -0.312383	0.012134 0.012134 0.053161 0.054238 0.086460	3.3948 -0.5124 -2.5980 -1.3830 -5.7595 -1.2878	0.0001 0.0094 0.0094 0.0001 0.0001	

Table C.5--continued

SSE 3791.353 F RATIO DFE 3516 PROB>F MSE 1.078314 R-SQUARE PARAMETER STANDARD T RATIO	2.698418 0.161921 16.6650 0.687863 0.049043 14.0258 -0.034152 0.038014 -0.8984 .0016586707 0.023554 0.2796 0.067824 0.02734 0.0341 -0.067824 0.027359 2.0420 -0.067829 0.042898 -1.3800 0.025862 0.051311 4.9865 0.023712 0.015911 1.4903 -0.026699 0.011797 -3.7365 -0.026699 0.051517 -0.5553 -0.030371 0.083787 -0.5553	SSE 4125.977 F RATIO DFE 3516 PROBSF MSE 1.173486 R-SQUARE DADAMYTER STRANDED	RATE ERROR T RATIO	3.363574 0.168916 19.9127 0.258692 0.051161 5.0564 0.098386 0.039656 -2.4810 0.045910 0.045910 0.045910 0.045910 0.04454 0.044580 0.044544 0.044580 0.044596 1.4245 0.053811 0.049967 -1.8774 0.0599622 0.012938 -0.5557 0.0428392 0.055328 -0.5557 0.05536 0.044693 -1.2388 -0.055146 0.053742 -1.0819
MODEL: MODELO1 DEP VAR: V67 1	INTERCRPT 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1	MODEL: MODELO1 DEP VAR: V68	VARIABLE DF	INTERCEPT

Table C.5--continued

121055
SSE DEE MSE MSE MSE MSE MSE MSE MSE MSE ESTIMATE ESTIMATE 2.753673 -0.0331680 -0.055258 -0.055258 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.055202 -0.05520

Table C.5--continued

PARAMETER STANDARD T RATIO FRE 1 3.498689 0.176120 19.8653 0.053343 5.6291 0.0053343 5.6291 0.0053343 5.6291 0.0053343 5.6291 0.0058951 0.058176 0.043349 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.058176 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.0581776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.05817776 0.058177776 0.058177776 0.0581777777777777777777777777777777777777	HODEL: HODELO!		20 C	4485.447	F RATIO PROB>F P-SOUARE	17.80 0.0001 0.0706
### 1 3.498689 0.176120 19.8653		ğ	PARMETER ESTINATE	STANDARD	T RATIO	PROB> T
MODELO1  PARAMETER STANDARD  PARAMETER STANDARD  ESTINATE ERROR  1 0.0052542 0.005313  1 0.0052549 0.005313  1 0.0054695 0.0055619 1.6352  1 0.0054695 0.0054942 1.6352  1 0.0054695 0.0054942 1.6352  1 0.0054695 0.0054942 1.05234  2 119.12 FRATIO  PARAMETER STANDARD  PARAMETER STANDARD  1 0.005526242 0.005319 1.3670  1 0.00526524 0.005319 1.3670  1 0.0054695 0.005319 1.3670  1 0.005526242 0.005319 1.3670  1 0.0054695 0.0038361 0.1666  1 0.0054695 0.0038361 0.1666  1 0.0054695 0.0038361 0.01699  1 0.0064440 0.018816 0.018916 0.01699  1 0.0064440 0.018816 0.018816 0.018917 0.018919  1 0.0064440 0.018818 0.0038318 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.005818 0.0058	t				19.8653	0.0001
1		4 ~4			-9.5298	0.0001
0.059154   0.032287   0.03149   0.03149   0.03149   0.032287   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0.03149   0		٠,			-1.1301	0.2585
MODELOI  1		٦,			1.6352	0.1021
1		4			-0.7910	0.4290
MODELOI  1 0.055789 0.017306 -0.6062 -0.6062 -0.6062 -0.6062 -0.60783 0.015599 -5.2825 -0.057783 0.012832 -5.2825 -0.057783 0.012832 -5.2825 -0.05777 0.05639 -0.55277 0.05639 -0.55277 0.05639 -0.55277 0.05629 -0.55277 0.05177 0.05629 -0.5322 0.05629 0.05778		٦,			-0.9349	0.3499
MODELO1		<b></b>			1.0532	0.2923
T 1 0.0064267 0.046599 -0.6062 0.067783 0.012832 -5.2825 0.057170 -0.52825 0.057170 -0.52825 0.057170 -0.52825 0.057170 -0.52827 0.057170 -0.52825 0.057170 -0.52825 0.057170 -0.52825 0.057170 -0.5322 0.057170 -0.5322 0.057170 -0.5322 0.057170 -0.5322 0.057184 0.057188 0.024620 -2.0728 0.031894 0.015819 -3.0108 0.016526242 0.035810 0.015819 -3.0108 0.05526242 0.035810 0.015819 -3.0108 0.056440 0.0188515 0.0464 0.0188515 0.0464 0.038212482 0.056440 0.038212482 0.0464 0.0188515 0.0464 0.0565460 0.038215 0.0464 0.0565460 0.038215 0.0464 0.0565487 0.038215 0.0464 0.0565487 0.038215 0.0464 0.0565487 0.038215 0.0464 0.0565487 0.038215 0.0188515 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.038215 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.0565487 0.05		- ۲			-3.2236	0.0013
-0.067783   0.012832   -5.2825   0.025635   2.0629   0.055317   0.05635   2.0629   0.055317   0.05635   0.055322   0.052317   0.05635   0.057170   0.55322   0.057170   0.05322   0.057170   0.057170   0.057170   0.055459   0.057170   0.0554587   0.05925   0.059272   0.055459   0.059272   0.055459   0.059272   0.055510   0.056500   0.015319   0.056500   0.015319   0.056500   0.015319   0.056500   0.015319   0.056500   0.016650   0.016650   0.056500   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.016650   0.01665		٠-			-0.6062	0.5444
0.15594   0.056035   2.0629   1   -0.029625   0.057170   -0.5217   0.057170   -0.5217   0.057170   -0.5217   0.057170   -0.5322   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170   0.057170		• -			-5.2825	0.0001
-0.029625   0.057170   -0.5217   0.044497   0.091134   -0.5322   0.091134   -0.5322   0.091134   -0.5322   0.091134   -0.5322   0.091134   -0.5322   0.091134   -0.5322   0.091134   0.0520ARE   0.0028420   -2.0760   0.0186184   0.018665   0.018665   0.0186184   0.018665   0.0186184   0.018665   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184   0.0186184		- ۱			2.0629	0.0392
MODELO1 88E 2119.12 F RATIO DEED 35.6 BARDARE COURE COURS COURE COURS COURE COURS COURE COURS CO		ه			-0.5217	0.6019
MODELO1   SSE   2119.12   FRATIO   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956   1956		• ~			-0.5322	0.5947
PARAMETER STANDARD T RATIO FRO 1 1 3.966520 0.121055 32.7661 0.166364 0.036665 5.0780 1.0.036500 0.036665 1.3672 0.037284 0.037284 0.035810 0.01459 1.0.005226242 0.035810 0.015319 1.3656 1.0.004440 0.0138361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.04644 0.038361 0.068600 0.038351 0.0464 0.068600 0.038256 0.038256 0.05259				6. 6		
PARAMETER STANDARD T RATIO FRO ESTIMATE ERROR T RATIO FRO 13.966520 0.121055 32.7661 0.186184 0.036665 5.0780 1.0.036500 0.036665 1.3637 0.031894 0.0318949 1.3632 1.3632 1.0.046124 0.015319 0.1459 0.015319 0.1459 0.01680696 0.008819776 0.016860 1.0.068600 0.0188361 0.04644 0.0188361 0.04644 0.0188361 0.04644 0.0188361 0.04644 0.0188361 0.04644 0.0188361 0.04644 0.018819776 0.0464 0.008469599 0.038215 0.02199 0.0525489 0.039296 0.016566 0.008819776 0.016860 0.008469599 0.038215 0.02199	MODETO1			31.8112	PROBSE	
PARAMETER STANDARD  T 3.966520 0.121055 32.7661 1			181	•	R-SQUARE	•
DE ESTINATE ERROR T RATIO PRO 1 3.966520 0.121055 32.7661 1 0.186184 0.036665 5.0780 1 0.036560 0.017609 -2.0728 1 0.037284 0.028420 -2.0728 1 0.046124 0.031949 -1.1670 1 0.046124 0.015319 -3.0108 1 0.05226242 0.09272482 0.1459 1 0.008469696 0.008819776 0.0464 0 0.01895 5.4172 1 0.008469599 0.098515 0.2199 1 0.068696 0.008819776 0.2199 1 0.068698 0.0088515 0.2199			PARAMETER	STANDARD		
3.966520 0.186184 0.036665 10.166364 0.038420 -0.037284 0.031849 10.031898 0.031849 -1.1670 1.0.005226242 0.035810 -0.046242 0.035810 0.1459 0.036600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.068600 0.038361 0.066606	<b>L</b>	D	ESTIMATE	ERROR		PROB>  T
1 0.186184 0.036665 5.0780 1 -0.166364 0.028420 -5.8537 0.0316500 0.031849 -1.1670 0.0318949 -1.1670 0.0318949 -1.1670 0.0318949 -1.1670 0.0318949 -1.1670 0.0318949 -1.1670 0.0318949 -1.1670 0.0318949 -1.1670 0.0328865 1.3632 0.0328865 1.3632 0.0328865 1.3632 0.0328361 0.064467 0.038361 0.064460 0.0332030 2.1418 0.008469599 0.038515 0.2199 0.03654587 0.038515 0.031895 -0.1666	•	-	3.966520	0.121055	32.7661	0.0001
-0.166364 0.028420 -5.8537 -0.031284 0.017609 -2.0728 -0.0317284 0.017609 -2.0728 0.0317284 0.015319 -3.0108 0.005226242 0.015319 -3.0108 0.05226242 0.035810 0.1459 0.0529409 0.01895 5.4172 0.006469696 0.008819776 0.0464 0.00846959 0.038215 0.2199 0.00846959 0.038215 0.2199	,	_	0.186184	0.036665	5.0780	0.0001
-0.036500 0.017609 -2.0728 -0.0317284 0.031949 -1.1670 0.031898 0.024865 1.3632 0.005226242 0.035810 0.1459 -0.1459 0.05242 0.035810 0.1459 0.052400 0.01895 5.4172 0.0064440 0.01895 5.4172 0.00846959 0.038361 0.0464 0.00846959 0.038315 0.0464 0.00846959 0.038515 0.2199 0.052546 0.052546 0.052546 0.052546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.055546 0.0		~	-0.166364	0.028420	-5.8537	0.0001
0.001949		~	-0.036500	0.017609	-2.0728	0.0383
0.033898 0.024865 1.3532 -0.046124 0.015319 -3.0108 0.005226242 0.035810 0.1459 -0.02940 0.038361 0.78467 0.06440 0.038361 0.7666 0.06440 0.038361 0.7666 0.004096696 0.008819776 0.0464 0.008469599 0.038215 0.2199		_	-0.037284	0.031949	-1.1670	0.2433
0.005225242 0.015319 -3.0108 0.005225242 0.035810 0.1459 -0.002940 0.038361 0.7666 0.056440 0.011895 5.4172 0.056600 0.032030 2.1418 0.008469599 0.038515 0.0464 0.008469599 0.038515 0.0464		~	0.033898	0.024865	1.3632	0.1729
0.00525242 0.035810 0.1459 -0.00785058 0.009272482 -0.8467 0.054409 0.01895 5.4172 0.066400 0.032030 2.1418 0.0004096696 0.008819776 0.0464 0.00846959 0.038515 0.2199 0.038515 0.2199		-		0.015319	9070.5-	0.0070
0.0094695058 0.009212462 -0.009409 0.064409 0.011895 5.4172 0.0004096696 0.008819776 0.0464 0.008469599 0.038515 0.2199 0.008469587 0.038515 0.2199		<del>, -</del>		7	0.1404	
0.06440 0.011895 5.4172 0.06440 0.032030 2.1418 0.0004096696 0.008819776 0.0464 0.00846959 0.038515 0.2199 0.038515 0.019596 0.01666				į.	0.7666	0.4434
0.0084096696 0.008819776 0.0464 0 0.008469599 0.038515 0.2199 0.008469599 0.038515 0.2199 0.008469590 0.038515 0.2199		- ۱	0.05440	0.011895	5.4172	0.0001
0.0004096696 0.008819776 0.0464 0 0.008469599 0.038515 0.2199 0 -0.0084887 0.039296 -0.1666 0		-	0.068600	0.032030	2.1418	0.0323
0.008469599 0.038515 0.2199 0 -0.00854587 0.038296 -0.1666 0		۱ 🗝	٦.	ĕ	0.0464	0.9630
-0.00654587 0.039296 -0.1066 C		-		0.038515	0.2199	0.8260
		٦.		0.039296	-0.1066	7.08.0

Table C.5--continued

	252 DF3 DF3	3443.859 3516 0.979482	F RATIO PROB>F R-SQUARE	13.76 0.0001 0.0555
	Parameter Estimate	STANDARD	T RATIO	PROB> [T]
	3.575083		166	0.0001
(	091466		524	0.2997
o	976431 016796		220	0.5962 0.5962
, ,	047819	0.045650	-1.0475	0.2949
	967670		200	0.3074
•	224715		100	0.0001
7	121106 164385		200	0.0000
	022717 057711		123	0.6502 0.4699
	SSE	4565.412 3516	F RATIO	33.79
<u>a</u>	MSE Parameter	1.298468 STANDARD	•	0071.0
30	ESTIMATE		T KATLO	FRUBSITI
	55102		10.3147	0.0001
9	67769		-6.4191	0.0001
	40583		7.2628	0.0001
	50988 96110		-4.2744	0.0001
	63 <b>488</b> 17826		-1.2079 1.3098	0.2272
1.00.1	67425 20606	0.056306	2.9735 1.1802	0.0030 0.2380
	21813		-2.5911	0.0096
	07614		1.9036	0.0270
7	-0.040633 ).00596498		-0.7045	0.4812 0.9483

Table C.5--continued

75 61 61	Ŧ	20000000000000000000000000000000000000
16.75 0.0001 0.0667	PROB>   T	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
FRATIO PROBSF R-SQUARE	T RATIO	20 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.00 66.
4426.106 3516 1.258847	STANDARD	0.052989 0.052989 0.025499 0.025149 0.025149 0.013154 0.013154 0.015181 0.05569 0.05569
83E DFT MBM	PARAMETER ESTIMATE	-0.25522 -0.25522 -0.25522 -0.055235 -0.055235 -0.05522 -0.05522 -0.05522 -0.05522 -0.05522 -0.05522 -0.05522 -0.05522 -0.05522
HODEL: HODELO1 DEP VAR: V75	VARIABLE	INTERCEPT 8UFER 8UFER 9UFER VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS VISS

Table C.5--continued

MODEL: MOD	MODELO1	35E 07E	4116.887 3519 1.169903	P RATIO PROBSF R-SQUARE	23.64 0.0001 0.0915
VARIABLE	å	Paraneter Estinate	STANDARD	T RATIO	&   < <b>808</b> 4
INTERCEPT SUPER SACTO V152 V156W	ММММ	3.077713 0.538270 -0.211672 -0.049490 0.164075	.05106 .03106 .03957 .02452	18.2560 10.5417 -5.3481 -2.0181	88828
V157C V158 V169A V165 V168	ન <b>ન ન</b> ન ન	0.064600 -0.027920 -0.121896 -0.00785387 0.0138687	0.034628 0.021334 0.012913 0.053413 0.05366	2.4431 -1.3087 -2.4443 -0.6082 -2.5960 4.3216	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
V169 V172 WHS BNHS OTH	#####     	-0.030273 -0.061660 0.050092 0.04678967	.01228 .01228 .05363 .05472 .08723	-0.6787 -5.0201 0.9339 0.8213 0.0468	<b>48848</b>
MODEL: MOD DEP VAR: V77	MODEL01 V77	SSK DFE HSE	3641.406 3519 1.034784	F RATIO PROB>F R-SQUARE	10.01 0.0001 0.0409
VARIABLE	DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT SUPER SACTO	e e e e e	016	.15855 .04802 .03722	886 309 765 064	8882
V156W V157C V159A	' <del></del>	555	03256	5628 628 188 331	5227
V165 V168 V173 WHS OTH	1 M M M M M M M	0.012849 0.042470 0.042470 -0.081835 -0.015924 -0.104244	0.050245 0.015584 0.011552 0.050445 0.051465	22.5565 2.7259 -2.4529 -2.03157 -0.9264	0.000000000000000000000000000000000000

Table C.5--continued

NODEL: MODEL:01	_	888 770	3882.177 3519	F RATIO	8.29 0.0001
DED VAR: V78		<b>191</b>	1.103205	R-SQUARE	9
VARIABLE	2	PARAMETER ESTIMATE	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT	~	3.231309	.16371	19.7330	9
	<b></b>	0.206239	0.049584	4,1594	0.000
		-0.623588 -0.023588	02381	-0.9905	
V156W	• ~	0.006474093	.04320	0.1498	₩.
V157C	-	-0.017864	.03362	-0.5312	٠į
V150	<b></b>	-0.0 4426	.02071	-2.1444	99
V1594 V160	<b>-</b>	-0.00238776	01254	-0.1904	. =
V165	-	0.007091886	.05107	0.1367	•
V160	-		.01608	7.0984	9
V169	⊶.	0.006944817	.04331	0.1603	₹-
V172	<b>-</b>	0.010.0-	20110.	7000	: 9
	<b>-</b>	0.157667	05314	2.9707	9
TE O		-0.039342	.08471	-0.4644	
	•				
HODEE: HODEE01	_	<b>3</b>	3205.724	F RATIO	13.63
DEP VAR: V79		191	0.910976	R-SQUARE	0.0549
		PARAMETER	STANDARD		
VARIABLE	DE	ESTIMATE	ERROR	T RATIO	PROB>  T
INTERCEPT	-	2.092169	7	14.0636	0.0001
SUPER		0.314586	٠.	6.9010	0.0001
SACTO	<b>~</b>	0.167124	9,	4.7852	0.0001
V152	٦,	-0.02/454		1 1587	0.2040
V157C		0.141277		4.6234	0.0001
V158	-	-0.083154	•	-4.4170	0.0001
V159A	~	Ŧ	9	-2.0251	0.0429
V160	<b>-</b> -1	0.001994278	9	0.1750	0.8611
V165	٠.	0.022684	9	0.4812	0.6304
8917	<b></b>			9050-0-	9886.0
V172	٠.	;		-3.0701	0.0022
SES.	-	0.250946	•	5.3019	0.0001
BNHS	٦.	0.019314	0.046290	0.4000	0.6892
	→	*******	?	17071	1981.0

Table C.5--continued

15.25 .0001 .0610	PROB>   T	00011200000000000000000000000000000000	35.32 0.0001 0.1309 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001
	RATIO PRO	25.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.00 26.55.	FRATIO PROB>F R-SQUARE T RATIO 12.2757 3.5445 -5.8671 -0.7180 -1.9166 -4.8370 -1.9166 -4.661 -6.555
7 RATIO 19 PROB>F 12 R-BQUAR	•	000000000000000000000000000000000000	
1807.473 3519 0.513632	STANDARD	000000000000000000000000000000000000000	4488.293 1.275446 STANDARD ERROR 0.176026 0.051315 0.041326 0.041326 0.046457 0.052070 0.052070 0.012825 0.012825
338 340 340	Parameter Estinate	3.844903 0.186368 -0.064251 0.042261 0.0574285 -0.0574285 0.099171 0.099171 0.036389 0.036389 0.026241 -0.182396	88E DEE MSE PARAMETER ESTIMATE 2.160847 0.18930 -0.242462 0.018930 -0.49724 0.018930 -0.008377891 -0.008377891 -0.01342 -0.05842 0.061342 -0.01342 -0.01342
1701	ð	<b>налапананана</b>	6 AAAAAAAAAAAAA 10 11
MODEL: MODEL01 DEP VAR: V80	VARIABLE	INTERCEPT SUPER SACTO V152 V156 V156 V156 V169 V169 V172 WHS	MODEL: MODELO1 DEP VAR: V81 VARIABLE INTERCEPT SAC 7 V15 V15 V150 V150 V150 V160 V160 V169 V169 V169 V169 V169 V169 V172 WHS

Table C.5--continued

HODEL: HODEL01		33E 07E	2954.519 3519	F RATIO	11.47
VAR: V82			0.639590	R-SQUARE	0.0
VARIABLE	20	Parameter Estimate	STANDARD	T RATIO	PROB>   T
NTERCEPT	-	17.00	•	14.4762	0.0001
	<b></b> -	0.218456	-	-0.7025	0.4824
	٦.	04095		-1.9715	0.0487
	• ~	11157	٦.	2.9602	0.0031
	۱,-4	10699	٦	3.6471	0.0003
	-	05543	٦.	-3.0672	0.0022
		06345	٠.	-1.5020	0.1332
	-4	01034	٠,	1076.0-	0.3443
	<b>~</b>	08280	٠.	1.65.1	7.00.0
	<b>-</b> 4 ,	7372	٠,	7060	0.0358
	⊣,	7777	•	1 631	0.1051
	<b>~</b>	98910	•	1170.1-	
	<b>~</b>	24518	٠,٠	0.1909	0.00T
	-	7010	•	PC77.0-	
	-	13642	٠;	1.0400	
MODET 01		100	4654.741	F RATIO	22.64
7071		DFE	1.322745	R-SOUARE	0.0880
		•			•
		PARAMETER	STANDARD		
VARIABLE	Ģ	ESTIMATE	ERROR	T RATIO	PROB>   T
	-	2.319332		12.9383	8
;		0.257134		4.7359	8
	-	0.037336		0.8872	.37
	-	0.104270		3.9987	8
	·	-0.193101		-4.0816	ë
	-	0.092390		2.5092	2
	-	-0.010509		-0.4633	3
	· <del></del>	0.060785		1.1463	52
	-	-0.00475639		-0.3464	. 72
	-	_		0.5283	5.5
	~	0.143916		8.1701	9
	-			-1.8304	5
	~	-0.016152		-1.2367	7.
	-	-0.080430	0.057034	-1.4102	9901.0
	-	-0.347982		200K.C-	36
	~	-0.271450		2171.71	3

Table C.5--continued

20.37 0.0001 0.0799	<u>+</u>	000 000 000 000 000 000 000 000 000 00	0926	>   <del>1</del>	00001 00003 52001 00019 01066 01066 5011 5601
	PROB> [T		700	PROE	<b>૽૽૽૽૽૽૽૽૽</b>
F RATIO PROB>F R-SQUARE	T RATIO	21.6634 4.46230 1.2.6231 1.2.6231 1.2.6231 1.2.6351 2.3.1331 2.4309 2.4409 2.4409 2.4409 2.4409 2.4409 2.4409 2.4409	FRATIO PROBSE R-SQUARE		13.8752 8.04782 9.04782 -4.2782 5.2980 0.0993 -7.1986 -1.1085
4768.518 3519 1.355078	STANDARD	0.01819888 0.0228888 0.0328888 0.0328888 0.0328888 0.0328888 0.0532888 0.0532889 0.0532889 0.0532889	5444.341 3519 1.547127	ERROR	0.193870 0.058419 0.0285119 0.0285215 0.0285215 0.028520 0.054384 0.0518859 0.0518850 0.0518850 0.0518850 0.0518850
SSE DFE NSE	Parameter Bstimate	3.919690 -0.508985 -0.190079 -0.026908 -0.125701 -0.082711 0.067719 -0.192237 -0.043341 -0.241936 -0.241936	MSG BRACE MSG MSG MSG MSG MSG MSG MSG MSG MSG MSG	Parameter Estimate	2.689984 -0.178969 -0.393165 -0.018121 -0.158927 -0.57337 -0.057337 -0.147231 -0.136851 -0.068374 -0.068374
	ď			DF	
MODELO1	••	t	MODELO1	w	£.
MODEL: DEP VAR:	VARIABLE	INTERCEPT SACTO V152 V156 V156 V159 V169 V172 W13 W13 W143 W143 W143 W143 W143 W143	MODEL: DEP VAR	VARIABLE	INTERCEPT SUPER SACTO VISS VISS VISS VISS VISS VISS VISS VIS

Table C.5--continued

52.75 0.0001 0.1836	PROB>   T	0.00001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.00001 0.00001	11.46 0.0061 0.0466 0.0288 0.2333 0.0001 0.0001 0.8585 0.3979 0.0579 0.0603 0.0603 0.0603
F RATIO PROB>F R-SQUARE	T RATIO	15 05 05 05 05 05 05 05 05 05 0	F RATIO PROBSE R-SQUARE 16.8315 -2.18315 -1.1920 -0.6877 -0.6877 -0.6877 -0.1983 -4.451 -0.1983 -4.1377 -1.9664 -1.9664 -1.9664
4638.322 3519 1.318080	STANDARD	0.178944 0.0541944 0.042011 0.042011 0.017227 0.052945 0.013707 0.013846 0.013846 0.013846 0.058087	3796.353 1.078616 2519 1.078616 20161890 0.049033 0.023549 0.023549 0.023549 0.023549 0.023549 0.023549 0.023549 0.023553 0.0515908 0.0515908 0.0515908
888 DF18 181	Parameter Estimate	2.687536 -0.370426 -0.370426 0.233399 0.333399 -0.119170 -0.00281915 -0.00281915 -0.058162 -0.158841 -0.158841 -0.158841	BSB DFE MSE PARAMETER ES IMATE -0.107249 -0.278456 -0.278456 -0.278456 -0.216196 -0.278456 -0.016196 -0.016198 -0.016198 -0.016198 -0.008534 -0.008534 -0.010483 -0.010483 -0.010483 -0.010483 -0.010483 -0.010483
	3		<u> </u>
MODEL: MODEL01 DEP VAR: V86	VARIABLE	INTERCEPT SUPER SACTO V152 V155W V159W V159W V168 V168 V168 V172 WHS BNHS	MODEL: MODEL01  DEP VAR: V87  VARIABLE SACTO V152 V156 V158 V159 V159 V169 V169 V169 V169 V172 WHS BNHS

Table C.5--continued

MODEL: MODELO1	101	338	4315.793	F RATIO	32.44 0.0001	
DEP VAR: V88		100	1.226426	R-SQUARE	0.1215	
VARIABLE	Ď	Parajeter Estinate	STANDARD ERROR	T RATIO	PROB>[T]	
INTERCEPT		.9926	1726	17.3377	0.0001	
SACTO		43139	.04052	Ö,	9;	
V152	<b></b>	95	.02510 .04555	2.1408	10	
V157C	•	14390	.03545	÷,	85	
V158	r-1 r-	.0525B	.05106	-1.4840	::	
V160	•	0.01384	.01322	٠i د	55	
V165	<b></b>	.11458	.03469	3.6850	38	
691A		.09125	.04567	-1.9980	28	
V172	٦.	.08027	.01257	-6.3832	36	
WHS	<b></b> -	06/2T.	.05603	2.8476	18	
BANHS OTH		.07300	.08931	0.8174	7	
MODEL: MODEL01	101	14 TO 0	:	F RATIO	15.52	
DEP VAR: V89		NSE	1.102722	R-SQUARE	0.0621	
VARIABLE	DF	PARAMETER ESTIMATE	STANDARD ERROR	T RATIO	PROB> [T]	
604004471	_	3.856676		23.5632	0.0001	
SUPER	••	0.146820		2.9617	0.0031	
SACTO	<b>~</b> •	-0.269952		1.4109	0.1584	
751A V156W		-0.096815		-2.2413	0.0251	
V157C	٦.	-0.081060		-2.4111	0.0160	
V158 V159A	<b></b>	-0.180670		-3.7316	0.0002	
V160	<b></b> -	0.039593		3.1581	0.0016	
V165	<b>-</b> -	0.009643784		0.5996	0.5488	
V169 V169	• ~	-0.05720		-1.3210	0.1866	
V172	٦.	-0.055370			0.0001	
WHS		0.238856	0.053130	1.7334	0.0831	
HEO	-	0.089201			0.2923	

Table C.5--continued

MODEL	MODEL 01			336	3816.97 3519		23.98	
DEP VAR	067			M SM	1.084675	R-SQUARE	0.0927	
VARIABLE		D.	PAR	Parameter Estimate	STANDARD	T RATIO	PROB> [T	
INTERCEP'	•	-	m		16232	21.1553	0.0001	
SUPER		<b>-</b>	0 6	309243	0.049166	-5.8975	0.001	
SACTO VI S2		٠.	ö		.02361	1.0982		
V156W		-	ö		.04284	0.5532		
V157C		٦.	00		.03334	5.4754 13.6509		
V158		<b>→</b> -	9		04801	-0.4471		
4134 0160		_	, 0		.01243	0.2083		
V165			9		.05144	-0.6819		
V168		-	ö		.01595	6.5437		
6917		<b>~</b> ,	90		- <b>6469</b> 0.	-3.4115		
V172		٦.	į		05164	3.4849		
		<b>-</b>	ģ		.05269	-0.7112		
OTH OTH		44	ö		.08399	-1.3069		
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		! !	; ; ; ; ; ; ;		01	31.34	
HODEL:	MODETO1			100	2 .	PBORYE	0.0001	
DEP VAR	16/			NSE TSE	1.325256	R-SQUARE	0.1178	
				1				
VARIABLE		DF	PA	Parameter Estimate	STANDARD	T RATIO	PROB>   T	
		,	•			950		
INTERCEPT	Į-	<b>⊣</b> -	n c	.060929		033		
SOPER			Š	93585		3		
SACTO		٠.	Ö	025053		959		
W) 56W		. –	0	131654		. 780		
V157C		~	o	.245676		6.655		
V158		<b>–</b>	0	109571		4.625		
V159A		۰,	•	. 133691		3.A.		
V160		<b>⊣</b> -	5 c	164086		2.885		
5917			ò	047968		720		
691A		٠,-	o	.073854		. 555		
V172		<b>,-4</b>	9	.084583		470		
WHS		<b></b> .	00	0.284551	0.057088	1.1248	0.2608	
BNH®		<b>→</b> -	<b>&gt;</b> C	124451		350		
H.S		•	•	4 > > > > + + + + + + + + + + + + + + +				

Table C.5--continued

PARAMETER STANDARD T RATIO PRESTINATE REBOR 14.9298 10.189480 10.57390 6.5930 6.5930 6.378369 0.057390 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.5930 6.59		888 DFR	5200.606 3519	F RATIO PROB>F	20.58
2.831MATE ERROR T RATIO PROPERTION OF STANDARD CONTROL OF STANDARD			1.477865 Genumber	K-SQUAKE	
2.828898 0.189480 14.9298 0.378369 0.057390 6.5930 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.057390 0.0573	Ę,		ERROR	T RATIO	PROB> [T]
0.378369 0.024464 0.024464 0.024464 0.024464 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.0239789 0.038928 0.038028 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.096.894 0.0	~	2.828898		676	0.000
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0.127179 0.050134 -2.5368 0.0559287 0.013805 -5.0190 0.055928 0.06150285 1.2090 0.054363 0.0561502 1.2090 0.055928 0.06150285 1.2090 0.055928 0.056047 0.9339 0.05592 0.055928 0.05474 R-SQUARE ERROR ESTINATE ERROR T RATIO PROJ 0.054784 0.038825 -1.6196 0.054784 0.038825 -1.6196 0.054784 0.018233 -0.6303 0.04251 0.011493 0.018233 -0.6303 0.04251 0.0138121 0.024295 0.014158 3.8369 0.0145840 0.025251 0.0338121 0.04251 0.045657 0.033812 0.045657 0.045650 0.045650 0.045650 0.045650 0.045650 0.045650 0.045650 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.055831 0.045650 0.055831 0.045650 0.055831 0.045650 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831 0.055831	-	0.047676		9	6010.0
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0.061507 0.08659 0.0061507 0.098047 0.098047 0.098047 0.098047 0.098047 0.098048 0.098047 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.098048 0.0	-	-0.069287		616	0.0007
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3006.894 F RATIO 3519 PROB>F 0.85474 R-SQUARE 0.144078 18.8220 0 0.043638 -1.6196 0.020958 -1.6196 0.029594 1.8500 0.018233 -0.6303 0.018233 -0.8374 0.01620 -1.3961 0.045620 -1.3961 0.045620 -1.3961 0.0456340 -1.3600 0.0456340 -1.3600 0.045630 -1.3600 0.04	-	0.074363			0.4407
3006.894 F RATIO 3519 PROB>F 0.85474 R-SQUARE STANDARD T RATIO PR 0.043638 6.1777 0.043638 -1.6196 0.038025 -1.6196 0.029594 1.8500 0.029594 -0.6303 0.018233 -0.6303 0.012620 -1.3501 0.01458 -1.3501 0.014036 -1.3961 0.014158 3.8369 0.046769 3.6990 0.046769 3.6990	-	0.091570		E 1	0.3504
PARAMETER STANDARD T RATIO PRESTINATE ERROR 0.043636 -1.6196 -0.024540 0.024540 0.038025 -1.6196 -0.014580 0.018233 -0.6303 -0.6303 -0.015689 0.016233 -0.6303 -0.6303 -0.03363 0.014158 3.8369 0.014283 0.045840 2.1561 0.04553 -0.302.	!	B 0	٥	01440	12.58
STANDARD ERROR  0.144078 0.043638 0.043638 0.033825 0.029594 0.03825 0.029594 0.018233 0.018233 0.018233 0.04562 0.038121 0.04564 0.04564 0.04564 0.04564 0.04564 0.045655 0.04564 0.045655 0.045655 0.045655 0.045655 0.045655 0.045655 0.045655 0.045655 0.045655		4 6 6	٠,	PRORVE	0.0001
STANDARD T RATIO PROE 0.144078 18.8220 0.0443638 6.1377 0.023825 0.02958 6.1377 0.029594 0.029594 0.04566 0.010233 0.08374 0.01036 0.02455 0.038121 0.24551 0.04559 0.046569 3.6591 0.04553		MSE	.85447	R-SQUARE	0.0509
0.04468 0.04568 0.038628 0.038628 0.029584 0.029594 0.029594 0.018233 0.045620 0.042620 0.016230 0.016230 0.016230 0.016240 0.016557 0.016567 0.016567 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016569 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669 0.016669		DARAMPTER	STANDARD		
2.711829 0.144078 18.8220 0.054784 0.043638 6.1777 0.0554784 0.023825 -1.6196 0.0554784 0.020958 -3.6212 0.055474 0.029594 1.8500 0.055474 0.029594 1.8500 0.015408 0.018233 -0.6303 0.015408 0.011391 0.045657 0.08752 0.055334 0.045640 3.6990 0.045559 0.045690 0.04559 0.04559 0.04559 0.04559 0.04559 0.052521 0.046569 3.6990 0.0745299	DF	ESTIMATE	ERROR		PROB>[T]
0.269584 0.043638 6.1777 0.054784 0.033825 -1.6196 0.025894 0.02958 -3.6212 0.025894 0.02958 -3.6212 0.025894 0.02958 6.4546 0.025474 0.029594 1.8500 0.035474 0.018233 -0.6303 0.015408 0.011391 0.011036 -1.3951 0.014158 3.8369 0.024521 0.014158 3.8369 0.024521 0.014158 3.8369 0.024521 0.046769 3.6990 0.045769 0.045769 0.035253 0.045769 3.6990 0.025253 0.025253	_		.14407	18.8220	•
0.054784 0.033825 -1.6196 0.075894 0.020958 -3.6212 0.020958 0.025436 0.020958 -3.6212 0.054748 0.029594 1.8500 0.054748 0.018233 -0.6303 0.011491 0.042620 -1.8951 0.011391 0.045657 0.24955 0.054321 0.014158 3.8369 0.054321 0.014158 3.8369 0.0044201 0.01497 -4.2108 0.0045840 3.6990 0.0745299 0.046769 3.6990 0.025251 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074559 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579 0.074579	-		.04363	6.1777	•
0.075894 0.020958 -3.6212 0.0245436 0.028625 6.4546 0.02854 1.8500 0.054748 0.029594 1.8500 0.054748 0.028594 1.8500 0.035689 0.018233 -0.6303 0.015408 0.011391 0.045657 0.2495 0.054321 0.014158 3.8369 0.05431 0.014158 3.8369 0.0544201 0.014897 -4.2108 0.0467694 3.6990 0.025251 0.046569 3.6990 0.025251	-		.03382	~	•
0.245436 0.038025 6.4546 0.054748 0.029594 1.8500 0.0254748 0.029594 1.8500 0.035689 0.018233 -0.8303 0.035689 0.012620 -1.3951 0.01358 0.02495 0.054321 0.014158 3.8369 0.054321 0.014158 3.8369 0.0544201 0.016497 -4.2108 0.0569834 0.046769 3.6990 0.074553 -0.3055 0.052521 0.074553 -0.3055 0.052521	-		.02095	m	•
0.054748 0.029594 1.8500 0.031493 0.018233 -0.6303 0.035689 0.018233 -0.6303 0.015408 0.0182620 -1.3961 0.011391 0.045657 0.24955 0.0048321 0.014158 3.8369 0.0044201 0.014158 3.8369 0.0044201 0.014897 -4.2108 0.0046769 3.6990 0.004553 -0.3055 0.0025251 0.074553 -0.3055 0.0025251	۱		.03802	6.4546	•
0.011493 0.018233 -0.6303 0.035689 0.042620 -0.8374 0.0115408 0.011036 -0.8374 0.00113491 0.045657 0.24955 0.0554321 0.044128 3.8369 0.054321 0.038121 0.8752 0.0044201 0.046769 3.6990 0.074553 -0.305253 0.02553	-		.02959	1.8500	•
0.035689 0.042620 -0.8374 0.015408 0.011036 -1.3961 0.2495 0.011391 0.045657 0.2495 0.054321 0.014158 3.8369 0.044201 0.0138121 0.8752 0.0172998 0.046769 3.6990 0.046769 0.02551 0.074553 -0.302 0.052521	-	0	.01823	0	•
0.015408 0.011036 -1.3961 0.0011391 0.045657 0.2495 0.054321 0.014158 3.8369 0.05033363 0.038121 0.8752 0.0044201 0.016497 -4.2108 0.046769 3.6990 0.02553 0.074553 -0.3022 0.002553	-	o	.04262	0	•
.011391 0.045657 0.2495 0.054321 0.014158 3.8369 0.033363 0.038121 0.8752 0.044201 0.010497 -4.2108 0.098834 0.045840 2.1561 0.02521 0.074553 -0.302_0 0.	. —	o	.01103	~	•
.054321 0.014158 3.8369 0033363 0.038121 0.8752 0044201 0.010497 -4.2108 0098834 0.045840 3.1561 0172998 0.046769 3.6990 0.	-	•	.04565	0.2495	•
.033563 0.038121 0.8752 0. .044201 0.010497 -4.2108 0. .098834 0.046769 3.1561 0. .172991 0.046769 3.6990 0.	<b>,</b>	•	.01415	3.8369	•
.044201 0.010497 -4.2108 0. .098834 0.045840 2.1561 0. .172998 0.046769 3.6990 0.	-	•	.03812	0.8752	•
.098834 0.045840 2.1581 0. 172998 0.046769 3.6990 0. .022521 0.074553 -0.30	-	•	.01049	• (	•
.022521 0.074553 -0.30°.	⊣.	•	.04584	1961.7	•
	٠,	•	07456	-0.30	•

Table C.5--continued

HODEL	HODETO1		388 377	4379.665	F RATIO	33.56
DEP VAR. V	767		181	1.244577	R-SQUARE	7
VARIABLE		å	Parameter Estinate	STANDARD ERROR	T RATIO	PROB> (T)
INTERCEPT		٠,	2.499865	0.173883	14.3767	
SUPER		<b></b>	0.702693		7 (77	
V152		۰,-	-0.054103		-2.1390	.032
V156W		-	0.199995		4.3580	98
V157C		٦,	0.125747		3.5207	
V158		<b>-</b> -	-0.063227		, 0	119
V150			0.006881703		•	.605
V165					3.6048	8
V168		<b>-</b>	0.062892			95.
V169		٦.	-0.062865		900C-T-	000
7/1A		<b>-</b>	0.145133		2.6234	80
BNHS		٠.	0.049797	0.056444	0.8822	.377
OFF.		-	0.010512		0.1108	704.
HODELI	HODEL01		10 6 00 0	4011.029	F RATIO	14.65
DEP VAR: V	795		MSE	1.139821	R-SQUARE	•
VARIABLE		DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T
-04-03-17		-		16640	.153	.000
SUPER		٠,		.05040	.622	000
SACTO			-0.1258	.03906	.221	
V152				.02420	750	33
V1568		<b></b>		03418	383	017
V15/C V15/8		•		.02105	.318	.000
V159A				.04922	0.083	. 933
V160		٠ ١٠		.01274	. 321	070
V165		<b>→</b> -			179	200
9910		<b>-</b>		.04402	335	.181
V172		ı –		.01212	. 595	600.
WHS		⊶,	-0.024462	0.052944	-0.4620	0.0
BUHB		<b>→</b> -		08610	. 116	90
5		•		) ) ) )		

Table C.5--continued

D.185915 16.4930 0.0001 0.056310 6.7179 0.0001 0.043647 -0.7190 0.0001 0.043647 -0.7190 0.0001 0.058915 1.4503 0.0001 0.058915 1.4503 0.0001 0.058915 1.4502 0.1074 0.049191 -3.4917 0.0009 0.058915 1.4502 0.1074 0.049191 -3.4917 0.0009 0.0589151 1.6105 0.0009 0.0589151 -3.4917 0.0009 0.0589151 -3.4917 0.0009 0.059151 -3.4917 0.0009 0.059151 -0.1398 0.0009 0.0575175 R-SQUARE 0.0649 0.037752 0.2380 0.0001 0.037893 3.3992 0.0001 0.034897 -1.8464 0.0582 0.034897 -1.8464 0.0582 0.034897 -1.8464 0.0582 0.034897 -1.6485 0.0993 0.03197 -1.3108 0.0001 0.0318769 1.3807 0.0001 0.031813 6.5220 0.0093	<b>6</b>
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0.02752 -0.9558 0.034197 -1.8464 0.034280 2.380 0.034280 2.91197 -1.8464 0.034967 0.034967 -1.8946 0.037659 -1.6485 0.008612313 6.5220 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.037609 1.8207 0.03760	3.644742
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0.024280 2.9137 0. 0.014959 -1.3167 0. 0.0905437 -0.6496 0. 0.037459 -1.6495 0. 0.031276 -4.3187 0. 0.037609 1.8207 0.	•
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0.031276 1.3108 0.031276 -4.3187 0.008612313 6.5220 0.037609 1.8207 0.008420 0.008420	1 -0.0058817 1 -0.06175
0.031276 -4.3187 0. 0.08612313 6.5220 0. 0.037609 1.8207 0. 0.08420 0.	
0.037609 1.8207 0. 0.038371 -0.8420 0.	•
038371 -0.8420 0.	

Table C.5--continued

19.20 0.0001 0.0757	PROB> [ T	0004400	000000000000000000000000000000000000000	13.35 0.0001 0.0538 PROB>[T]	0.0001 0.0001 0.0001 0.0001 0.0019 0.0019 0.0019 0.00102
FRATIO PROBSF R-SQUARE	T RATIO	24.1155 -8.9189 5.1502 1.4251 -1.0403 -3.2047	1, 4680 -2, 1680 -3, 6298 -0, 2756 -0, 89046 -0, 89046 -0, 89046	F RATIO PROBSF R-SQUARE T RATIO	17.8409 -5.1195 -5.1195 -0.7266 -2.2927 -2.8456 -2.4225 -2.9744 -1.552
2990.69 3519 0.849869	STANDARD ERROR	, , , , , , ,	0.042503 0.042503 0.042503 0.045200 0.045200 0.045200 0.045300	4363.21 3519 1.245584 STANDARD ERROR	0.173954 0.052687 0.052687 0.053930 0.055304 0.051457 0.013024 0.015033 0.012674 0.055345 0.055345
SSE	PARAMETER ESTINATE	3.465124 -0.388152 0.173737 -0.039450 -0.094585	0.00714097 0.007140875 -0.051250 -0.010478 0.0140853 0.008038443	SSE DFB MSE MSE PARAMETER ESTIMATE	3.103487 -0.209599 0.209599 0.018385 0.058485 -0.050469 -0.01182 0.071182 -0.01182 -0.037697 -0.097415
	ä	наннан		D	
MODEL: MODELO1 DEP VAR: V98	VARIABLE	INTERCEPT SUPER SACTO V152 V156W V157C	V159A V160 V160 V169 V172 WHS BNHS OFF	MODEL: MODELO: DEP VAR: V99 VARIABLE	INTERCEPT SUPER SACTO V152 V152 V156 V156 V160 V165 V168 V168 V172 WHS BNHS

Table C.5--continued

Table C.5--continued

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27.14 0.0001 0.1038	PROB> [ T	0.0001	•	• •	•		•		•		•		33.4	•	PROB>   1	•	9,		: :	9.		4	Ģ	, 0	0.0001	99	
FRATIO PROBSF R-SQUARE	T RATIO	23.2538	5.3726	-3.8974	-6.2225	2.1903	-0.6477	-1.1014	2.7640	-4.3970	-0.9780		F RATIO	R-SQUARE	T RATIO	14.6257	10.3153	-3./650	-0.6792	6.7281	-3.8247	1.0695	2.0989	-2.4117	-5.4403	3.6054	-0.0482
3634.866 3516 1.033807	STANDARD	0.158544											3649.54	1.037961	STANDARD										0.011574		
	Parameter Estimate	3.686767	0.199975	-0.163080	-0.202640	0.102721	-0.00786515	-0.018406	0.115980	-0.221797	-0.050331			181	Parameter Estimate										-0.062969		-0.16374
	2			<b>-</b>	⊶.	<b>-</b>	⊶.	-	<b>~</b>	<b>-</b>	-	•			<u>P</u>	7	-	<b>~</b> -	۱	-		• ~	<b></b> 4 ,		•		<b>-</b>
HODEL: HODELOI	VARIABLE	INTERCEPT	BACTO	#951A	157c	268 1598	091		V169				HODEL: MODEL01	DEP VARI V102	VARIABLE	INTERCEPT	SUPER	250	395	157C	851		99	9 G	V172	WAS	

Table C.5--continued

1156902 1156902 1156902 1156902 1156902 1156902 1156902 1156902 1156902 1166902 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992 116992	PROB>F 0.0001	3559.944 3516
PARAMETER STANDARD  BSTINATE ERBOR  1	R-SQUARE 0.0946	1.012498
MODELOI  2.336117  0.24226  1.0.028781  0.018021  1.0.018021  0.0186284  0.012409  1.0.027609  0.012628  1.0.027609  0.012628  1.0.027609  0.012613  1.0.027609  0.012613  1.0.012619  0.012613  1.0.012619  0.012613  1.0.012619  0.012613  1.0.012619  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.0126118  0.01	T RATIO PROB>  T	STANDARD RRBOR
MODELO1  1	5.0977 0.0001	.156902
MODELO1  1 0.126496 0.019855 1 0.227609 0.016413 1 0.019681 0.012018 1 0.019688 0.012018 1 0.019688 0.041514 1 0.016440 0.041514 1 0.016440 0.041514 1 0.016440 0.0619920 1 0.06294 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.062217 0.029918 1 0.015255 0.06840 1 0.0158795 0.066840 1 0.0158795 0.0659418 1 0.0158796 0.056418 1 0.015879 0.065418	263	.022824
MCDELO1  1 0.237609 0.046413 1 0.136501 0.046413 1 0.106440 0.049721 1 0.0012521 0.049920 1 0.021802 0.050932 1 0.021802 0.050932 1 0.155467 0.061189 DFE ESTIMATE ERROR  1 0.105449 0.062294 1 0.105449 0.062294 1 0.10587 0.060840 1 0.10587 0.060840 1 0.115795 0.060840 1 0.115795 0.060840 1 0.115795 0.060840 1 0.115795 0.060840 1 0.018795 0.060840 1 0.018795 0.060840 1 0.018795 0.060840 1 0.018795 0.060840 1 0.018795 0.060840 1 0.018795 0.060840	052	.03226
MCDELO1  1 0.019488 0.041514  1 0.019440 0.041514  1 0.00412521 0.011431  -0.411602 0.050932  1 -0.411602 0.050932  1 -0.411602 0.061999  DFE ESTIMATE ERROR  1 2.684591 0.205671  1 2.684591 0.205671  1 0.105449 0.062294  1 0.10587 0.029918  -0.131255 0.048285  1 0.062217 0.029918  -0.1316587 0.060840  1 0.10587 0.06517540  1 0.10587 0.06517540  1 0.10587 0.06517540  1 0.10587 0.056189  1 0.015220 0.056418  1 0.015220 0.056418  1 0.015220 0.056418	200	.046413
0.019488 0.015418   0.106440 0.041514   -0.00412521 0.011631   -0.421802 0.050932   -0.411602 0.050932   -0.155467 0.061189   DFE   3516   NSE   1.739744   DFE   1.739744   D	153	.049721
MCDELO1	540	.015418
MCDELO1	603	.011431
MODELO1 88E 6116.936 V104 MSE 1.739744 NIO4 PARAMETER STANDARD DF ESTIMATE ERROR 1 0.105449 0.062294 1 0.062217 0.029918 1 0.013255 0.048285 1 0.062217 0.029918 1 0.015257 0.060840 1 0.110587 0.060840 1 0.110587 0.060840 1 0.110587 0.060840 1 0.110587 0.060840 1 0.110587 0.060840 1 0.110587 0.060840 1 0.110587 0.060840 1 0.110587 0.060840 1 0.015220 0.065175 1 0.015220 0.065418	918	.050932
PARAMETER STANDARD  DF ESTIMATE ERROR  1 2.684591 0.205671  1 0.105449 0.062294  1 0.105419 0.052918  1 0.105419 0.059918  1 0.110587 0.029918  1 0.110587 0.029918  1 0.110587 0.050918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.110587 0.056918  1 0.015220 0.056418  1 0.015220 0.056418		
PARAMETER STANDARD  ESTIMATE ERROR  1 2.684591 0.205671 1 0.105449 0.062294 1 -0.132255 0.048285 1 -0.134026 0.054281 1 -0.14494 0.042246 1 0.115795 0.060840 1 -0.18795 0.065175 1 -0.18331 0.054418 1 0.033567 0.054418 1 0.033552 0.065443		930
DE ESTIMATE ERROR  1 2.684591 0.205671 13.0 1 0.105449 0.062294 1.6 1 0.132255 0.062294 1.6 1 0.052217 0.052994 1.6 1 0.015494 0.062294 1.6 1 0.015754 0.054281 -2.4 1 0.015795 0.0560840 1.9 1 0.015795 0.0560840 1.9 1 0.015795 0.0560840 1.9 1 0.015795 0.0560840 1.9 1 0.015795 0.0560840 1.9 1 0.015795 0.0560840 1.9 1 0.015795 0.056889 1.9 1 0.015350 0.054418 2.0 1 0.033507 0.014985 2.3		. 739744
2.684591 0.205671 13.0 1 0.105449 0.062294 1.6 1 0.062217 0.029918 -2.7 1 -0.041494 0.054246 -0.9 1 0.115595 0.056027 4.2 1 0.115795 0.056027 4.2 1 -0.016083 0.015754 -1.0 1 0.015220 0.055175 -2.8 1 0.035007 0.014985 2.3 1 0.033507 0.014985 2.3	T RATIO PROB>(T)	STANDARD ERROR
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	2363	
-0.087019 0.066763 -1.3	5.0973 0.	
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Table C.5--continued

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	PARA ETER Est./ATE		-0.24438 0.13422 0.055923 0.025026 -0.186280 -0.206486 -0.099176 0.076390 -0.00805092 0.223713	SSE DFE MSE Parameter	ESTIMATE	3.605325 0.337493 -0.124696 -0.124696 0.1153124 -0.153191 -0.153191 -0.179135 -0.179139 -0.179129 -0.179129 -0.179129 -0.015290 -0.179129 -0.015290 -0.015290 -0.015290 -0.015290 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0.055200 -0
	à	AAAAA,			ğ	<b>делегенелегене</b>
MODEL: MODELO1 DEP VAR: V105	VARIABLE	INTERCEPT SUPER SACTO V152 V156W	V157C V158 V158 V160 V168 V172 WHS BWHS	MODEL: MODELO! DEP VAR: V106	VARIABLE	INTERCEPT SUPER SACTO V155 V156 V156 V158 V169 V169 V169 V172 WHS

Table C.5--continued

17300	HODEFOI		200 200 200	2926.653	F RATIO	9.50
DEP VAR	V107		M 998	0.832381	R-SQUARE	038
VARIABLE		à	Parameter Estimate	STANDARD	T RATIO	PROB>   T
INTERCEPT SUPER	F+	~~	5893 1545	.14226	358	.719
SACTO V152			-0.237731	0.033399	-7.1179	0.0001 0.1255
V1568			2015	.02922	689	
V159A V159A			3600	.04208	231	.007
V165		٠,	5161	.04508	145	222
V168			5422	03764	2	159
V172 WHS			3529 1946	.01036 .04526	35	.667
BNHS OTH			7896 5978	.04618	124	
MODEL	MODETO1		88 CO	3297.257	F RATIO	7.40
DEP VAR:	V108		NSH	0.937787	R-SQUARE	0.0306
VARIABLE		DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>  T
INTERCEPT	•	٦.	.66750	15100	17.6653	0.0001
SACTO			0.15865	03545	-4.4753	0.0001
V156W		<b>-</b>	.09238	03985	2.3181	0.0205
V157C V158			.03333	.03101 .01910	1.0748	0.2825 0.0259
V159A			0.06103	04466	-1.3664	0.1719
V165		٠ ١	03988	04785	0.8334	0.4047
V168 V169			.03946	.03995	0.9877	0.3233
VI72		<b></b>	15069	01100	-3.9752 3.1367	0.0001
BNHS			0.067823	0.049017	1.3837	0.1665
;		ı	) ) )	; ; ;		

Table C.5--continued

HODEL: HODELO?		1960 1970	3500.086 3516	F RATIO	11.18
DEP VARI V109		201	0.995474	R-SQUARE	•
VARIABLE	40	Parameter Estinate	STANDARD	T RATIO	PROB>   T
INTERCEPT	, mi	2.391633	0.155577	15.3726	0.0001
SOPER		-0.144085		3.91	
V152		-0.071639	0.022631	.165 .578	o a
V157C		0.125956		3.941	9.
V158	<b></b> -	-0.087343		536	. v.
V150		0.011191		0.939	
V165	<b></b>	0.045404		. 921 . 168	70
V169 V169		0.056119		363	
V172	٦.	-0.042183		721	7
PAHS	-11	-0.026082		. 516	
OTH	· ~	-0.058058		.721	₹;
HODEL: HODELO1		M (0)	3240.664	F RATIO	
DEP VAR: V110			0.921691	R-SQUARE	0.0349
VARIABLE	DF	Paraheter Estimate	STANDARD	T RATIO	PROB>  T
	_	78426	.14970	598	
SUPER	·	13831	.04534	250	
SACTO	٦,	0.16367	.03514	557	
V152 V156W		.13765	.03950	3.484	
V157C	٦.	0.01092	.03074	355	
V159A	<b></b>	0.11740	.04428	2.651	
V160		.01328	.01146	800	
V168 V168	٠.	0.06243	.01471	1.24	
V169	٠.	0.12102	.03960	3.055	
VI72 WHS		.02521 003607	.04762	075	
BNHS		0.048203 -0.132362	0.048594 0.077463	0.9919	0.3213 0.0876

Table C.5--continued

HODEL: MODEL01	_	10 E	644.689699	F RATIO	5.59
DEP VAR: RSM1		MSM MSM	0.186596	R-SQUARE	0.0237
VARIABLE	à	Parameter Estimate	STANDARD	T RATIO	PROB>[T
INTERCEPT	~.		0.067946	4.4709	0.0001
SACTO	<b>-</b>	0.00479528	0.020380	0.3541	
V152	-	-0.02856	0.009683775	-2.8899	9
V156W	<b>~</b>	0.032741	0.017932	1.8258	9
V157C		0.03099	•	2.2208	5,0
V158	<b>-</b>	-0.00282	•	-0.1408	; 8
V160	·	0597519	0.005204489	0.1148	8
V165	<b>~</b>	-0.03031	•	-1.4091	<u>.</u> ;
W168	·	0300872	0.006676707	4506	ي ج
V172	۰.	0.020644	0.004950393	4.1702	38
EH3	· ~	-0.016627	:	-0.7691	=
BNHS		-0.056527	0.022056	-2.5629	9
OTH	-	-0.033501	0.035159	-0.9528	0.3407
	_	9	4 6 6 3 4	6	,
MUDELI MUELUI	_	220	34	PROB>F	0.0014
DEP VAR: RSN2		HSE	0.176138	R-SQUARE	010
		PARAMETER	STANDARD		
VARIABLE	ď	ESTIMATE	ERROR	T RATIO	PROB>   T
INTERCEPT	~	0.962782	0.066015	•	0.0001
SUPER	<b>~</b>	0.017376	.01999	. 869	0.3849
SACTO	⊸,	-0.027975	0.01549	900	0.0712
751A	- ۱	0.01050	0.005602791	966	0.621
V157C	•	-0.039151	.01356	887	0.0039
V158	-	ĕ	835395	798	0.4246
V159A	_	ŏ	0.01952	.237	0.8120
V160	<b>~</b>	ĕ	505653	530	0.5959
V165	⊸.	ġ,	0.02092	.224	0.8224
V168	<b>→</b> -		648689 61746	200	0.1041
V172	٠.	-0.014442	480965	007	0.0027
WHS	· ~	•	•	-1.2639	0.2064
BNHS	٦,	-0.00629304	.02142	. 293	0.7690
HIO HIO	7	/ nencn . n -	.03416	481	0.1380

Table C.5--continued

15.20 0.0001 0.0619	0.000000000000000000000000000000000000	PROBY   4.14 0.00177 0.0021 0.0021 0.0021 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418 0.1418
<b>26</b> 1	1.05091 1.05091 1.05091 1.05091 1.05091 1.05091 1.05091 1.05091 1.05091 1.05091 1.05091	F RATIO PROB>F R-SQUARE T RATIO -0.1734 -0.1943 1.4694 1.4694 1.0312 -1.1907 0.6568 3.3507 0.3742 0.3742 0.3742 0.3742 0.3742
494.401517 3455 0.143097 STANDARD	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	458.025216 0.132569 0.132569 STANDARD ERROR 0.01346 0.0073416 0.013691 0.007247481 0.004366796 0.004366796 0.004366796 0.00562771 0.00562771 0.00562771 0.00562771
Ai T	0.493726 10.0018074 10.0018074 10.0018074 10.0018078 10.0018078 10.0018078 10.0018078 10.0018078 10.0018078 10.0018078 10.0018078 10.0018078 10.0018078	PARAKETER ESTINATE CO. 00992953
107		Q
MODEL: MODELO1 DEP VAR: RSN3	VARIABLE UNTERCEPT SUPER SACTO VISS VISS VISS VISS VISS VISS VISS WHS BANES	MCDEL: MCDELOI DEP VAR: RSN4 VARIABLE INTERCEPT SUPER SACTO V152 V155 V155 V156 V159 V169 V169 V172 WHS BNHS CTH

Table C.5--continued

5.62 0.0001 0.0238 PROB>   T	0.000000000000000000000000000000000000	PROB - 129 0.0001 0.01001 0.1755 0.1755 0.1755 0.1755 0.1267 0.1567 0.1567 0.01264 0.0164 0.0164
F RATIO PROBSF R-SQUARE T RATIO	1.2000000000000000000000000000000000000	FROBYE R-SQUARE R-SQUARE -0.9284 -0.9284 -0.9385 -0.93865 -0.93865 -0.93865 -0.93865 -0.93865 -0.93865 -0.93865 -0.93865 -0.93865 -0.5957 -1.55155 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627 -0.1627
802.199301 3455 0.232185 STANDARD ERROR	0.075794 0.022956 0.017794 0.017794 0.01003 0.01003 0.015568 0.02421 0.0058134 0.0058134 0.00582115 0.005822115	226.070464 3455 0.065433 STANDARD ERROR 0.00246156 0.005852877 0.005852877 0.008264641 0.008264641 0.008264641 0.008264641 0.003981780 0.003081944 0.003953747 0.002931475 0.002931475 0.002931475
SSE DFE MSE PARAMETER ESTIMATE	0.166728 0.035902 0.0588602 0.0688602 0.019486 0.019423 0.047180 0.047180 0.061374 0.016336 0.016336 0.016336 0.016336	SSE DFE PARAMETER -0.037356 -0.016512 -0.016512 -0.0165247 0.0165247 0.01662947 0.01682947 0.001829947 0.001829947 0.001829947 0.00173257 -0.00173254 -0.0017384
å		<u> </u>
MODEL: MODELO1 DEP VAR: RSN5 VARIABLE	INTERCEPT SUPER SACTO V152 V156W V156W V158 V159A V165 V165 V169 V172 WHS	MODEL: MODEL01 DEP VAR: RSN6 VARIABLE INTERCEPT SUPER SACTO V152 V152 V153 V159 V159 V169 V169 V172 WHS BNHS GTH

Table C.5--continued

	MODEL: MODEL01		388 380	517.381350	F RATIO	7.90	
PARAMETER  CEPT 1 0.002544989 1 0.002544989 1 0.0021787 0.0 1 0.001460428 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.0017617 0.0 1 0.	_		100	0.149749	R-SQUARE	0.0332	
CEPT 1 0.002544989 0.002544989 0.002544989 0.002544989 0.002534 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.002544989 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00254498 0.00	IABLE	ă	Parameter Estinate	STANDARD ERROR	T RATIO	PROB>   T	
REPT 1 0.0024104 0.0    0.00146428	ERCEPT.			0.060869	3.3401	0.0008	
NR: RONE  PARAMETER  PARAMETER  PARAMETER  PO.0012819 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0  10.0012810 0.0	12	٠,			1.8008	.071	
NR: RSN8  NCDELOI  1 0.001480428  1 0.0020099 0.0  1 0.001557409 0.0  1 0.00109301  1 0.00109301  1 0.00109301  1 0.002410435  1 0.002410435  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002519856  1 0.002410431  1 0.0026189  1 0.0026189  1 0.0026189  1 0.0026189  1 0.00251991  1 0.0026189  1 0.0026189  1 0.0026189			0.021787	٠.	2.4607	700	
NR: RSN8  NR: RSN8  D. 001255409 0.0  1 0.00125109 0.0  1 0.0012950 0.0  1 0.00109301  DFE MSE 18  NSE 18  NSE 19  0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.00261159 0.0  1 0.00261159 0.0  1 0.00261159 0.0	:2	-			0.1184	905	
NR: RSN8  NR: RSN8  D. 0.01557409 0.0  1		<b>~</b> .	0.020009	٣.	2.5976	. 009 0.09	
NR: RSN8  DE ESTINATE  RODELO1  1 0.001557409 0.0  1 0.00109301  1 0.0013960  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002410431  1 0.002511951  1 0.0050159	<b>₹</b> .	<b>-</b>		٦.	-1.7797	.075	
NR: RSN8  NR: RSN8  DFE  DFE  DFE  DFE  DFE  DFE  DFE  DF		-			-2.3531	.018	
NR: RSN8  1	_	٦.		٦	0.2604		
NR: RSN8  NR: RSN8  DFE		<b></b>	0.042435	•	2.0349		
NR: RSN8  NR: RSN8  DEE DEE MSE 15  NSE 15  NSE 16  NS	•	- ۱		•	-0.0564	955	
AR: RBN6  BLE DF ESTIMATE  PARAMETER  BLE DF ESTIMATE  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.002410431 0.0  1 0.00251951 0.0  1 0.00506159 0.0  1 0.00506159 0.0  1 0.005075976 0.0  1 0.005075976 0.0	-	• •		0.019759	2.3261	.020	
NR: RSNS  BLZ  BLZ  BLZ  BLZ  DF  ESTINATE  1 -0.00695263  1 0.005519856  1 0.005519856  1 0.005519857  1 0.005519857  1 -0.000128472  1 -0.000128472  1 -0.000128472  1 -0.000128472  1 -0.00179292  1 -0.00179292  1 -0.0056189  1 0.00551951  1 0.0056189  1 0.0056189  1 0.0056189  1 0.0056189  1 0.0056189		-	0.073386	0.031497	2.3299	.019	
NODELO1 SSE DEE NR. RSN8 MSE NSE NSE NSE NSE NSE NSE NSE NSE NSE N	• • • • • • • • •	!					
DFE NR: RBN8 MSE NR: RBN8 MSE NS: MSE			388	2	F RATIO	2.29	
PARAMETER  BLE DF ESTINATE  CEPT 1 -0.00695263  1 0.005519856 0  1 0.005519856 0  1 0.005519857 0  1 -0.001284734 0  1 -0.001284792 0  1 -0.00178592 0  1 -0.00178592 0  1 -0.00178592 0  1 -0.00178978 0  1 0.0056189 0  1 0.0056189 0  1 0.0056189 0  1 0.0056189 0  1 0.0056189 0				3455	PROB>F	0.0033	
PARAMETER  ESTINATE  ESTINATE  1 0.00595263  1 0.0054359  1 0.005419431  0 0.005419431  1 0.005419431  1 0.005419431  1 0.00541953  1 0.00241951  1 0.002571951  1 0.002571951  1 0.002571951  1 0.002571951  1 0.004698971  1 0.005075976  1 0.005075976	VAR			0.044260	R-SQUARE	500	
1 0.00551951 1 0.005519856 0 1 0.005519856 0 1 0.005519856 0 1 0.00561311 0 1 0.005613159 0 1 0.00561311 0 1 0.0056131951 0 1 0.0056159 0 1 0.0056159 0 1 0.0056159 0 1 0.0056169 0 1 0.0056189 0 1 0.0056189 0	ABLE	DF	Parameter Estinate	STANDARD ERROR	T RATIO	PROB-   T	
1 0.0054579 1 0.005519856 0 1 0.005619856 0 1 -0.005643259 1 -0.000128473 0 1 -0.00278292 0 1 0.002789292 0	RCEPT	-		0.033092	-0.2101	.833	
1 0.005519856 0 1 0.002410431 0 1 0.002410431 0 1 0.00241359 0 1 0.0024359 0 1 0.00279292 0 1 0.00279292 0 1 0.00279292 0 1 0.00267895 0 1 0.005078991 0 1 0.005078991 0	E	-	0.024579	0.010023	2.4523	10:	
1 0.002410431 0 1 0.002413259 0 1 0.003043259 0 1 0.003128432 0 1 0.00279292 0 1 0.00279292 0 1 0.00279292 0 1 0.00279292 0 1 0.00279292 0 1 0.00279292 0 1 0.00257951 0 1 0.005075976 0	2	<b></b>			0.7105	. 177	
1 -0.00364534 1 -0.00364534 1 -0.00364534 1 -0.00379292 1 -0.00279292 1 -0.00279292 1 -0.00279955 0 0.00267955 1 0.004698971 1 -0.005078976 1 0.005078976		٠,	0.002410431		0.5007	979	
1 -0.00128472 1 -0.00178472 1 -0.001782872 1 0.00278282 0 0.0026185 1 0.0056185 1 0.0056185 1 0.0056185 1 0.0056185	<b>*</b> (	٦-	0.005043639		-0.5363	200	
1 -0.00279292 0 1 -0.00279292 0 1 0.002571951 0 1 -0.005061951 0 1 0.00507886 0 1 0.005078971 0 1 -0.005078976	_ د	- ۱	-0.000128472		-0.0307	975	
1 -0.00276955 0 1 0.002571951 1 -0.0025786 0 1 0.025786 0 1 0.004698971 0 1 -0.005075976	4	, ,	-0.00279292		-0.2853	.775	
1 0.002571951 1 -0.00506159 0 1 0.0025786 0 1 0.004698971 0 1 -0.005075976 1 -0.005075976		<b>-4</b> ·	-0.00276955		-1.0926	.274	
1 -0.00506159 U. 0.00506159 U. 0.0050780 U. 0.005075976 U. 0.0050759 U. 0.00		٠,	0.002571951		0.2453	908:	
1 0.004698971 0 1 0.005075976 1 -0.005075976		<b></b>			2.9450	003	
1 0.005075976 1 -0.00326182		٠.			1.9490	.051	
1 -0.00326182		٦,		0.010529	0.4821	٠ŗ	
0.02020			-0.00326182 6.020820	0.010/42	1.2159	0.2241	

Table C.5--continued

######################################	MODELO1	SSE 78 DFE MSE	786.348631 3455 0.227597	F RATIO PROB>F R-SQUARE	9.69 0.0001 0.0404
0.075041 6.9284 0.022726 -0.2839 0.010916 0.7336 0.015414 -2.5586 0.015414 -2.5586 0.01542 1.7509 0.0237854 -4.8756 0.024359 -1.1750 0.024359 -2.1221 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.038300 TRATIO PR ERROR TRATIO PR 0.03831475 -0.7476 0.005587435 -0.7476 0.005835418 -0.7476 0.005835418 -0.3318 0.00331049 -0.3318 0.003315312 0.3318 0.003375312 0.33418 0.0016375 -0.07381	PARAMETER DF ESTIMATE		STANDARD KRROR		PROB> [T]
0.010916 0.019805 0.019805 0.019805 0.023780 0.023780 0.023780 0.023780 0.023875 0.024359 0.024359 0.024359 0.024359 0.024359 0.024359 0.024359 0.024359 0.024359 0.024359 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.04498 0.	•		0.075041	6.9284	0.0001
0.015414 -2.5586 0.09496202 -0.8011 0.05747915 -1.7909 0.0237854 -4.3858 0.024359 -1.3858 0.024359 -2.1821 0.024359 -2.1221 0.024359 -2.1221 139.921242 FRATIO 0.038830 -2.1221 0.038830 -2.1221 0.0404573 -0.7476 0.0464573 -0.7476 0.0464573 -1.4207 0.00551855 -1.3208 0.00424625 -1.3234 0.00316249 -0.3418 0.0031049 -0.3418 0.0031049 -0.3418 0.0031049 -0.3418 0.0031049 -0.3418 0.0031049 -0.3418 0.002306249 -0.7260 0.01275 -0.9281	1 0.008007774		0.010916	0.7336	0.4632
0.022198 1.7909 .005747915 -1.1750 .007373854 -4.8756 .0054672875 0.84623 0.024359 0.84623 0.024359 0.84623 0.024359 0.86423 0.024359 0.8160 0.0236242 FRATIO PR ERROR R-SQUARE 0.040498 R-SQUARE 0.040498 -0.1023 0.0443475 -1.4207 0.04644573 0.1023 0.0431445 -1.3208 0.0443445 -1.3208 0.05581418 -0.1444 0.05011049 0.0143 0.011049 0.0311 0.02306249 0.7260 0.016380 1.3095 0.016380 1.3095 0.016380 1.3095	•	0	0.015414	-2.5586 -0.8011	0.0106 0.4231
0.0237854 -4.3858 0.0237854 -4.3858 0.024359 0.8165 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.024359 0.8160 0.038830 -2.1221 0.040888 R-SQUARE STANDARD T RATIO PR 0.031654 0.1023 0.031654 0.1023 0.04644573 0.1023 0.04644573 0.1023 0.04646573 0.1023 0.0431475 -1.4207 0.0464625 1.3234 0.0031049 0.0331 0.010031 0.0331 0.010031 0.0331 0.010031 0.0331 0.010031 0.0331 0.010031 0.0331 0.010071 -0.7381 0.010071 0.01395	•	•	0.022198	1.7909	0.0734
0.019855 0.02467287 0.024359 0.024359 0.024359 0.038830 0.04498 0.040498 0.040498 0.040498 0.040498 0.004485 0.004485 0.00587435 0.00587435 0.00587435 0.004331475 0.0043318 0.00433149 0.00835418 0.00835418 0.004331 0.004331 0.00331 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049 0.003311049			0.023780	0.1546	0.8772
0.024675 0.023675 0.0236830 0.036830 0.036830 0.040498 STANDARD ERROR 0.031654 0.005687435 0.007431475 0.009587435 0.009587435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.009687435 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875312 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.0096875485 0.		•	0.019855	4.8756	0000
0.024359 0.8160 0.038830 -2.1221 139.921242 F RATIO 3.455 R-SQUARE 0.040498 TATIO PR 0.031654 0.1023 0.00583435 -0.7476 0.04644573 0.3699 0.00835418 1.5590 0.00835418 -0.398 0.004005753 0.0143 0.00406501955 0.0143 0.0031049 -0.3418 0.0031049 0.0331 0.0031049 0.0331 0.002306249 0.7260 0.010071 -0.7381 0.010275 1.3095			0.023875	3.3465 0.8423	0.3997
139.921242 FRATIO 0.040498 R-SQUARE STANDARD TRATIO PE 0.031654 0.1023 0.031654 0.7476 0.04604573 0.3699 0.00835418 1.5590 0.00835418 1.5590 0.00835418 -0.1398 0.004065753 0.0143 0.009363691 2.1144 0.009363691 -0.3418 0.010031 -0.3418 0.010031 0.7260 0.010071 -0.7260 0.010375 1.3095	1 0.019877		0.024359	0.8160	0.4146
STANDARD  ERROR  0.031654 0.1023 0.009587435 0.004604573 0.00635418 0.00635418 0.00501955 0.0143 0.005010553 0.0143 0.00511049 0.00311049 0.0031049 0.0031049 0.0031049 0.0031049 0.0031049 0.0031049 0.0031049 0.0031049 0.0031049 0.0031049 0.0031049 0.00311	MODELO1 8SE	13	9.921242	F RATIO PROB>F	45.
0.031654 0.1023 0.09587435 -0.7476 0.004031475 -1.4207 0.00404673 0.3699 0.00835418 1.5590 0.00835418 1.5590 0.00835418 1.5590 0.0083553 0.0143 0.009363625 -1.3208 0.010031 1.3234 0.010031 0.0331 0.010071 -0.3418 0.010071 -0.3418 0.010071 -0.3418	PARAME		STANDARD		
0.031654 0.1023 .009587435 -0.7476 .007431475 -1.4207 .00464673 0.3699 .006501955 -0.1398 .004005753 0.0143 .009363691 2.1144 .002424625 -1.3208 0.011049 -0.3418 .008375312 0.7260 0.010071 -0.7381 0.016380 1.3095	DF ESTINATE		ENROR		PROB>   T
.007431475 -1.4207 .004604573 0.3699 0.006501955 0.398 .004005753 0.0143 .009363691 2.1144 .0052464625 1.3234 0.00311049 -0.3418 .008375312 0.0331 .002306249 0.7260 0.010071 -0.7381 0.016380 1.3095	1 0.003238286	0.0	0.031654	0.1023	0.9185
0.0046045/3 0.3699 0.00455418 1.5590 0.004501955 -0.1398 0.00424625 -1.3204 0.010031 1.3234 0.0031049 -0.3418 0.00310512 0.7361 0.010071 -0.7381 0.016380 1.3095		0.0	07431475	-1.4207	0.1555
.006501955 .004005753 .009363691 .002424625 .0.010031 .0.0311049 .0.08375312 .0.03306249 .0.010071 .0.010275 .0.016380 1.3095		9.0	046045/3	1.2049	0.7115
.009463591 2.0143 .002424625 2.0144 .002424625 -1.3234 0.00311049 -0.3418 .008375312 0.0331 0.010071 -0.7381 0.010375 -0.9281	1 -0.000909147	0.0	06501955	-0.1398	0.8888
.002424625 -1.3208 0.010031 1.3234 0.00311049 -0.3418 .008375312 0.0331 0.010071 -0.7381 0.010275 -0.9281 0.016380 1.3095		90	09363691	2.1144	0.0345
0.010031 1.3234 0.00311049 -0.3418 .008375312 0.0331 .002306249 0.7260 0.010275 -0.9281 0.016380 1.3095		0	02424625	-1.3208	0.1867
0.00311049 0.003375312 0.03306249 0.010071 0.010275 0.016380 1.3095		•	0.010031	1.3234	0.1858
.002306249 0.7260 0.010071 -0.7381 0.010275 -0.9281 0.016380 1.3095		5	00311049	0.0331	0.9736
-0.7381 -0.9281 1.3095		Ö	02306249	0.7260	0.4679
1.3095		_	0.010071	-0.7381	0.4605
			0.016380	1.3095	0.1905

Table C.5 -- continued

MODEL	MODEL 01		## BB C	146.401457	F RATIO	4.07	
DEP VAR	RSM11			-	R-SQUARE	0.0174	
VARIABLE		à	Parameter Estimate	STANDARD ERROR	T RATIO	PROBY   T	
INTERCEPT	•		0.040367		1.2467	0.2126	
SACTO		٠	0056842	.00760161	0.717	0.4547	
V152		⊶.	-0.01313	.00470999	. 789	0.0053	
V156W		<b>-</b>	12625	.00665081	388	0.0007	
V158		<b>~</b>	0.0030689	.00409746	719	0.4539	
V159A		<b></b>	.00320485	0.009578069	334	0.7379	
V165		-	0.01085	0.01026	.057	0.2903	
V168		-	20825	.00318170	69.	0.4877	
V169		<b>-</b> -	-0.02377	0.008567061	.775	0.000.0	
1 X		<b>-</b>	-0.02571	0.01030	495	0.0126	
BAHS		-	32825	0.010511	2.688	0.0072	
or TH		-	-0.0056193	0.016755	. 335	0.7374	
MODEL	MODEL 01		188	451.203309	F RATIO		
DEP VAR	RSN12		asu War	3455	PROB>F R-SQUARE	0.0194	
			PARAMETER	STANDARD			
VARIABLE		D.	ESTIMATE	ERROR	T RATIO	PROB> [T]	
INTERCEPT	F	-	0.205469	0.056843	3.6147	000	
SUPER			0.019835	0.017217	1.1521	200	
V152			0432772	0.008268631	0.0523	958	
V156W		-	0.0089158	0.015002	-0.5943	. 552	
V157C		<b></b> -	0.022830	0.011676		0.0506	
V159A		· ~	-0.024333	•	-1.4471	148	
V160		<b>~</b>	0 109235485	0.004354005	2.1211	.034	
V165		7	. JO153911	•	0.0854	.931	
V168		<b>-</b>	0.017709	0.005585642	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	500	
V109		<b>-</b>	-0.012499	0.004141431	-3.0180	007	
VHS		·	0.014299			429	
BNHS		<b>~</b> .	-0.016629	0.018452	-0.9012	.367	
H.C		4	0.02040	0.029414	1016.0	. 333	

Table C.5--continued

PARAMETER ESTIMATE  T 1 2.610558 1 0.0004827872 1 0.0004827872 1 0.0004827872 1 0.001348 1 0.015527 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998 1 0.0316998	EL: MODELO:	70	888 1990 1980 1980 1980 1980 1980 1980 1	6576.383 3516 1.870416	FRATIO PROB>F R-SQUARE	13.86 0.0001 0.0558
1		Ö		STANDARD ERROR		PROB>   T
0.00477937	<b>#</b>		0	0.213256 0.064591 0.050066	12.2415 6.2501 0.0096	0.0001 0.0001 0.9923
1 -0.077138			,	0.031021 0.056282 0.043804	0.1540 0.4026 2.3137	0.8776 0.6873 0.0207
0.037107 0.067579 0.5491 0.5491 0.093660 0.056425 2.6123 0.056425 2.6123 0.056425 2.6123 0.056425 2.6123 0.0569225 4.0480 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.4388 0.0569225 2.0710 0.059647 0.048115 -2.0710 0.054089 0.042087 0.18673 0.056699 0.012698 0.025935 -2.1235 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.015698 0.016932 0.054225 -2.1235 0.056699 0.014932 -3.7952 0.0156699 0.016049 2.6805 0.015698 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.016049 2.6805 0.0				0.026987	-2.8583 -1.8313	0.0043 0.0671
0.147399 0.056425		4 544 544 1		0.067579	0.5491	0.5830
MODELO1 SSE 6073.76 F RATIO 75 F				0.056425 0.015537 0.067850	-3.9269 -8.8027 	0000
PARAMETER STANDARD T RATIO PROBLE O. 595216 PARAMETER STANDARD T RATIO PROE O. 595216 0.052073 9.5889 0.059547 0.059647 0.0596812 -0.059647 0.054089 0.054089 0.054089 0.054089 0.054089 0.055935 -0.051860 0.055935 -0.051865 0.055935 -0.051865 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.056669 0.0540845 1.6635 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.065205 9.3859 0.052099 0.065207 5.02989 0.052099 0.056509 0.056507 5.02989 0.054086 0.054086 0.054086 0.056089 0.056089 0.056089 0.056089 0.056089 0.056089 0.056089 0.056089 0.054086 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089 0.054089		1.7		0.110350	2.4388	0.0148
PARAMETER STANDARD T RATIO PROE ESTINATE ERROR T TATIO PROE ESTINATE ERROR T TATIO PROE 1 1 2.581762 0.204944 12.5974 0.595218 0.062073 9.5869 0.062073 1 -0.0199647 0.062073 -2.0710 0.010096647 0.0629812 -0.3657 0.007604489 0.062997 -1.8537 0.007604489 0.062997 -1.8537 0.007604489 0.062997 -1.9996 0.010899 0.065298 0.3285 0.01089945 1.6635 0.3285 0.01089945 1.6635 0.01089945 1.6635 0.01089945 1.6635 0.01089945 1.6635 0.01089945 1.6635 0.01089945 1.6635 0.01089945 1.6635 0.0108996 0.06527 5.0298 0.0108049 2.6805 0.0108049 2.6805	1	010	SSE	6073.76 3516 1.727463	F RATIO PROB>F R-SQUARE	000
1 2.581762 0.204944 12.5974 0.65218 0.062073 9.58894 0.6595218 0.062073 9.58899 0.6595218 0.062073 9.58899 0.6595218 0.054089 -1.8577 0.054089 -1.8577 0.054089 -1.8577 0.054089 0.025935 -1.9996 0.025935 0.025935 0.025935 0.025935 0.025935 0.025935 0.025935 0.025659 0.025698 0.025698 0.025698 0.025698 0.025698 0.025698 0.025699 0.054225 -0.3816 0.054225 0.054225 0.054225 0.055205 9.3859 0.065227 5.02988 0.065227 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.054266 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.066527 5.02988 0.0666527 5.02988 0.0666527 5.02988 0.0666527 5.02988 0.0666527 5.0		Ö		STANDARD ERROR	RATI	PROB>[T]
-0.099647 0.048115 -2.0710 0.010902 0.029812 -0.3657 0.050812 -0.3657 0.050826 0.055935 -1.8537 0.050825 -1.8996 0.025935 -1.9996 0.025935 -1.9996 0.025137 0.015698 0.03585 0.0168175 0.015698 0.03285 0.056659 0.05635 0.056659 0.05635 0.05659 0.05635 0.03816 0.056557 5.03816 0.055265 0.056527 5.03816 0.055265 0.03816 0.034614 0.065527 5.03988 0.0384266 0.056527 5.03988 0.056654	ţ.		2.581762		12.5974 9.5889	
0.007604489 0.054089 -1.8537 0.007604489 0.042097 0.1806 0.1806 0.025935 -1.8996 0.0051235 0.055089 0.055089 0.055089 0.055089 0.055089 0.055089 0.055089 0.055089 0.055089 0.055089 0.055089 0.055089 0.055205 9.3816 0.055205 0.055209 0.06527 5.0298 0.055205 0.0284266 0.106049 2.6805 0.0508					-2.0710 -0.3657	
-0.051860 0.025935 -1.9996 0.00128739 0.015698 0.3285 0.02051757 0.015698 0.3285 0.020691 0.020139 7.2088 0.020691 0.05425 -0.3816 0.020691 0.06525 -3.7952 0.0312049 0.06527 5.02988 0.026426 0.106049 2.6805 0.0050649			0		-1.8537 0.1806	
0.005157157 0.015698 0.3285 0. 0.108034 0.064945 1.6635 0. 0.145175 0.020139 7.2088 0. -0.020691 0.054225 -0.3816 0. -0.056669 0.014932 -3.7952 0. 0.61209 0.065205 9.3859 0. 0.334614 0.066527 5.0298 0.		6-4 pm			-1.9996 -2.1235	
0.145175 0.020139 7.2088 0.020691 0.054225 -0.3816 0.054225 -0.3816 0.056669 0.014932 -3.7952 0.0053205 9.3859 0.334614 0.066527 5.0298 0.0284266 0.106049 2.6805 0.005049		• ~ ~	0		0.3285	
0.056691 0.014932 -3.7952 0.014932 -3.7952 0.065205 9.3859 0.066527 5.0298 0.066527 5.0298 0.066527 5.06805 0.06649					7.2088	
0.334614 0.066527 5.0298 0. 0.284266 0.106049 2.6805 0.		- P-			-3.7952 9.3859	
		-			5.0298 2.6805	

Table C.5--continued

### SQUARE  ### SQ	MODEL: NO	HODET 01		11 SEC.	57 <b>68</b> .39	F RATIO	18.27
PARAMETER STANDARD T RATIO PROE STANDARD T RATIO PROE STANDARD T RATIO PROE STANDARD T S. 472109 0.200072 12.3561 0.0052401 0.0053403 0.05734 0.00551406 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0551403 0.0	VAR	16		NSH NSH		R-SQUARE	0.0723
0.0514711   0.200072   12.3561   0.05014711   0.029103   0.17591   0.0514711   0.029103   0.17591   0.0514711   0.029103   0.17591   0.0514711   0.029103   0.17591   0.015105   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805   0.051805	IABLE		ă	Paraceter Estimate	STANDARD		PROB>   T
0.051920   0.029103   0.05911   0.05911   0.059103   0.05791   0.05147111   0.059103   0.05791   0.055195   0.055198   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199   0.055199	TERCEPT			2.472109	.20007	12.3561	• •
0.005147111	12			-0.027203	.04697	-0.5791	
1	~		٦.	.00514711	.02910	0.1769	•
1			<b>-</b> -	0.021406	00170	2.4600	
0.059183	, .		۱	-0.055195	.02531	-2.1800	
0.117109   0.054401   1.074491   0.054401   1.0244   0.05429   0.014577   -3.4138   0.014577   -3.4138   0.014577   -3.4138   0.014577   -3.4138   0.0134876   0.014577   -3.4138   0.0134876   0.014577   -3.4138   0.0134876   0.016555   0.054945   2.0768   0.0134876   0.016528   0.0559946   0.054945   0.5959   0.016989   0.103528   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0.5959   0	<b>V</b> 6		٦.	-0.060803	.05918	-1.0274	•
0.085494   0.019660   4.3486   0.054229   0.052936   1.0244   0.054229   0.052936   1.0244   0.05702396   1.0244   0.05702396   1.0244   0.05702396   1.0244   0.05702396   1.0244   0.0570238   0.053528   0.053528   0.053528   0.055589   0.055589   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.055599   0.0	<b>.</b>		<b>→</b> -	0.011109	76510.	1 8491	
0.054229 0.052936   1.0244   0.0576858   0.0649455   0.06422   0.0576858   0.0649455   0.0522   0.0576858   0.0649455   0.05529   0.057689   0.0649455   0.05959   0.0649455   0.05959   0.0649455   0.05959   0.0649455   0.064945   0.05959   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945	n ee		•-	0.085494	.01966	4.3486	
0.049762   0.014577   -3.4138   0.0576858   0.064365   9.0622   0.0134676   0.064365   9.0622   0.0134676   0.064365   9.0622   0.0134676   0.064365   0.05959   0.067858   0.067858   0.067858   0.067871   0.073563   0.067863   1.1519   0.073563   0.062372   0.0987   0.00169467   0.055648   -0.09872   0.065873   0.065873   0.065872   0.065872   0.065872   0.065872   0.065872   0.065872   0.065872   0.065872   0.066817   0.056817   0.056817   0.056817   0.056817   0.056817   0.056817   0.056817   0.067744   0.055748   0.067774   0.055748   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.05578   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.05778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.055778   0.0557	<b>.</b>		-4	0.054229	.05293	1.0244	•
0.576858 0.064945 2.0768 0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064945   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.064967   0.0649	ū		-	-0.049762	.01457	-3.4138	•
0.061689	!		⊶.	0.576858	.06365	9.0622	•
NR: V117  NR: V117  PARAMETER  STANDARD  BLE  DF ESTINATE  ERROR  1 -0.00302711  -0.00302711  -0.00302711  -0.0049502  1 -0.00302711  -0.0049503  1 -0.00302711  -0.0049503  1 -0.00302711  -0.0049503  1 -0.00302711  -0.0049503  1 -0.00302711  -0.0049503  1 -0.00302711  -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  1 -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.004967  -0.0	<b>27</b>			0.1348/6	.10352	4.0/68 0.5959	• •
PARAMETER STANDARD T RATIO PROBSE U.00 PARAMETER STANDARD T RATIO PROBSE U.01 PARAMETER STANDARD T RATIO PROBSE U.016929 U.016929 U.016929 U.016929 U.016929 U.016929 U.016920 U.019621 U.016929 U.016920 U.019621 U.019621 U.016929 U.019620 U.019620 U.019620 U.019620 U.019620 U.019620 U.019620 U.026693 U.026693 U.026987 U.026987 U.026987 U.026693 U.026987 U.026988 U.026989 U.026998 U.026998 U.026998 U.026998 U.0269989 U.0269989 U.0269989 U.0269989 U.0269999 U.0269999 U.02699999 U.0269999 U.0269999 U.026999999 U.02699999 U.02699999 U.02699999 U.026999999 U.026999999 U.0269999999 U.026999999 U.026999999 U.0269999999 U.0269999999 U.0269999999 U.0269999999 U.026999999 U.0269999999 U.02699999999 U.026999999 U.0269999999 U.026999999 U.026999999 U.026999999 U.02699999 U.02699999 U.02699999 U.02699999 U.02699999 U.02699999 U.02699999 U.02699999 U.02699999 U.0269999 U.026999 U.		OELO1		386	6429.02	F RATIO	<b>a</b>
PARAMETER STANDARD T RATIO PROB>   T	VAR	17		DFE MSB	.828	R-SQUARE	38
3.028298 0.210853 14.3621 0.000 1.0.07363 0.049502 1.1519 0.249 1.0.00302711 0.03663 -0.0987 0.732 1.0.0186171 0.055648 -3.3455 0.000 1.0.0186171 0.055648 -3.3455 0.000 1.0.0186171 0.05683 -0.0987 0.949 1.0.0159467 0.02683 -0.0635 0.949 1.0.025908 0.016151 1.6042 0.108 1.0.05770 0.016151 0.8426 0.399 1.0.067770 0.05199 3.2709 0.001 1.0.0135905 0.015362 -0.0885 0.929 1.0.0135905 0.015362 5.5129 0.007	IABLE		90	PARAMETER ESTIMATE	STANDARD		PROB>   T
3.028298					ľ		١ (
1 -0.00302711 0.049502 -0.3427 0.7327 1 -0.00302711 0.03672 -0.0987 0.7327 1 -0.00302711 0.03672 -0.0987 0.0921 1 -0.220728 0.049502 -0.0985 0.00001	ERCEPT		⊶.	3.028298	Ġ	14.3621	000.
-0.00302711	ž £		<b>-</b> -	0.073363	٥٠	-0.3420	732
-0.186171	2		• ~	0		-0.0987	921
1     -0.220728     0.043310     -5.0965     0.000       1     -0.00169467     0.026683     -0.0635     0.949       1     -0.096152     0.062372     -1.5416     0.124       1     0.025908     0.016151     1.6042     0.108       1     0.067770     0.020719     3.2709     0.039       1     -0.085356     0.055789     -1.5300     0.126       1     -0.0135905     0.015362     -0.0885     0.929       1     0.376468     0.067085     5.6118     0.000       1     0.15459     0.064445     2.2129     0.126       1     0.157391     0.068445     2.2129     0.126	39		, <b></b> -		۰.	-3.3455	.000
1 -0.00169467 0.026683 -0.0635 0.949   1 -0.096152 0.062372 -1.5416 0.123   1 0.025908 0.016151 1.6042 0.109   1 0.067303 0.066817 0.8426 0.399   1 -0.085356 0.020719 3.2709 0.001   1 -0.085356 0.055789 -1.5300 0.126   1 -0.0135905 0.015362 -0.0885 0.929   1 0.376468 0.067085 5.6118 0.000   1 0.151459 0.069445 2.2129 0.027   1 0.151459 0.069445 1.4425 0.140	20		-	-0.220728	٠.	-5.0965	000.
1 -0.096152 0.062372 -1.5416 0.123   1 0.025908 0.016151 1.6042 0.108   1 0.056303 0.066817 0.8426 0.399   1 -0.085356 0.020719 3.2709 0.001   1 -0.0135905 0.015789 -1.5300 0.126   1 -0.0135905 0.015362 -0.0885 0.929   1 0.376468 0.067085 5.6118 0.000   1 0.151459 0.068445 2.2129 0.027   1 0.151459 0.068445 2.2129 0.027	80		-	0	Ö	-0.0635	949
1 0.055303 0.066817 0.8426 0.399 1 0.056303 0.066817 0.8426 0.399 1 0.085356 0.055789 -1.5300 0.126 100135905 0.015362 -0.0885 0.329 1 0.376468 0.067085 5.6118 0.000	<b>V</b> 6		⊶.	-0.096152	9,	-1.5416	571.
1 0.06770 0.020719 3.2709 0.001 1 -0.085356 0.055789 -1.5300 0.126 100135905 0.015362 -0.0885 0.929 1 0.376468 0.067085 5.6118 0.000 1 0.157391 0.169106 1.4425 0.129	<b>.</b>		٦-	0.055308	,	7.00.1	000
1 -0.085356 0.055789 -1.5300 0.126 100135905 0.015362 -0.0885 0.929 1 0.376468 0.067085 5.6118 0.000 1 0.151459 0.068445 2.2129 0.027	n es		- ۱	0.067770	ייי	3.2709	.001
100135905 0.015362 -0.0885 0.929 1 0.376468 0.067085 5.6118 0.000 1 0.151459 0.068445 2.2129 0.027 1 0.157391 0.169106 1.4425 0.149			-	-0.085356		-1.5300	126
3 0.151468 0.067085 5.6318 0.000 0.151459 0.068445 2.2329 0.027 1 0.157391 0.109106 1.4425 0.149	. ~		-			-0.0885	.929
1 0.151459 0.068445 2.2129 0.027			-	0.376468	٠,	5.6318	900
	ø,		→	0.151459	9.5	2.2129	.027

HODEL: HODELO:		31	•	7	<u> </u>
DEP VAS: VIII		5 5	•		0,00
<b>1771 177</b>	3	Passagries TOT 1 Mg TO	3.	•	
- C. T. T. T. C.		****			1000
			•		
0.076		~			\$\$01 c
V152		0 031134	14 P. 0 0 0		
Ň		ō	- 100 77 3	:::	0 1250
V1570		0		701.	
		20	٠	<b>₹0</b> : 1	
A0517			0 02121	\$ <b>9 •</b>	
09(5		-	•	••••	0 1500
•	-	0	0		
V168	-	0 02000	0	7	00
•			0		
	-	0.044322	223	****	000
		02960	0 0220		1 90
87 <b>9</b> 40	-	034			134
H.LO		06022	2	_	0.1046
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					
HODEL: HODELO		22	1650.017	P 8410	•
		150	3516	PROBY	8
DEP VAR: VII9		888	0.471569	A - SQUARE	022
		PARAMETER	STANDARD		
VARIABLE	ğ	ESTIMATE	ERROR	T KATIO	PROB>   T
TWEPPOTPP	-	4.173226	9,10,019	38,9734	0
SUPER	-	0.123823	0.032432	3.61	9
SACTO	-	-0.071314	0.025139	-2.8368	9
V152		0.024172	0.015576	1.5519	-
V351V	. –	0.047260	0.028260	1.6723	0
V157C	~	0.006358016	0.021995	0.2891	۲.
V158	-		0.013550	-3.2528	٥.
V159A	-	-0.022296	0.031675	0	7
V160	-	-0.00902551	0.008201917	-1.1004	~
V165	-	-0.037728	0.033932	-1.1119	ä
V168	~	0.035007	0.010522	3.3270	۰.
V169	-	0.033972	0.028332	1.1991	~
V172	-	-0.014965	0.007801479	-1.9183	0.0552
WHS	<b>-</b>	0.061537	0.034068	1.8063	9
BNH3	<b>-</b>	0.079148	0.034759	2.2771	9
PI-	<b>~</b>	0.017430	0.055408	0.3146	۲.

Table C.5--continued

MODEL:	MODETO!		388 DFR	2793.013	F RATIO	11.64
DEP VAR.	V120		M8M	37	R-SQUARE	0.0473
VARIABLE		ď	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T
Intercept Sider	<b>9.</b> ,		3.424057	0.138977	24.6376	0.0001
SACTO		<b>-</b>	•		946	.003
V152 V156#			0.008504083		332	
V157C		-	0.084510		960	.003
V158		٦.	-0.060979		7467	45.4
V159A V160			-0.011626		. 092	27.
V165		-	-0.041877		950	.341
V168		<b>-</b> -	0.029581		577	
V172		٠,	0.034512		408	90
WHS		-	0.153444		.470	96
BNHS OTH			0.010936		836	990.
1		-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		• • • • • • • • • • • • •	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
MODEL	MODET 01		10 C	2642.791	F RATIO	10.90
DEP VAR	V121		NSE NO	0.751647	R-SQUARE	0.0444
VARIABLE		DF	Parameter Estinate	STANDARD ERROR	T RATIO	PROB>  T
INTERCEPT	•	-	3.617959		762	•
SUPER		-	0.136098		323	٠,
SACTO		٦.	-0.035307		112	•
V156			0.121228		397	••
V157C			0.106321		828	0
V158		_	-0.037296		180	•
V159A			0.048989		642	7
2917		• -	, '		647	'n
V168		~	0.002424304		182	æ.
V169		-	0.149996	0	193	•
V172		<b></b> -	0.038389		209	9.5
BNES		<b>-</b>	-0.00506892	0.043883	-0.1155	0.9080
OTH		-			17.	∹

Table C.5--continued

444 <del>-</del>		446	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
9.6 0.0000 0.039	0.0000000000000000000000000000000000000	— · · · · ·	0.000000000000000000000000000000000000
F RATIO PROB>F R-SQUAR T RATIO	26 26 27 27 27 27 27 27 27 27 27 27 27 27 27	F RATIO PROBSF R-SQUARE T RATIO	1.264 1.264 1.264 1.264 1.264 1.2664 1.2664 1.2664 1.2664 1.2664 1.2664 1.2664 1.3664 1.3664 1.3664 1.3664 1.3664
2720.976 3516 0.773884 STANDARD ERROR	0.013173 0.011547 0.013224 0.0136203 0.0136203 0.0136203 0.0136203 0.013643 0.013643 0.009994065 0.014663	2476.85 3516 0.704451 STANDARD ERROR	0.0139639 0.0139639 0.0130728 0.0146882 0.0166882 0.016682 0.016682 0.009535197 0.041639 0.042483
99E DPE MSE PARAMETER ESTIMATE	3.677081 0.091474 -0.075506 -0.038937 -0.0586083 -0.0586083 -0.0586083 -0.0586509 -0.058559 -0.058559 -0.058589	S D PARAMET ESTIMA	-0.021105 -0.031310 -0.031310 -0.032025 -0.08228 -0.003764097 -0.00374456 -0.0131893 -0.013496
<b>60</b>	- MMMMMMMMMMMM   		1 M M M M M M M M M M M M M M M M M M M
MODEL: MODELO: DEP VAR: V122 VARIABLE	INTERCEPT SACTO V153 V155W V157C V159A V165 V165 V168 V172 WHS DNHS OTH	MODEL: MODELO! DEP VAR: V123 VARIABLE	SACTO V152 V155W V155W V159 V160 V168 V169 V172 WHS

Table C.5--continued

17700M	HODET 01		MOS	2065.847	F RATIO	7.47	
DEP VAR:	V124			18	R-SQUARE	0	
VARIABLE		å	PARAMETER ESTIMATE	STANDARD ERROR	T RATIO	PROB> [T]	
INTERCRET		-	0407	14077	.702	.000	
SUPER		-	0.00791473	0.042639	0.1856	0.8528	
SACTO		~	5090	.03305	3	. 065	
V152		-	5070	.02047	.001	.045	
V1 56W		-	-0.1205	.03715	. 245	90	
V157C		~	329	.02891	.215	. 829	
V150		-	22	01701	. 227	-219	
V159A		-	0.0921	04164	.212	.027	
V160		~	1637	0107	. 107	.914	
V165		-	0153	.04461	. 343	731	
V168		-	200	.01363	. 117	.147	
V169		-	9660	.03724	.676	.007	
V172		-	381	.01025	. 722	80.	
SH3		-	1348	.04179	.010	.002	
BNHS		-	120	.04569	. 820	8	
OTH		~	3815	.07284	. 119	. 262	
[	1 1 2 1			! ! ! ! ! ! ! !			
HODEL	MODELO1		19 S S	2862.752	F RATIO	15	
			DEE	351	œ		
DEP VAR:	V125		HSE	2	R-SQUARE	.062	
			PARAMETER	STANDARD			
VARIABLE		DF	ESTIMATE	ERROR	T RATIO	PROB> [T]	
TOAUGAENI		-	•	14070	•	000	
SUPER		٠,		.04261		421	
SACTO		-	-	.03303	5	.000	
V152		-	9	.02046	٠.	. 101	
MyS IA		-	36	.03713	۰.	. 921	
V157C		-	٩.	.02890	ď	8	
V158		-	٠.	.01780	ď.	. 228	
V159A		-	۹.	.04162	٠.	.548	
V160		-	9	.01077	٠.	.106	
V165		→.	9	.04458	֡֟֝֟֝֟֝֟֟֝֟֝֟֟֝֟֝֟֟֝֟֟֝֟֝֟֟֟֟֝ <u>֚</u>	.254	
V168		⊣.	9,	28610.	•	36	
6917		٠,	7,	44150.	e u	35	
7/1/		٦-	?~	04040			
PINE		<b>→</b>	:-	90	3.5454	0.000	
OTH.			-0.026505	07280	<u>س</u>	715	

Table C.5--continued

FRATIO 6.56 PROBSF 0.0001 R-SQUARE 0.0272	T RATIO PROB> T	31.2652 0.2594 -3.3243 -0.5756 0.0009 -2.8435 0.0045 -1.9980 0.4768 0.4768 0.4768 0.4768 0.4768 0.4587 1.369 0.2557 -3.9878 0.0001 2.2591 0.2338 -1.2590 0.2338	F RATIO 13.52 PROB>F 0.0001 R-SQUARE 0.0545	T RATIO PROB> T	28.7389 -1.4257 -6.1806 -0.3918 -2.2364 -3.9195 -1.6411 -0.0001 -2.2263 0.0001 -0.1158 0.9079 0.4759 0.6850 -4.4684 0.0001
2878.704 3516 0.818744	STANDARD	6.141093 0.033124 0.033124 0.033124 0.0126224 0.0126224 0.01263124 0.013851 0.013851 0.013851 0.013861 0.013861 0.014880	4133.908 3516 1.175742	STANDARD	0.169078 0.051210 0.051210 0.0246595 0.0344595 0.0344595 0.050915 0.012951 0.012951 0.014614
20 20 20 20 20 20 20 20 20 20 20 20 20 2	Parameter Estimate	4.411293 0.011085 -0.0110813 -0.010882 -0.05882 -0.076846 0.076846 0.076846 0.076846 0.076846 0.076846 0.076846 0.076846 0.076846 0.076846 0.076869	188 189 189 189 189 189 189 189 189 189	Parameter Estimate	4.859124 -0.073011 -0.095336 -0.095793 -0.136121 -0.035113 -0.011349 -0.011349 -0.011381
MODELO1 V126	å	пестемененене	1075	DE	<b>пппппппппппп</b>
MODEL: MODE DEP VAR: V126	VARIABLE	INTERCEPT SACTO SACTO VI52 VI55W VI56W VI56W VI59A VI69 VI69 VI69 VI72 VI73 MHS BNHS	MODEL: MODELO! Dep var: V127	VARIABLE	INTERCEPT SUPER SACTO VI 52 VI 558 VI 558 VI 598 VI 60 VI 69 VI 69 VI 69 VI 69 VI 69

Table C.5--continued
NONSUPERVISORS ONLY

15.87 0.0001 0.0759	PROB> [T	0.0001 0.0001 0.0001 0.0001 0.0001 0.0000 0.0000	0.0001 0.3143 0.0001 0.1736 0.0256	7.96 0.0001 0.0396	PROB>[T]	0.0001 0.0001 0.0358 0.7874 0.0013	0.5614 0.3062 0.0062 0.0001 0.0002 0.0099 0.5199
F RATIO PROB>F R-SQUARE	T RATIO	13.0055 -6.10992 -0.10992 -0.1098 -1.4151 -1.31982 -1.31982	3.8670 -1.0065 -6.1051 1.3611 -2.2332 -0.4191	f ratio Prob>f R-square	T RATIO	10.9730 -4.7277 -2.0892 -0.2697 3.2126 1.2318	-0.4380 1.0235 4.6606 -1.0275 -3.4863 0.66461
3146.17 2704 1.163524	STANDARD KRROR	0.184706 0.043610 0.050436 0.050436 0.025186 0.055142 0.055549	0.018488 0.050687 0.014287 0.060395 0.094606	2820.177 2704 1.042965	STANDARD	0.174876 0.041289 0.025976 0.047733 0.039639	0.052592 0.014061 0.017504 0.047989 0.013527 0.058048
8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Parameter Estinate	2.402198 -0.270346 -0.0089452 -0.0054471 -0.060721 0.005046467	0.071493 -0.051017 -0.087940 0.083020 -0.136916	15 MAG	Parameter Estimate		-0.023036 0.081391 0.081579 -0.049307 -0.051217 0.037356
	Ď				DE	пппппп	<b>ннянняння</b>
MODELO1 V32		<b>b</b>		MODEL01 V59		Eu	
MODEL: DEP VAR:	VARIABLE	INTERCEPT 9ACTO V152 V156W V156W V158 V159A V160	V168 V169 V172 WH9 BNHS OTH	MODEL: DEP VAR:	VARIABLE	INTERCEPT SACTO V152 V156W V157C	V159A V160 V168 V169 V172 WHS BNHS

Table C.6

RECRESSION RESULTS FOR SCALES. ALL EMPLOYEES

35.03 0.0001 0.1311	PROB> [T]	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0010 0.0527 0.00103 0.0103 0.0107	22.07 0.0001 0.0868 PROB>[T]	0.0001 0.0001 0.0001 0.00101 0.00101 0.00101 0.00101 0.00101 0.00101 0.00101 0.00101 0.00101 0.00101
F RATIO PROB>F R-SQUARE	T RATIO	25.1740 7.3035 -9.0140 -0.2138 7.1758 4.3625	- 4. 5625 - 1. 2566 - 1. 2	F RATIO PROB>F R-SQUARE T RATIO	26.9177 8.1642 -2.3646 -3.9466 2.5367 -4.5841 -1.9089 -0.7666 -2.9206 -2.9206 -2.9206 -2.9206 -2.9206
1963.415 3484 0.563552	STANDARD ERROR	0.117591 0.035616 0.027607 0.017105 0.024154	0.009007132 0.00307132 0.015554 0.008567381 0.037413 0.060848	2554.6 3484 0.733238 STANDARD ERROR	0.134131 0.04626 0.0316413 0.0319511 0.035400 0.0105974 0.0105974 0.0105974 0.0105974 0.0105974 0.0105974 0.0105974 0.0105974
SSE COM	Parameter Estimate	2.960240 0.260122 -0.248819 -0.0365759 0.105309	0.003640456 0.0036404586 0.0036404586 0.0036404586 0.0036623	89E DFE MSE PARAMETER ESTIMATE	3.610503 0.331676 -0.137640 -0.145682 0.069943 -0.07810 -0.07810 0.00738559 0.007730576 -0.126842 -0.176462
	à			DF	ппппппппппппппппппппппппппппппппппппппп
MODEL: MODELO1 DEP VAR: PN02	VARIABLE	INTERCEPT SUPER SACTO VISS VISS VISS	V159A V160 V168 V172 V173 WHS BNHS OTH	MODEL: MODELO1 DEP VAR: PM03B VARIABLE	INTERCEPT SUPER SACTO V152 V152 V159 V159 V160 V169 V169 V169 V172 WHS BNHS

Table C.6--continued

MODEL: DEP VAR:	MODELO1		SSE	3112.7 3484 0.893427	F RATIO PROB>F R-SQUARE	24.69 0.0001 0.0961
VARIABLE		ď	Parameter Estimate	STANDARD	T RATIO	PROB>   T
INTERCEPT			2.743156	.1480	527	0.0001
9ACTO V152 V156#			-0.333880 0.032735 -0.461996	0.021537	-9.6033 1.5199 -11.8231	0.1286 0.0001
V157C			0.049157	0304	616.	0.1061 0.0030
V159A V160			-0.012058 -0.057192	.0437	275	0.7831 0.0001
V165			0.191015	.0469	071	0.0001 0.0001
V169		·	0.108055	.0391	758	0.0058
VI / Z			0.001484216	0471	100	0.9749
BNHS			-0.061369	.0480	384	0.2017
MODEL	MODELU1		20 C) 1	1911.808	F RATIO PROB>F	0.0001
VARIABLE		90	PARAMETER ESTIMATE	TANDAR	T RATIO	. An
	1				200	. 6
SUPERCEPT	<b>+</b>	<b>-</b> -	4.33921B -0.00429731	.03514	. 122	. 902
SACTO		<b>.</b>		.02724	684	000
V152		<b></b>	-0.00189495	.03062	456	.03
V157C				.02383	.015	.043
V159A				.03432	890	.058
V160 V165		<b></b>	-0.00369609 0.00681947A	0.008887971	-0.4159 0.1855	0.6775 0.8529
V168		· ·	•	.01140	271	.023
V169 V172			0.149959	.030/0 845403	. 884 . 131	. 033
WHS		, <b></b> 1 -	0.141913	0.03691	844	900
BNHS OTH		<b>-</b>	-0.067576	.06004	125	260

Table C.6--continued

9TANDARD T RATIO PROE ERROR T. 134417 25.2100 0.013417 25.2100 0.0131557 -9.0682 0.0131557 -9.0682 0.0131557 -9.0682 0.0131557 -9.0682 0.013162 0.013264 0.013268 0.013268 0.013268 0.013268 0.013268 0.013268 0.013219 0.0137576 0.013219 0.0137576 0.013219 0.0137576 0.013219 0.0137576 0.013219 0.013219 0.013219 0.013219 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013119 0.013189 0.013189 0.013189 0.013189 0.013189 0.013189 0.013189	MODEL	MODET01		336	2565.476 3484	F RATIO	27.40
PARAMETER STANDARD T RATIO PRO ESTINATE ERROR T TATIO PRO ESTINATE TO 134417 25.2100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VAR	PM06		HSR.	. 73635	R-SQUARE	
1	VARIABLE		J.C	Parameter Estinate	STANDARD ERROR	RATI	PROB> [T]
0.386376 0.040712 9.3431   0.086716 1 0.086716   0.031557   -9.0662   0.011553   -9.0662   0.011553   -9.0662   0.011553   -9.0662   0.011553   -9.0662   0.0115213   0.0115610   -3.7322   -0.06573416   0.0127610   -3.7322   -3.6526   0.013762   -2.4636   0.013276   -2.4636   0.013276   -3.6596   0.013208   2.4433   0.013271   0.013208   2.4433   0.013271   0.013265   -2.9483   0.013271   0.013265   -2.9483   0.013271   0.013265   -2.9483   0.013271   0.013265   -2.9483   0.013271   0.045766   0.065771   0.045766   0.045766   0.045769   0.045769   0.045769   0.045769   0.045766   0.059576   0.013279   0.5115   0.013576   0.013279   0.5115   0.013576   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013279   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013271   0.013171   0.013271   0.013171   0.013271   0.013171   0.013271   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171   0.013171	EGREGATI	•	-	.38864	.13441	5.210	.000
-0.286163 0.011557 -9.0682     -0.009515997 0.019553 -0.0479     -0.00573416 0.037610 0.1330     -0.00573416 0.037610 0.1330     -0.00573416 0.037610 0.1330     -0.00573416 0.037610 0.1330     -0.00573416 0.037612 -2.4526     -0.007519 0.012296 1.8649     -0.004765 0.035565 -2.9458     -0.00457691 0.043633 -2.9458     -0.00457691 0.043633 -2.9458     -0.00457691 0.043633 -0.1049     -0.00457691 0.069554 0.5115     -0.00457691 0.069554 0.5115     -0.00457691 0.069554 0.5115     -0.005644 0.026339 -6.0508     -0.005644 0.026012 0.13576 0.03639     -0.005644 0.026012 0.13566     -0.005644 0.026012 0.13516     -0.005644 0.01659 0.13516     -0.005644 0.01659 0.13516     -0.01893 0.010538 1.7929     -0.01893 0.013539 -3.2866     -0.013231 0.013539 -3.2156     -0.0031231 0.013631 1.3105     -0.0031295 0.001468 -0.8324     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -0.0031295 0.001468 -0.8334     -	SUPER		-	037	.04071	. 343	800
1 -0.000935997   0.019553   -0.0479   0.013571   0.027610   0.027610   0.027610   0.027610   0.027610   0.027610   0.027610   0.027610   0.027610   0.027610   0.027610   0.027610   0.01322   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013261   0.013161   0.013261   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013161   0.013	SACTO		-	919	.03155	.068	.000
0.143213 0.035475 4.0370     0.00367416 0.027510 0.1330     0.00367416 0.017010 -3.7322     0.0143241 0.017010 -3.7322     0.0143241 0.017010 -3.7322     0.0143241 0.017010 -3.7322     0.0143241 0.017010 -3.7322     0.0143241 0.017010 -3.7322     0.0143241 0.013208	V152		٠	.00093599	.01955	0.047	.961
0.003673416   0.027610   0.1330     0.00367819   0.017010   -3.7322     0.0197819   0.0137026   1.8649     0.0143543   0.013208   2.4433     0.0143543   0.013208   2.4433     0.014765   0.0037585   3.5699     0.0657691   0.043583   -5.1715     0.0657691   0.043633   -0.1049     0.0657691   0.043633   -0.1049     0.0657691   0.043633   -0.1049     0.043578   0.043633   -0.1049     0.043578   0.043633   0.5115     0.03578   0.071376   ERRICOR     0.052644   0.032012   0.1321     0.052644   0.032012   0.1321     0.052644   0.032012   0.1321     0.052644   0.032012   0.1321     0.077538   0.010538   1.7929     0.077538   0.010538   1.7929     0.077538   0.013519   5.7356     0.077538   0.013519   -3.8814     0.077538   0.014658   -0.8324     0.077538   0.014658   -0.8324     0.077538   0.014658   -0.8324     0.077539   0.013519   -3.8814     0.077539   0.014658   -0.8324     0.077539   0.014658   -0.8324     0.077539   0.014658   -0.8324     0.077539   0.014658   -0.8324     0.077539   0.017189   -1.3105     0.077539   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.077189   0.077189   -1.3105     0.07	V156W		-	321	.03547	.037	900
-0.063485	V157C			.00367341	.02761	. 133	200
ELI MODELOI DE ESTIMATE ERROR TAILO PRO CONTACT TO CONT	V158		~	36348	.01701	3.732	000.
0.019201 0.010296 1.8649   0.042595   0.042595   0.042595   0.042595   0.042595   0.042595   0.042595   0.042595   0.0132271   0.0435233   -2.9458   0.042766   0.042766   0.042766   0.042766   0.042766   0.042766   0.042766   0.042766   0.043633   0.01049   0.042766   0.043633   0.01049   0.042766   0.05254   0.05254   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059554   0.059569   0.05959   0.05959   0.05969   0.052699   0.052699   0.052699   0.052699   0.052699   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.05959   0.0	V159A		-	19751	.03976	2.452	• 10 ·
ELI MODELOI 0.143543 0.042595 3.3699 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.035565 0.036333 0.01049 0.0065171 0.045633 0.043633 0.05115 0.0065578 0.043633 0.05115 0.05155 0.043633 0.05155 0.041669 0.05115 0.03578 0.037410 PRC ESTIMATE ERNOR TANDARD TANTIO PRC ESTIMATE ERNOR 0.037299 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229 0.03229	V160		_	11920	.01029	964	790.
1	V165			14354	.04259	. 369	. 000
1	V168		-	3227	.01320	. 443	10.
ELI MODELO1 0.065171 0.042766 1.5239 0.042766 1.5239 0.046537 0.046533 0.5115 0.046554 1.5239 0.046554 0.069554 0.069554 0.5115 0.046554 0.069554 0.5115 0.046591 0.069554 0.5115 0.04659 0.069554 0.05115 0.04659 0.771376 PROBER ESTIMATE ERROR TRATIO PROBECT 1 2.977387 0.137576 21.6418 0.052612 0.041669 8.4755 0.041669 8.4755 0.041669 0.026012 0.1321 0.109544 0.026012 0.1321 0.109544 0.026012 0.1321 0.173964 0.026012 0.1321 0.173964 0.026012 0.1321 0.173964 0.036399 3.5689 0.173964 0.036399 0.173929 0.040696 0.173929 0.040696 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.013519 0.036401 0.035171 0.037175 0.044658 0.071189 0.071189	6917		_	10476	.03556	2.945	.003
0.065171   0.04364   1.5239   0.044564   0.044564   0.01449   0.044564   0.01449   0.044564   0.01449   0.0144644   0.0144644   0.0174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.174410   0.0144410   0.0144410   0.0144410   0.0144410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.014444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.014444410   0.01444410   0.01444410   0.01444410   0.01444410   0.014444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01444410   0.01	V172		,4	15064	.00979323	5.171	000
-0.00457691   0.043633   -0.1049   0.043554   0.053155   0.069554   0.51155   0.069554   0.053155   0.069554   0.051155   0.069554   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155   0.051155	6H3		<b>~</b> 4	56517	.04276	. 523	.127
0.035576	SHAR			0.0045769	.04363	104	916
MODELO1   SSE	OTH			0.03557	.06955	. 511	. 609
MODELO    SSE   2087.475   FRAIL   FROMES   1484   FROMES   1484   FROMES   1484   FROMES   1484   FROMES   1484   FROMES   1484   1484   1484   1484   1484   1484   1484   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   1884   18	1 1 2		1		; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;		G C
PARAMETER STANDARD T RATIO PRO CENTRE CONTROL T RATIO PRO CESTIMATE ERROR T RATIO PRO CESTIMATE ERROR T RATIO PRO CESTIMATE CONTROL T RATIO PRO CESTIMATE CONTROL T RATIO PRO CESTIMATE CONTROL T CO	MODEL	HODETO1		300	77.780	OLINA S	1000
PARAMETER STANDARD T RATIO PRO ESTIMATE ERROR T RATIO PRO 10.353165 0.041669 6.0508 0.17357 0.137576 8.4755 0.0052444 0.026012 0.1321 0.105854 0.035309 4.7912 0.173964 0.035309 4.7912 0.103950 0.017410 -3.2866 1.0957219 0.017410 -3.2866 1.7959 0.016893 0.010538 1.7929 0.010538 1.7929 0.010538 1.7929 0.010538 1.7929 0.010538 1.7929 0.0077538 0.010538 1.7929 0.0077538 0.010523 1.32156 0.0079329 0.0073771 1.8124 0.0079329 0.0077189 -1.3105				310	900		1900
PARAMETER   STANDARD   T RATIO   PROB> T	VAR	PM07		MSM	. 11131	K-SOOAKE	0.109
LELE DE ESTIMATE ERROR T RATIO PROBENTY  1 2.977387 0.137576 21.6418 0.000  1 -0.195434 0.031299 -6.0508  1 -0.195434 0.020012 -6.0508  1 0.0026444 0.020012 0.1321 0.000  1 0.173964 0.026259 3.5688 0.000  1 0.073956 0.017410 -3.2866 0.001  1 0.079356 0.040696 -1.9500 0.073  1 0.096081 0.040696 -1.950 0.073  1 0.07538 0.013519 5.7356 0.000  1 0.077538 0.013519 5.7356 0.000  1 0.077538 0.013519 5.7356 0.000  1 0.0372231 0.013023 -3.2156 0.070  1 0.0372231 0.014028 -3.2156 0.070  1 0.037175 0.044658 -0.8324 0.405				PARAMETER	STANDARD		
1	VARIABLE		DF.	ESTIMATE	ERROR		PROB>   T
1 0.353165 0.041669 8.4755 0.0000 1.0000 1.0000000 1.00000000000	CONTRACTOR		_	97738	.13757	_	.000
-0.195434	STIPER			35316	.04166	8.4755	900
0.0026444	SACTO			0.19543	.03229	-6.0508	000
1 0.173964 0.036309 4.7912 0.000 1 0.100850 0.026259 3.5688 0.000 1 -0.057219 0.017410 -3.2866 0.000 1 -0.079356 0.040696 -1.9500 0.051 1 0.018893 0.010538 1.7929 0.073 1 0.096081 0.043597 2.2039 0.073 1 -0.04538 0.013519 -3.8814 0.000 1 -0.079323 0.010023 -3.2156 0.000 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V1 52			002644	.02001	0.1321	894
1 0.100850 0.028259 3.5688 0.000 1 -0.057219 0.017410 -3.2866 0.001 1 0.079356 0.0106548 1.7929 0.073 1 0.096081 0.010538 1.7929 0.073 1 0.077538 0.013519 5.7356 0.000 1 -0.141284 0.036401 -3.8814 0.000 1 0.079329 0.013771 1.8124 0.001 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V156W		_	.17396	.03630	4.7912	000
1 -0.057219 0.017410 -3.2866 0.001 1 -0.079356 0.040696 -1.9550 0.051 1 0.018693 0.040538 -1.9529 0.0731 1 0.077538 0.013519 5.7356 0.027 1 -0.141284 0.036401 -3.8814 0.000 1 -0.032231 0.010023 -3.2156 0.000 1 -0.03771 1.8124 0.0701 1 -0.093295 0.071189 -1.3105 0.190	V157C		-	.10085	.02825	3.5688	000
A 1 -0.079356 0.040696 -1.9500 0.051 1 0.018893 0.010538 1.7929 0.073 1 0.077538 0.013519 5.7356 0.020 1 -0.141284 0.036401 -3.8814 0.000 1 -0.032231 0.010023 -3.2156 0.0001 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V158		-	.05721	.01741	~	.00
1 0.018893 0.010538 1.7929 0.073 1 0.096081 0.043597 2.2039 0.027 1 0.077538 0.013519 5.7356 0.000 1 -0.141284 0.036401 -3.8814 0.000 1 -0.037231 0.010023 -3.2156 0.001 1 0.079329 0.043771 1.8124 0.070 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V159A		-	.07935	.04069	→ .	.051
1 0.096081 0.043597 2.2039 0.027 1 0.077538 0.013519 5.7356 0.000 1 -0.141284 0.036401 -3.8814 0.000 1 -0.032231 0.010023 -3.2156 0.001 1 0.079329 0.043771 1.8124 0.070 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V160		-	.01889	.01053	1.7929	. 073
1 0.07538 0.013519 5.7356 0.000 1 -0.141284 0.036401 -3.8814 0.000 1 -0.032231 0.010023 -3.2156 0.001 1 0.079329 0.043771 1.8124 0.070 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	4165			.09608	.04359	2.2039	.027
1 -0.141284 0.036401 -3.8814 0.000 1 -0.032231 0.010023 -3.2156 0.001 1 0.073229 0.043771 1.8124 0.070 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V168		~4	.07753	.01351	5.7356	000
1 -0.032231 0.010023 -3.2156 0.001 1 0.079329 0.043771 1.8124 0.070 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V169		-	.14128	.03640	<b>~</b>	000.
1 0.079329 0.043771 1.8124 0.070 1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	V172		-	.03223	.01002	σ,	.001
1 -0.037175 0.044658 -0.8324 0.405 1 -0.093295 0.071189 -1.3105 0.190	WHS		-	.07932	.04377	1.8124	0.00
1 -0.093295 0.071189 -1.3105 0.150	BNHS		-	.03717	.04465	-0.8324	SOP.
	OTH			.09329	.07118	-1.3105	. 190

Table C.6--continued

NARIABLE   PARAMETER   1.086336   R-SQUARE   0.1353			MSM	1.086306	D-90/1ARK	
PARAMETER STANDARD T RATIO FF (1) 10 10 10 10 10 10 10 10 10 10 10 10 10				1 1 1 1		0.1353
## 1 3.305742 0.163262 20.2481  1	ei	DF	Parameter Estimate	STANDARD ERROR		PROB>[T]
0.250100 0.038329 6.5251     0.020355 0.043088 4-3.2163     0.020355 0.043088 4-3.2163     0.020355 0.043088 4-3.2163     0.020355 0.043688 4-3.2163     0.054586 0.042695 1.1303     0.054586 0.042695 1.1303     0.054586 0.043197 -0.8488     0.017082 0.051736 -0.8488     0.017082 0.011895 -0.5991     0.078502 0.011895 -0.5991     0.078502 0.011895 -0.5991     0.078502 0.011895 -0.5991     0.0134219 0.052996 2.5326     0.0134219 0.052996 2.5326     0.0134219 0.052996 2.5326     0.0213904 0.021895 0.18338     0.0213904 0.037850 -1.4199     0.086840 0.037850 -1.4199     0.068840 0.037850 -1.4199     0.068840 0.037850 -1.4199     0.068840 0.037850 -1.4199     0.068840 0.037850 -1.4199     0.068840 0.037850 -1.4199     0.0139186 0.031308 -1.5303     0.013186 0.037850 -0.4015     0.0131854 0.00864295 3.5667     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.0131854 0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508 0.4972     0.038508	re.			16326	~~	80
1		-	0.250100	.03832	6.5251	
1		⊶,	-0.076383	.02374	-, -	
MODELOI  DEE  PARAMETER  PARAMETER  ESTINATE  1 0.054566  0.048295  1.1303  1.072082  0.048295  1.1303  1.072082  0.048295  1.1303  1.072082  1.1303  1.072082  0.048295  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1303  1.1333  1.1333  1.1333  1.1333  1.1333  1.1333  1.1333  1.1333  1.1833  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.10033854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.1003854  1.		<b>→</b> -	0.203383	00530.		
0.054586		- ٠	0.10100	02066	, .	
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-0.172082		• ~	0.011610	.01250	0.9284	
1		-		.05173	***	
-0.036666   0.043197   -0.8488       0.078502   0.051944   -0.73197       0.038015   0.0529944   -0.73199       0.134219   0.052996   2.5326       0.134219   0.084480   2.5326       0.213904   0.084480   2.5326       0.213904   0.084480   2.5326       0.213904   0.084480   2.5326       0.213904   0.084480   2.5326       0.213904   0.084480   2.5326       0.137714   0.035337   RAZIO PRE ERROR   T. RATIO PRE ERROR   2.0432       0.037566   0.017856   -1.4199       0.077566   0.013836   -0.4753       0.0684109   0.015012   -3.2579       0.0684109   0.015092   1.5303       0.0684109   0.015592   0.4753       0.0684109   0.037592   0.4753       0.0183184   0.00864295   3.9169       0.0138391   0.038508   0.038508       0.0138391   0.038508   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.0138391   0.038508       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408       0.015086408		-		.01604	J	
0.078502   0.011895   6.5997   0.0518914   0.0518914   0.0518914   0.0518914   0.0518914   0.0518914   0.0518914   0.0518914   0.0518914   0.0518914   0.0518914   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916   0.0518916		-		.04319	v	
0.134219   0.052996   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.5326   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.53237   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.5328   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53337   2.53338   2.53338   2.53338   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.53328   2.533		~	0.078502	.01189	6.5997	
0.134219   0.052996   2.5326		_	-0.038015	.05194	u	
MODELO1		-	0.134219	.05299	2.5326	
PARAMETER STANDARD  PARAMETER STANDARD  T 1 3.593892 0.118628 30.2954 1 -0.056904 0.035930 -2.0432 1 -0.024502 0.035930 -2.0432 1 -0.024502 0.031865 -2.0432 1 -0.024502 0.031865 -2.0432 1 -0.024502 0.031308 2.7737 1 -0.048908 0.015012 -3.2579 1 -0.048908 0.015012 -3.2579 1 -0.048908 0.03592 1.5303 1 -0.048908 0.03592 2.5303 1 -0.048908 0.03592 2.5303 1 -0.048908 0.031388 5.8426 1 0.038391 0.031743 3.6667 1 0.038391 0.0317443 3.6667		-	0.213904	.08448	2.5320	
PARAMETER 3464 FROESE  PARAMETER STANDARD  DF ESTIMATE ERROR T RATIO PR  1 0.137714 0.035930 3.6328 1 -0.056904 0.037850 -2.0432 1 0.086840 0.037856 -1.4199 1 0.077566 0.031308 2.7737 1 0.077566 0.031308 2.7737 1 0.0684109 0.015012 -3.2579 1 0.0684109 0.015592 0.4753 1 0.015084 0.00864295 3.9169 1 0.138391 0.031388 5.8426 1 0.138391 0.031343	MODREO		or or	698.20	F RATIO	12.98
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-0.024502 0.017256 -1.4199 0.00.086840 0.031308 2.7737 0.00.024367 3.1833 0.00.024367 3.2579 0.00.024367 3.2579 0.00.024367 0.005902 1.5303 0.00590858 -0.4753 0.00908658 -0.4753 0.00908658 0.0049753 0.013838 0.031388 5.8426 0.0138391 0.031743 3.6667 0.009145 0.0318508 0.0318508 0.04972 0.0090864295		~	-0.056904	0.027850	-2.0432	•
0.086840 0.031308 2.7737 0.007566 0.024367 3.1833 0.007566 0.024367 3.1833 0.00508308 0.015012 -3.2579 0.00508658 -0.04753 0.005084109 0.037592 -0.4753 0.00684109 0.031854 0.00864295 3.9169 0.0138391 0.037743 3.6667 0.0098145 0.038508 0.04972 0.0098508		-	-0.024502	0.017256	-1.4199	
0.077566 0.024367 3.1833 0. 0.048908 0.015012 -3.2579 0. 0.053702 0.035092 1.5303 0. -0.00431801 0.00908658 -0.4753 0. 0.00684109 0.037592 -0.401 0. 0.183385 0.011657 0.5865 0. 0.0338391 0.037743 3.6667 0. 0.019145 0.038508 0.4972 0.		-	0.086840	0.031308	2.7737	
-0.048908 0.015012 -3.2579 0. 0.053702 0.035092 1.5303 0. 0.00431861 0.00908658 -0.4753 0. 0.00684109 0.013657 0.8665 0. 0.138385 0.031388 5.8426 0. 0.138391 0.037743 3.6667 0.		-	0.077566	0.024367	3.1833	•
0.053702 0.035092 1.5303 00.00431861 0.00908658 -0.4753 00.015084 0.01592 -0.401 0. 0.00684109 0.011657 0.5865 0. 0.033854 0.00864295 3.9169 0. 0.138391 0.037743 3.6667 0.			-0.048908	0.015012	-3.2579	•
-0.00431861 0.00908658 -0.4753 0. -0.015084 0.037592 -0.4015 0. 0.0684109 0.011657 0.5865 0. 0.18315 0.031388 5.8426 0. 0.033854 0.00864295 3.9169 0. 0.138391 0.037743 3.6667 0.		-	0.053702	0.035092	1.5303	•
-0.015084 0.037592 -0.401 0.00684109 0.011657 0.5865 0.0018386 5.8426 0.0031854 0.00864295 3.9169 0.0138391 0.037743 3.6667 0.0019145 0.038508 0.4972 0.0019145 0.038508 0.4972			•	•	-0.4753	•
0.00684109 0.011657 0.5865 0. 0.183385 0.031388 5.8426 0. 0.033854 0.00864295 3.9169 0. 0.138391 0.037743 3.6667 0. 0.019145 0.038508 0.4972 0.			-0.015084	0.037592	-0.401 🤅	•
0.183385 0.031388 5.8426 0. 0.033854 0.00864295 3.9169 0. 0.138391 0.037743 3.6667 0. 0.019145 0.038508 0.4972 0.			•	0.011657	5985.0	•
0.033854 0.00864295 3.9169 0.0.138391 0.03743 3.6667 0.0.019145 0.038508 0.4972 0.		-	0.183385		5.8426	
0.138391 0.037743 3.6667 0. 0.019145 0.038508 0.4972 0.		-	0.033854	•	3.9169	•
0.019145 0.038508 0.4972 0.		<b>~</b>	0.138391	0.037743	3.6667	•
		۰,	0.019145	0.038208	7.69.0	•

Table C.6--continued

MODEL	HOOET 01		888 1970	2888.361 3484	F RATIO	56.24 0.0001	
DEP VARI	PM11		2014	0.829036	R-SQUARE	0.1949	
VARIABLE		Ġ	Parameter Estimate	STANDARD	T RATIO	PROB> [ T ]	
INTERCEPT		-	.88624	0.142625	20.2366	0.0001	
SUPER			0.374844	0.043198	-9.5196	0.0001	
SACTO			04616	0.020747	2.2249	0.0261	
7CTA		•	11347	0.037641	3.0147	0.0026	
V157C		-	. 26227	0.029296	8.9525	0.0001	
V158			0.11048	0.018049	-6.1216	0.0001	
V159A		<b></b>	-0.03906	0.042190	-0.94.0	0.33	
V160		<b>~</b> -	0479222	0.010929	1 7726	0.0764	
V165			11000.	0.04015	8.2171	0.0001	
89IA		- ب	2227.0	0.037737	-3.5252	0.000	
67.5		4	05475	0.010391	-5.2693	0.0001	
7/1/		4	0.16142	0.045378	3.5573	0.000	
E E E		٠-	11745	0.046297	-2.5370	0.0112	
OTH			.08471	0.073802	-1.1479	0.2511	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			000	
MODEL	MODETO1		100	3243.42/	F KATIO	20.00	
			DFE	,	PROB>F	000.0	
DEP VAR	PM12		MSE	0.930949	R-SQUARE	0.1310	
			PARAMETER	STANDARD			
VARIABLE		DF	ESTIMATE	ERROR	T RATIO	PROB>  T	
THERCEPT		7	3.287068	0.151137	.748	0	
SUPER		-	0.240520		. 254	8	
SACTO		~	-0.235063		624	8	
V1 52		_	0.028311		. 287	5	
V156W		_	-0.114849		. 879	9	
V157C			0.207742		160.0	36	
V158		⊶ -	-0.1064/4	0.019126	-1.6910	6060.0	
V159A		٠,	` `		A C C C	6	
V160		٦-	0.000402.000.0		277	ò	
2017		→ -	0.121046		150	8	
0 4 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -		- ۱	-0.086442		161	6	
V103		• -	-0.064954		888.	ö	
EH3		· ~	0.196871		.094	8	
BNHS		_	-0.128491		619	9	
OTH		_	-0.161894		.070	5	
;							

Table C.6-continued

MODEL: MODELO! DEP VAR: PM14		335 346 346 346 346 346 346 346 346 346 346	2141.928 3484 0.614790	F RATIO PROB>F R-SQUARE	30.65 0.0001 0.1166
VARIABLE	DF	Parameter Estimate	STANDARD	I RATIO	PROB>[T]
INTERCEPT	,-4 ,-4 ,	2.684646	200	21.8583	0.0001
<b>SACT</b> 0 V152 U154		-0.159019 -0.014239 0.127626	0.028835 0.017866 0.032415	-5.514%	425
V1504 V157C	4 ~4 ~	0.082911	22	3.2865	000
V159A		-0.06117	. C. G	-1.6837	974
V165	•	0.11548	0.03892	2.9672	003
V169		-0.064147	0.03249	-1.9740	870
V172	<b></b>	-0.040243	28	1.3070	191
BNHS	4	0.018999	96	-0.4765	633
OIN	• ;		: :		
MODEL: MODEL01		1999	1640.971	F RATIO	39
DEP VAR: PM15		MSE	0.471002	R-SQUARE	146
VARIABLE	DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT	-	2.701900	10750	133	0.0001
SUPER		0.281476	02523	217	0.0001
V152	4 ~	-0.065904	.01563	7	0.0001
W351V	<b>-</b>	0.093715	.02837	203	0.00.0
V15/C V158		-0.021014	.01360	7	0.1225
V159A	⊶.	-0.09104	0.03180	363	0.0042
V160 V165		0669867 0.10980	.03406	233	0.0013
V168		0.05136	92	362	0.0001
V169 V172	<b>-</b>	-0.054549	0.007832358	-6.9645	0.0001
WHS	<b>-</b> -	0.161271	03420	715	0.0001
BINHS OTH	4 ~	0.044304	.05562	360	0.4258

Table C.6--continued

12.02 0.0001 0.0492	PROB>   T	0.0001 0.0001 0.0001 0.5152 0.0001 0.0203 0.114 0.001 0.0001 0.2229	40.61 0.0001 0.1488	PROB>  T  0.0001 0.0001 0.0001 0.0001 0.0001 0.0004 0.0028 0.0028
F RATIO PROB>F R-SQUARE	T RATIO	15.7875 5.44875 0.3705 0.3705 0.3705 0.3705 0.3207 1.4207 1.4214 1.4550 6.5501 1.2192 -0.8175	F RATIO PROB>F R-SQUARE	7 RATIO 22 9641 10.5619 -6.8238 -1.3660 5.6860 5.6860 -4.6132 -3.5597 0.1671 2.6001 2.4915 -2.4915 -2.4915
2783.827 3484 0.799032	STANDARD ERROR	0.140020 0.0424020 0.032872 0.036954 0.036954 0.014119 0.0141311 0.013731 0.013731 0.015459 0.045452	1695.047 3484 0.486523	STANDARD ERROR 0.109260 0.013092 0.015893 0.028836 0.013826 0.013826 0.013826 0.013826 0.013826 0.013826 0.013826 0.013826 0.013826 0.013826 0.013826
338 DPFI MSF	Parameter Estinate	2.210564 0.230921 0.007545848 0.0126051 0.0126051 0.0126068 0.010857 0.010857 0.010857 0.052168 0.052168 0.055415	SSR DFT	PARAMETER ESTIMATE 2.509052 0.349519 -0.15140 -0.053784 -0.131181 -0.063784 -0.13181 -0.063784 -0.063784 -0.063784 -0.063784 -0.06378618
10	<u>a</u>		10	<u> </u>
MODEL: MODELO1 DEP VAR: PM17	VARIABLE	INTERCEPT SUPER SACTO V155 V156 V156 V159 V165 V166 V166 V169 V172 WHS	MODEL: MODELOI DEP VAR: PM18D	VARIABLE INTERCEPT SUPER SACTO V1554 V1576 V1596 V169

Table C.6--continued

PARAMETER STANDARD	MODEL: MODE	MODELO1		11 14 15 17 15	3876.389 3484 1.112626	F RATIO PROB>F R-SQUARE	38.65 0.0001 0.1427
1 2.204547 0.165228 13.3425 0.191848 0.036044 3.8336 0.036190 0.036190 0.050044 3.8336 0.0212136 0.036090 0.0202186 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.021286 0.02	ABLE		_	PARAMETER ESTIMATE	STANDARD	# RATIO	PROB>   T
1 2.204547 0.165228 13.3425 1 3.425							
0.191848	INTERCEPT	7		10454	. 16522	342	000
1 -0.212136 0.038790 -5.4688 0.022186 0.024635 0.0348790 -5.4688 0.022186 0.024635 0.024635 0.043607 10.6329 11.9560 1 0.405770 0.033939 11.9560 0.012636 1 0.06681 0.012656 0.012656 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012636 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0.012638 0	SUPER	-		19184	.05004		•
1 0.022186 0.024035 0.02313	SACTO	-		11213	.03879	<b>1</b> 68	•
1 0.463667 0.043607 -10.6329 1 0.405770 0.013939 -15.6426 1 0.006173606 0.048876 -2.3827 1 0.006173606 0.012656 -2.3827 1 0.006173606 0.016236 -2.3827 1 0.006173606 0.048876 -2.3827 1 0.033195 0.012339 -5.2496 1 0.039739 0.052569 -0.7559 1 0.039739 0.052569 -0.7559 1 0.039739 0.053634 -6.5172 1 0.039739 0.053634 -6.5172 1 0.039739 0.053634 -6.5172 1 0.039739 0.053634 -6.5172 1 0.023661 0.085497 -0.2791 2 0.036599 0.033268 R-SQUARE  PARAMETER STANDARD T RATIO PRO ESTIMATE ERROR T RATIO PRO 1 0.083123 0.0124653 22.0654 1 0.083123 0.012898 -1.9999 1 0.083123 0.012898 -1.9999 1 0.00977441 0.009548019 -0.5260 1 0.00977441 0.009548019 -0.5260 1 0.014928 0.013249 -2.3008 1 0.014928 0.0322981 -0.5260 1 0.014928 0.0322981 -0.5260 1 0.010750 0.004650 -0.48996	V152	7		32218	.02403	923	•
1 0.405770 0.033939 11.9560 1 0.012456 0.020909	V156W	~		16366	.04360	632	٠
1 -0.117980 0.020909 -5.6426 0.01263 0.01263 0.01263 0.01263 0.012656 -2.3827 0.012636 0.012636 -2.3827 0.012636 0.012336 4.1070 0.0133325 0.012038 -5.2496 0.052569 0.023645 0.052569 -0.7559 0.012038 0.052569 -0.7559 0.052569 0.053634 -6.5172 0.053634 0.053634 0.053634 0.053634 0.023961 0.065363 0.0653634 0.023961 0.065919 0.053634 0.02396 0.023661 0.037368 0.037368 0.037368 0.037368 0.037368 0.037368 0.037368 0.037368 0.0336263 0.018133 0.032667 0.036561 0.0036610 0.0124653 0.025604 0.025604 0.025604 0.025604 0.025604 0.025607 0.036610 0.01369119 0.025604 0.052607 0.0037348 0.032661 0.039660 0.039660 0.039660 0.039660 0.039660 0.039660 0.039660 0.039660 0.039660 0.039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039660 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.0039600 0.003	V157C			10577	.03393	926	•
1 0.006173606 0.048876 0.1263	V158	-		11798	.02090	642	•
-0.030156	V159A	7		17360	.04887	.126	•
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1 -0.039739	27.0			16319	.01203	249	•
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#SE 2206.305 FRAFIO DFE 3484 PROB>F PROBPE DFE 3484 PROB>F PROB>F PROB>F PROB>F PROBPE DFE 3484 PROB>F PROB>F PROB>F PROBPE DFE STINATE STANDARD T RATIO PRO 0.665919 0.0124653 22.0654 0.0365919 0.037755 17.6380 0.036263 0.031898 2.5267 0.036263 0.031898 2.5267 0.031898 0.025604 4.2555 0.031898 0.025604 4.2555 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318916 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.0318918 0.031	Dans.	• •		7000	01290	270	•
#SE 2206.305 F RATIO PEE 3484 PROB>F PROBP PROBPE P	<b>911</b>	<b>→</b> ;	1	90000			• 1
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PARAMETER         STANDARD         T RATIO         PROE           1         2.750515         0.124653         22.0654         0.037755         17.6380         0.037755         17.6380         0.037755         17.6380         0.037755         17.6380         0.037755         0.037755         0.037755         0.037755         0.037755         0.03775         0.03775         0.03775         0.03775         0.03775         0.03777         0.03777         0.03777         0.03777         0.03777         0.03777         0.03777         0.03777         0.03777         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.0377         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037         0.037		1.8		MSK	.63326	R-SQUARE	0.1916
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-0.189160 0.029265 -6.4638 0.036263 0.018133 -1.9999 0.018133 -1.9999 0.018133 -1.9999 0.018133 -1.9999 0.018133 -1.9999 0.0108181 0.025604 4.2555 0.0084837 0.025604 4.2555 0.0084837 0.035874 -3.0816 0.03097441 0.009548019 -1.0237 0.03097441 0.039501 5.0990 0.0104938 0.039501 5.0990 0.012348 0.039501 5.0990 0.012348 0.039501 -0.017348 0.039581 -0.5260 0.018190 0.046465 0.040463 -2.48999 0.0040463 -2.48999 0.0040463 -2.48999 0.0064502 -0.8764 0.0056528 0.0064502 -0.8764 0.0064502	SIIOPP	1		0.665919	.03775	9	•
1 -0.036263 0.018133 -1.9999 0.0081123 0.032898 2.5267 0.025604 4.2555 0.025604 4.2555 0.025604 4.2555 0.025604 4.2555 0.0084817 0.036814 -2.30816 0.036813 0.036819 -1.0237 0.036819 0.036819 0.036819 0.036819 0.036819 0.03249 0.032891 0.05260 0.039660 0.039660 0.039660 0.04899 0.0064522 0.0064502 -0.8764 0.0056528 0.064502 -0.8764 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.008818 0.0		'-		-0.189160	.02926	•	•
1 0.083123 0.032898 2.5267 0.0108959 0.025604 4.2555 0.025604 4.2555 0.025604 4.2555 0.025604 4.2555 0.01084837 0.015774 -3.0816 0.0108741 0.009548019 -1.02308 0.0201416 0.039501 -1.0237 0.009548019 -1.0237 0.0049928 0.012249 4.0761 0.0049928 0.012249 4.0761 0.0049465 0.0039660 -0.4586 0.0039660 -0.4586 0.0039660 -0.4586 0.0056528 0.004663 -2.48999 0.0056528 0.004502 -0.8764 0.0056528 0.004502 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.0048660 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004860 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004863 -0.8764 0.004864 0.004864 -0.8764 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.004864 0.0048	V152			-0.036263	01813	σ.	•
0.108959	71564		_	0.083123	.03289	s,	•
1     -0.048610     0.015774     -3.0816     0.036874       1     -0.084837     0.036874     -2.3008     0.0       1     -0.0977441     0.00554801     -1.0237     0.0       1     0.049928     0.012249     4.0761     0.0       1     -0.017348     0.032981     -0.5260     0.0       1     -0.046465     0.032981     -0.5260     0.0       1     -0.018190     0.040463     -2.4899     0.0       1     -0.056528     0.064502     -0.8764     0.0	V157C			0.108959	.02560	~	•
1     -0.084837     0.036874     -2.3008     0.       1     -0.00977441     0.009548019     -1.0237     0.       1     0.201416     0.039501     5.0990     0.       1     0.049928     0.012249     4.0761     0.       1     -0.017348     0.032981     -0.5260     0.       1     -0.046465     0.00908186     -5.1162     0.       1     -0.018190     0.039660     -0.4586     0.       1     -0.100750     0.040463     -2.4899     0.       1     -0.056528     0.064502     -0.8764     0.	V158			0.04861	.01577	٥.	•
1     -0.00977441     0.009548019     -1.0237     0.       1     0.201416     0.039501     5.0990     0.       1     -0.049928     0.012249     4.0761     0.       1     -0.017348     0.032981     -0.5260     0.       1     -0.046465     0.00908186     -5.1162     0.       1     -0.0189860     0.039660     -0.4586     0.       1     -0.100750     0.040463     -2.4899     0.       1     -0.056528     0.064502     -0.8764     0.	V159A	-	_	0.08483	.03687	۳.	•
1 0.201416 0.039501 5.0990 0. 1 0.049928 0.012249 4.0761 0. 1 -0.017348 0.032981 -0.5260 0. 1 -0.046465 0.00908186 -5.1162 0. 1 -0.018190 0.039660 -0.4586 0. 1 -0.100750 0.040463 -2.4899 0. 1 -0.056528 0.064502 -0.8764 0.	V160	~	1	.0097744	.00954801	٥.	•
1 0.049928 0.012249 4.0761 0. 1 -0.017348 0.032981 0.5260 0. 1 -0.046465 0.00398186 -5.1162 0. 1 -0.018190 0.039660 -0.4586 0. 1 -0.100750 0.040463 -2.4899 0. 1 -0.056528 0.064502 -0.8764 0.	V165	-		0.20141	.03950	٥.	•
1 -0.017348 0.032981 -0.5260 0. 1 -0.046465 0.00908186 -5.1162 0. 1 -0.018190 0.04660 -0.4586 0. 1 -0.100750 0.040463 -2.4899 0. 1 -0.056528 0.064502 -0.8764 0.	V168	-		0.049928	.01224	٥.	•
1 -0.046465 0.00908186 -5.1162 0. 1 -0.018190 0.039660 -0.4586 0. 1 -0.100750 0.040463 -2.4899 0. 1 -0.056528 0.064502 -0.8764 0.	V169	-		0.01734	.03298	'n	•
1 -0.018190 0.039660 -0.4586 0. 1 -0.100750 0.040463 -2.4899 0. 1 -0.056528 0.064502 -0.8764 0.	V172	-	_	-0.046465	.0090818	つ.	•
1 -0.100750 0.040463 -2.4899 0. 1 -0.056528 0.064502 -0.8764 0.	MHS	7		-0.018190	.03966	₹.	•
1 -0.056528 0.064502 -0.8764 0.	BNHS	7		-0.100750	.04046	₹.	•
	OTH	7		-0.056528	.06450	æ	•

Table C.6--continue

1.100144 BRRUDARD 0.16434 0.0389344 0.0383344 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808 0.0520808	MODEL: MODEL01	388	3835.167	PROB>F	0.0001
PARAMETER STANDARD  ERFT 1 2.864641 0.164347 11  -0.185590 0.049777 11  -0.1864641 0.164347 11  -0.1864641 0.164347 11  -0.1864641 0.164347 11  -0.186418 0.038584  -0.044236 0.038584  -0.186418 0.038584  -0.186418 0.038584  -0.186418 0.038584  -0.03803186 0.038584  -0.03803186 0.043484  -0.0380318 0.043484  -0.074655 0.011974  -0.074655 0.011974  -0.074655 0.011974  -0.074655 0.043484  -0.058404 0.052489 0.052189  -0.058404 0.0385042  -0.0393135 0.043987  -0.0393135 0.043987  -0.045838 0.01124  -0.045838 0.01124  -0.05611 0.01581  -0.045838 0.01124  -0.045838 0.01124  -0.045838 0.01124  -0.045838 0.01124  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013872  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.01373  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.058334 0.013873  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583433 0.014271  -0.0583434 0.011271		HSH	1.100794	R-SQUARE	0.1400
TEPT 1 2.864641 0.164347 11 0.66344	-	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>  T
1	ACEPT 1	2.864641		17.4305	0.0001
1		0.565266		-4.8127	
0.122587 0.043374   0.180418 0.033758   0.180418 0.023758   0.023758   0.0216280   0.0216280   0.0216280   0.0216280   0.0216280   0.0216280   0.0216219   0.0216219   0.0216219   0.022289   0.023484   0.023484   0.023484   0.023484   0.023484   0.02348   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.023484   0.042714   0.02344   0.042714   0.02344   0.014271   0.023434   0.014271   0.023434   0.014271   0.023434   0.014271   0.023434   0.075149		-0.044236		-1.8504	
0.180418 0.033758		0.222587		5.1318	•
1 -0.142421 0.020798		0.180418		5.3445	•
0.0122030 0.048616   0.003803156 0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012080   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010   0.012010		-0.142421		-6.8480	•
0.061906   0.012086   0.016149   0.061906   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908   0.061908		-0.12203		-2.5101	•
0.021906   0.03484     0.026318   0.043484     0.026219   0.053248     0.057288   0.053348     0.057288   0.055348     0.057288   0.055348     0.058404   0.085042     0.058404   0.085042     0.058404   0.0859580   R     RSTANDARD   F     ESTIMATE   ERROR   T     0.385115   0.043987     0.05045499   0.0145228     0.05045499   0.014329     0.05045499   0.018379     0.05045499   0.018379     0.05046499   0.018379     0.05046499   0.018379     0.05046499   0.018379     0.05046499   0.014271     0.045838   0.014271     0.045838   0.014271     0.054393   0.047142     0.054234   0.075149		.00380315		1.3021	•
1 -0.086189   0.043484   0.082219   0.082289   0.087588   0.085042   0.085042   0.085042   0.087588   0.085042   0.087588   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.0850423   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085042   0.085		0.001900		7001.1	•
MODELO1   1 -0.074655   0.052289   1 -0.057588   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.055289   0.0552		-0.041035		0850	•
1		916990.0-		-1.9050 -6.9348	•
MODELO1 SSE 2994.775 F 0.05348		-0.04600		5 1973	• •
MODELO1 SSE 2994.775 F 3484 P PRRAMETER STANDARD T 2.962433 0.145228 2 1 0.385115 0.043987 1 0.385115 0.034095 1 0.056149 0.013329 1 0.056149 0.018379 1 0.056163 0.014271 1 0.045838 0.014271 1 0.045838 0.014271 1 0.045838 0.014271 1 0.054393 0.014271 1 0.054393 0.014271 1 0.054393 0.014271 1 0.054393 0.047142		0.50519		-1.0795	•
REPT 1 2.9624.775 F  PARAMETER 3464 R  SIE DF ESTIMATE ERROR T  1 0.385115 0.043987  1 0.045499 0.021126  1 0.065499 0.021126  1 0.065649 0.029831  1 0.065019 0.018379  1 0.065019 0.018379  1 0.065019 0.018379  1 0.065019 0.016271  1 0.054393 0.0427142  1 0.054393 0.0427142		0.058404		0.6868	
MODELO1   SSE   2994.775   F	• • • • • • • • • • • • • • • • • • •	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1		
MSE 0.659580 R PARAMETER STANDARD  JLE DF ESTIMATE ERROR T  1 0.385115 0.043987  1 -0.393135 0.034095  1 -0.004599 0.029831  0.166849 0.029831  1 -0.047913 0.018379  1 -0.047913 0.018379  1 -0.047913 0.018379  1 -0.047913 0.018379  1 -0.056811 0.016221  1 -0.05534 0.014271  1 0.054393 0.047142  1 0.054234 0.075149	_	1000 1000	994.	F RATIO	38.12
PARAMETER STANDARD  1. 2.962433 0.145228 2 2.862433 0.145228 2 2.962433 0.043987 1. 0.393135 0.034095 1. 0.0045499 0.034095 1. 0.0045499 0.034095 1. 0.047913 0.018379 1. 0.047913 0.018379 1. 0.047913 0.018379 1. 0.045838 0.014271 1. 0.095234 0.038425 1. 0.095234 0.014271 1. 0.054393 0.047142 1. 0.054234 0.075149		DFE	7 0	PROBAE DE	1416
PARAMETER STANDARD  ESTIMATE ERROR T  2.962433 0.145228  20.145228  1 -0.393135 0.043987  1 -0.065489 0.021126  -0.0650165 0.018329  1 -0.067913 0.018329  1 -0.047913 0.018379  1 -0.0947913 0.018379  1 -0.0945838 0.042966  1 -0.095234 0.038425  1 -0.095234 0.046201  1 0.054393 0.046142  1 0.054393 0.046142		36	. 60	THE WORLD	
JEE DF ESTIMATE ERROR T 1 2.962433 0.145228 26 1 0.385115 0.043987 26 1 0.065499 0.021126 -0 1 0.065499 0.021126 -0 1 0.065849 0.029831 1 0.067913 0.018373 -2 1 0.047913 0.018373 -2 1 0.045838 0.014271 -6 1 0.095234 0.038425 -2 1 0.054393 0.046142 1		PARAMETER	STANDARD		
2.962433 0.145228 26 1		ESTIMATE	ERROR		PROB>   T
1 0.385115 0.043987 11 0.393135 0.043987 11 0.393135 0.034095 -11 0.055165 0.034095 -12 0.055165 0.038139 11 0.056189 0.018373 -2 0.042964 11 0.045838 0.014271 1 0.056234 0.038425 -2 0.05611 0.056393 0.045149 11 0.054234 0.036424 0.054234 0.05424 0.05424 0.054234 0.075149	RCEPT	2.962433	.1452	20.3985	•
1 -0.393135 0.034095 -11 1 -0.0045499 0.023126 -0 1 0.166849 0.029831 1 -0.047913 0.018373 -2 1 -0.0316038 0.042966 -3 1 -0.0316038 0.018373 -2 1 0.129700 0.046022 -3 1 0.045838 0.014271 -0 1 0.095234 0.038425 -2 1 0.054393 0.047142 1		0.385115	.0439	8.7553	•
1 -0.0045499 0.021126 -0.050165 0.0383129 1 0.050165 0.0383129 1 0.0641913 0.0163131 0.0163131 0.0156259 0.0641966 -0.02831 0.04521 0.005531 0.05611 0.016281 0.054231 0.045149 0.054231 0.055149 0.075149		0.39313	.0340	-11.5305	•
1 0.050165 0.038329 1 -0.166849 0.029831 1 -0.156259 0.042956 1 -0.0316038 0.041324 1 -0.095234 0.01424 1 -0.095234 0.01422 1 -0.095234 0.014271 1 -0.066611 0.016581 1 0.151730 0.047142 1 0.054334 0.047142		.004549	.0211	-0.2154	•
1 0.166849 0.029831 5 0.047913 0.018373 2 1 0.047913 0.018373 2 1 0.00316038 0.011124 2 1 0.095234 0.014271 1 0.095234 0.014271 1 0.095234 0.01681 1 0.151730 0.04626 1 1 0.054393 0.047142 1 0.054234 0.075149		0.050165	.0383	1.3088	•
1 -0.047913 0.018373 -2 1 -0.156259 0.042966 -3 1 -0.00316038 0.01124 -6 1 0.045838 0.014271 -6 1 -0.095234 0.038425 -2 1 -0.066611 0.016581 -6 1 0.151730 0.04626 3 1 0.054393 0.047142 1		0.166849	. 0298	5.5932	•
1 -0.0156259 0.042966 -1 1 -0.00316038 0.011124 -1 1 0.045838 0.014271 1 -0.095234 0.038425 -2 1 -0.066611 0.010581 -6 1 0.054393 0.046142 1 0.054234 0.075149		0.04791	.0183	-2.6070	•
1 -0.00315038 0.0111124 1 0.045838 0.014621 1 0.095234 0.038425 -2 1 0.066611 0.010581 -6 1 0.151730 0.046206 1 0.054393 0.04742		-0.15625	92.00	2/50.5-	•
1 0.045838 0.014271 3 0.045834 1 0.014271 3 0 0.045834 0.010581 -2 0.05534 0.010581 -6 0.05581 0.05583 0.047142 1 0.054234 0.075149 0.0		0.0031603	1110.	-0.2041	•
1 -0.095234 0.038425 -2 1 -0.066511 0.010581 -6 1 0.151730 0.046206 1 0.054393 0.047142 1		0.129/00		3 2120	•
1 -0.066511 0.010581 -6 1 0.151730 0.046206 1 0.054393 0.047142 1 1 0.054234 0.075149		0.045838	0384	-2.4784	• •
1 0.151730 0.046206 3 1 0.054393 0.047142 1 1 0.054234 0.075149 0		-0.066611	.0105	-6.2953	
3 1 0.054393 0.047142 1 1 0.054234 0.075149 C		0.151730	.0462	3.2838	0.0010
1 0.054234 0.075149 0		0.054393	.0471	1.1538	•
	-	0.054234	.0751	0.7217	•

Table C.6--continued

MODEL:	MODEL01		200	4824.933	F RATIO	22.05	
DEP VAR	PAYDETRM	_		1.364663	R-SQUARE	0.0867	
VARIABLE		ğ	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>  T	
INTERCEPT	<b>6</b> 4	٦.	2.549068		13.8282	0.0001	
SUPER		<b></b>	-0.041473	25	958		
V152			0024169	.02681	060	•	
V156W		-	0.01194	.04865	245	۳.	
V157C		⊶.	0.07204	.03786	.905	ÖĠ	
V158		٠ -	0.00183	75570.	פינים פינים		
477A		<b>-</b>		01412	9069	•	
2917		•	0.08987	.05841	538	7	
V168		-		.01011	024	0	
V169		_		.04877	. 276	ä	
V172		~		.01343	.125	ö	
MAS MAS		-		.05864	. 165	ö	
BNHS		-		.05983	. 224	9	
OTH		-		.09538	. 151	9	
! ! ! ! !	 						
MODEL	MODEL 01		888	28	F RATIO	=	
			DFE	1	PROB>F	٥.	
DEP VAR:	UNIONSAT		MSR	\$	R-SQUARE		
			PARAMETER	STANDARD			
VARIABLE		DF.	ESTIMATE	ERROR	T RATIO	PROB>   T	
INTERCEPT	<b></b>	-		12067	34	•	
SUPER		-		03654	33	•	
SACTO		-		02833	7	•	
V152		<b>,</b>		01755	8	•	
300				20100	ה מ	٠	
V15.0		<b>-</b>		01527	5.5		
V159A		- ،	ā	03569	2		
V160			ö	92429	49	•	
V165		-		03823	36	•	
V168		<b></b>		01185	8	•	
V169		⊶.		0.03192	5	•	
7172		٦.	-0.030571	0.008791724	-3.4773	0.0005	
WAS		<b>→</b> -		75050	7	•	
BINE		<b>→</b> -		17650	2 6		
5		•		,	3	•	

Table C.6-continued

HODEL: HODELOI DEP VAR: ORGINVOL	ي	SSE DETE	885.655016 3484 0.254206	F RATIO PROB>F R-SQUARE	39.59 0.0001 0.1456
VARIABLE	ď	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT SUPER SACTO VISS		50526 24135 09916 84665	0.078977 0.023921 0.018541 0.011488	. 383 . 948 . 348	0.0001 0.0001 0.0001 0.8689
V1558 V158 V168 V168 V169 V169	чанананан	0.065219 0.016981 0.016981 0.020372 0.065219 0.019529	0.00994301 0.009994301 0.023362 0.025027 0.0276063 0.0276063 0.020896	-6.1268 -6.7268 -0.7268 -1.9774 -3.1213 -3.1173 0.3884	0.000000000000000000000000000000000000
BNHS OTH		10455	0.025637	. 764	0.0001
MODEL: MODELO! DEP VAR: SUPVMUNT	H	300 BF3 BSM	2496.253 3484 0.716490	F RATIO PROB>F R-SQUARE	31.83 0.0001 0.1205
VARIABLE	0£	PARAMETER ESTIMATE	STANDARD ERROR	T RATIO	PROB>[T]
INTERCEPT SUPER SACTO V155 V155 V156 V158 V165 V165 V168 V168 V172 WHS	ммммммммммммммммммммммммммммммммммммм	3.233705 0.396025 -0.235345 -0.010708 0.047331 0.065564 -0.065564 0.0144024 0.0144024 0.058352 -0.058352 -0.058352	0.132591 0.040159 0.031128 0.031287 0.034993 0.016779 0.016779 0.035222 0.013629 0.0350829 0.0350829 0.042185 0.042185	24.3886 -0.5552 -0.5552 -0.5552 -0.0518 -0.0518 -0.0518 -0.0509 -0.0509 -0.0509	0.000000000000000000000000000000000000
HES	4	0.033100	. 00000	•	0.040.0

Table C.7
RECRESSION RESULTS FOR SUPERVISOR VARIABLES AND SCALES

VARIABLE DF ESTINATE ST. VARIABLE DF ESTINATE E ST. VARIABLE DF ESTINATE E ST. VAS. VISS VISS VISS VISS VISS VISS VISS VI	772 PRC	P RATIO	0.0001
PARAMETER 55  1	<b>*</b>	-SQUARE	•
10.003888951 10.00388951 10.003880951 10.00385797 10.00385797 10.00385797 10.0038589 10.0035599 10.0035699 10.0035699 10.0035699 10.0035699 10.0035699 10.0035699 10.0035699 10.0035699 10.0035699 10.0035699	STANDARD T F	RATIO	PROB> [T]
DDELO1  10.003880951  10.003880951  10.003880951  10.003880951  10.003880951  10.003880951  10.003880951  10.003880951  10.00388813  10.00088813  10.00088813	533996 5.	9564	0.0001
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PARAMETER 31  1		-SQUARE	55
1	STANDARD ERROR T R	RATIO	PROB> [T]
1 -0.147669 0.041592 0.041592 0.0113030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.0130300 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.0130300 0.013030 0.013030 0.013030 0.013030 0.013030 0.013030 0.0130	556095	4231	.000
0.041592 0.123030 0.123030 0.123030 0.0086496 0.035685 0.095014 0.095014 0.095014	103559	4259	.154
0.123030 0.211769 0.00886496 0.035685 0.095014 0.095014 0.198843 0.0198843	065818	63.19	. 527
-0.00886496 0.00886496 0.00886496 0.0095885 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.0095014 0.	105993	1607	246
-0.076585 0.035685 0.095014 -0.00618843 -0.198573	0.0437	000	200
0.035685 0.095014 -0.00618843 -0.198573 0.0061885	124124	6170	537
0.095014 -0.00618843 -0.198573	028427	2553	. 209
-0.00618843 0. -0.198573 0.	224995	4223	.672
0 005040	041656	1486	.881
	103444	9190	
0 086760.0	120120	0.7908	0.4293
-0.118876 0.	132863	8947	.371

Table C.7--continued

ij		8.00 8.00 8.00 8.00 8.00 8.00 8.00 8.00	896.257381	F RATIO	0.0007
DEF VAR: VISU		PARAMETER	n asi	R-SQUARE	
VARIABLE	ď	ESTIMATE	ERROR	T RATIO	PROB>   T
INTERCEPT	-	2.380752	. 52388	4.5444	.000
SACTO	→.	0.314468	.09756	3.2233	
V152	<b>-</b> 4 ,	-0.035844	.06200	-0.5781	266
M9612	٦-	0.2/0420	. 09963	7.007	900
V15/C	-	•	04218	1.1366	256
0517 V159A	•		0.116934	-1.2219	0.2221
V160	-	-0.016450	.02678	0	539
VI65	-	•	.21196	0	. 592
V168	_	-0.025726	.03924	-0.6555	. 512
V169	→,	•	.09745	О.	. 529
V172	⊣.	0.024895	.02467	1.0090	313
SHES.	٠,	-0.004/8/	91611.	-0.5/26	72.
	۰,	-0.1/6164	91671.	1.4231	202
<b>1</b>	• [	1169510		96/0.7	
MODEL: MODEL01		200	982.535827	F RATIO	1.25
		DFE	172	PROB>F	.234
DEP VAR: V131		asw	1.272715	R-SQUARE	022
		PARAMETER	STANDARD		
VARIABLE	DF	ESTIMATE	ERROR	T RATIO	PROB>[T]
INTERCEPT	-	3.343322	.54852	.095	.000
SACTO	-	-0.197250	.10214	. 931	.053
V152	-	-0.078417	.06492	. 207	. 227
V156W	-	0.119087	.10454	. 139	. 255
V157C	-	0.021846	.06947	. 314	. 753
V158	_	0.038359	.04416	. 868	. 385
V159A	-	Ÿ	.12243	. 232	. 218
V160	-	0.002413205	.02804	. 086	.931
V165	-	-0.298287	. 22193	344	.179
V168	<b>,</b>	0.070729	.04108	721	.085
V169	┙.	-0.062840	. 10203	615	.538
V172	⊶ -	-0.015171	.02583	787	700
SHA	۰,	0.016503	12105	75.0	200
OTH	٠.	-0.011394	0.239777	-0.0475	0.9621
	ł				

Table C.7--continued

3.96 0.0001 0.0670	PROB>[T]	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	5.70 0.0001 0.0936	PROB>   T   C   O   O   O   O   O   O   O   O   O	
F RATIO PROB>F R-SQUARE	RATIO PR	.8353 .8353 .8253 .8275 .3528 .7711 .8596 .2130 .8598 .0241 .0539 .9485 .0332	F RATIO PROB>F R-SQUARE	54 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.1704
1095.43 F 772 PB .418951 R-	STANDARD ERROR	129216 129276 129276 129276 129276 129276 129276 129276 129279 129279 129279 129279 129279 129279 129279	846.432396 F 772 PE 1.096415 R-	STANDARD T T 1	
SSE 10	PARAMETER ST. ESTIMATE EI	2.241908 0.273457 0.273457 0.312134 0.172602 0.035959 0.240401 0.318067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067 0.218067	33E 846.4 DFE 3.0	PARAMETER 13.307858 0.019548 0.0589318 0.0589318 0.0587381 0.0587381 0.055231 0.055228 0.055228 0.055228 0.055228 0.055228 0.055228 0.055228 0.055228	ó
<b>~</b>	PARA DF EST	0.00.00.00.00.00.00.00.00.00.00.00.00.0	ed.	PARA 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	99
MODEL: MODELO1 DEP VAR: V132	VARIABLE	INTERCEPT SACTO V152 V156W V157C V158 V169 V168 V169 V172 WHS WHS WHS	MODEL: MODELO1 DEP VAR: V133	VARIABLE INTERCEPT SACTO V152 V158 V159A V159A V160 V160 V169 V169	BNHS

Table C.7--continued

MODEL: DEP VAR:	MODEL01 V134		SSE	937.058804 772 1.213807	F RATIO PROB>F R-SQUARE	7.65 0.0001 0.1218
VARIABLE		D.	Parameter Estimate	STANDARD	T RATIO	PROB>   T
INTERCEPT 9ACTO V152 V156W V157C V159 V165 V165 V165 V172 W172 W173		ппппппппппппппппппппппппппппппппппппппп	3.528561 -0.471775 -0.100768 -0.13704 -0.073805 -0.558027 -0.1568778 -0.199902 -0.199902 -0.040045	0.53 0.09957 0.069957 0.063401 0.063401 0.019566 0.027383 0.025330 0.025230	-4.7292 1.5894 1.5894 -1.4004 -1.7496 -2.1580 0.5071 -2.6243 -2.6061 -1.5872 -1.5872	00000000000000000000000000000000000000
ОТН		•	0.376815	0.234162	1.6092	0.1080
MODEL: DEP VAR:	MODEL01 V135		SSE	1142.064 772	F RATIO PROB>F R-SQUARE	2.82 0.0004 0.0487
VARIABLE		DF	Parameter Estimate	STANDARD	T RATIO	PROB>  T
INTERCEPT SACTO V152 V156W V156W V159A V159A V169 V169 V169 V172 WHS BNHS		пепененняния	3.66562 -0.212875 -0.070927 -0.194338 -0.070185 -0.0139334 -0.113753 -0.065979874 -0.055501 -0.042842 -0.047158 -0.047158 0.563240 0.174991	0.591378 0.110130 0.069994 0.112718 0.074906 0.031999 0.239270 0.110007 0.127853 0.127853 0.127853	6.1985 -1.9329 -1.0133 1.7241 0.9370 -1.9727 -0.8618 0.1978 -0.2320 0.6888 -0.3895 -1.6931 4.4092 1.2385	0.0001 0.0536 0.3112 0.3851 0.3889 0.3889 0.8889 0.8166 0.6970 0.0008 0.2159

Table C.7--continued

;; ;		8 0 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	862.136351	F RATIO PROB>F	5.12 0.0001 0.0850
DEF VAKI VI30	a C	PARAMETER	STANDARD	0144	PROB9-14
VARIABLE	Š		TOWNS TO THE PARTY OF THE PARTY		
INTERCEPT	~		0.513816	4.7542	0.0001
SACTO	-4	-0.349708	0.095686	~	9,
V152	-4	-0.036061	0.060614	-0.5930	'n.
V156W	-	-0.062931	0.097934	-0.6426	S.
V157C	-	0.219515	0.065082	3.3791	9
VI 58		-0.089141	0.041372	-2.1546	٥,
V159A	-	-0.087238	0.114687	-0.7607	7
V160	-	0.019118	0.026266	0.7279	▼ (
V165	-	0.044992	0.207889	0.2164	₽,1
V168	-	0.153535	0.038489	3.9891	9,
V169	-	-0.142276	0.095579	-1.4886	∹
V172		-0.017090	0.024200	-0.7062	7
WHS	-	0.248584	0.110987	2.2398	•
BNH3		-0.242082	0.122762	-1.9720	9,
отн	-	0.058349	0.224606	0.2598	•
MODEL: MODEL01		388	838.617029	FRATIO	
;			7/1	PRODY'S	0.00
DEF VAR: VI3/		3		The state of the s	•
		PARAMETER	STANDARD		
VARIABLE	OF.	ESTIMATE	ERROR	T RATIO	PROB>   T
FOR CORENT	-	3.963064		7.8204	
SACTO STATE	۰			-5.8202	
V152				1.2420	•
V156W	-			-1.0571	•
V157C	-			0.6491	•
VISB	_			-1.0794	
V159A	-			-0.2170	•
V160	7			0.8010	•
V165	_			-1.6016	٠
V168	<b>-</b>			0.6346	•
V169	<b></b> 4 .			V 0 40 .	•
V172	<b>-</b> - ,			0.5350	•
WHS	٦.	-0.05/565	201010	0.5239	7.09.0
BNHS	<b>-</b> -			0.9873	
<b>E</b> 35	4			,	•

Table C.7--continued

MODEL: MODELO1	10,	386	735.302943	F RATIO PROB>F	6.23
DEP VAR: V138		NSM NSM	0.952465	R-SQUARE	0.1015
VARIABLE	0	Parameter Estimate	STANDARD	T RATIO	PROB>  T
INTERCEPT	-	3.305183	.47451	6.9653	•
SACTO		-0.058233	.08836	-0.6590	•
V152	-	0.035452	.05616	0.6312	•
V156W		-0.192407	1060.	-2.1274	
V157C	<b>~</b>	0.190066	.06010	3.1623	•
V158	-	-0.00302715	.03820	-0.0792	•
V159A	→ .	0.261509	0.105915	2.4690	0.0138
V160	<b></b> 4 ,	0.008995281	.02425	0.3708	•
V165	٠,	-0.095025	19198	-0.4949	•
V168	<b>-</b>	-0.013346	.03554	-0.3755	•
V169	<b></b>	-0.191035	.08826	-2.1642	•
V172	-	0.044416	.02234	1.9874	
WHS	<b>→</b>	-0.437982	10249	-4.2731	•
BNH3		-0.419096	.11337	-4.2259	•
отн	<b>~</b>	-0.790330	. 20742	-3.6101	•
	f 	, , , , , , , , ,	1 † † † † † † † †	1 1 1 1 1 1 1 1 1 1 1 1	 
MODEL: MODELO1	01	335	843.819354	F RATIO	1.64
		DFB	77	PROB>F	•
DEP VARI V139		MSE	1.093030	R-SQUARE	0.0289
		PARAMETER	STANDARD		
VARIABLE	DF	ESTIMATE	ERROR	T RATIO	PROB>(T)
INTERCEPT	7		٠:	•	000
SACTO	7		٧.	•	.010
V152	-		٧.	•	. 725
M95!A	~		٠.	•	.622
V157C			٧.	•	. 428
2.58	_		٠.	•	. 377
Ċ	<b>-</b>		Ξ,	•	.356
			٠.	•	. 647
	<b></b> ,			•	.570
<b>x</b>	<b>-</b>		٠,٠	•	976
	<b>→</b> -		•	•	000
	<b>-</b>		-:	0.6440	. 370 A A 2
			:-	•	. E
	٠.	0.155370	0.222207	0.6992	0.4846

Table C.7--continued

	HODREOI		25 C 1	956.739919	F RATIO PROB>F B-SCIARE	0.0001
VARIABLE		à	PARAMETER ESTIMATE	STANDARD	T BATIO	PROB>[*]
INTERCEPT SACTO V152	<b>84</b>		3.600196 -0.44583 -0.090432	0.541274 0.100799 0.064064	6.6513 -4.4106 -1.4116 -0.6524	0.0001 0.0001 0.1585 0.5143
V150W V151C V158 V159A			0.274136 -0.047228 -0.177064 0.047251	0.068559 0.043589 0.120813 0.027669	1.0836 -1.4656 -1.7077	0.0000
V165 V168 V172 WHS BNHS			-0.263732 0.102710 0.006523672 -0.068237 0.190901 -0.098670	0.218998 0.040546 0.100687 0.116919 0.129922 0.236609	-1.2043 2.5332 0.00648 -2.67648 1.6335 0.7630	0.228 0.0018 0.0076 0.1028 0.4657 1457
HODEL: DEP VAR:	MODELO1 V141	!	160 160 160	743.962021 772 0.963681	F RATIO PROBSF R-SQUARE	4.19 0.0001 0.0706
VARIABLE		ă	Parameter Estimate	STANDARD	T RATIO	PROB>   T
Intercept Sacto	<b>L</b>		1.971708	0.477304	4.1309	0.0001
152 1564 157C			0.085788 0.085788 0.093169 0.028369	0.090975 0.060457 0.038433	0.9430 1.5411 0.7382	0.3460 0.1237 0.4606
V159 V169 V172 V173			-0.287460 0.051938 -0.138896 0.079144 -0.134859 -0.0645011	0.106537 0.024399 0.033116 0.035754 0.088787 0.103100	-2.6982 -0.1192 -0.2136 -0.2869	0.0071 0.0336 0.0271 0.1292 0.0119
SENS OFF			0.016996	0.114038	0.1490	0.8816 0.1656

Table C.7--continued

ä		M M G G	914.388175	F RATIO PROB>F	5.66 0.0001
UEF VAR! VIS.	2	PARAMETER ESTIMATE	STANDARD ERROR	# BATIO	• -
	-		0 529158		0.0001
SACTO	-	-0.261169	0.098543	-2.6503	0.0082
V152	-4	٠.	0.062630	.816	0.4147
V156W	-	٦	0.100858	. 518	0.6043
V157C	<b>~</b>	7	0.067025	. 292	0,0001
V158	٠,	3	0.042608	.338	0.0001
VI 59A	⊣,	Ξ,	0.118111	585	0.1141
0160	٦,		0.027050	25.	0.0310
V165	٦,	•	0.214096	ניני	0.7410
0 I O I	٠.	; ;		750.	9000
2012	٠,	; ;		. 380 666	0.00
2/1 <b>/</b>	- ۲		0.114301	37	0.0613
	۰,	•	0.126427	785	0.4327
	•	-0.176034	0.231312	62	0.4469
					: : : : : : : : : : : : : : : : : : : :
MODEL: MODEL01		388	725.172680	F RATIO	99.7
		120	172	PROB>F	0.0001
DEP VAR: V143		MSE	0.939343	R-SQUARE	•
		PARAMETER	STANDARD		
VARIABLE	DF	ESTIMATE	ERROR	T RATIO	PROB>   T
INTERCEPT	-	4.009318	0.471238	8.5080	8
SACTO	-	-0.474365	0.087757	-5.4055	8
V152	-	0.079734	0.055775	1.4296	.15
V156W	-	-0.203682	0.089819	-2.2677	9
V157C	-	0.012299	0.059689	0.2060	8
V158	_	-0.023295	0.037944	-0.6139	3
V159A	<b>-</b>	_	0.105183	0.1037	2:
V160	<b>-</b>	-0.00995209	0.024089	-0.4131	6
V165	٦,	-0.283990	0.190662	-1.4895	:
V168	٦.		0.035299	1.0251	3,5
V169	٦,	-0.10011/	0.00/039	-1.0950	5 %
7/1A	٠.	0.025368	0.101790	0.2492	0.8033
BAHS		0.167065	0.112589	1.4839	3
OTH	-	0.016830	0.205994	0.0817	8

Table C.7--continued

6.60	89	Ŧ	75	'n	~	0	T!	- 4	2	•	•	~	•	•	•	23	22	īī.		<u>.</u>	10	65	29	<b>5</b> 6	8	24	<b>~</b> 6	N 0	70	67	99	<b>‡</b>	81	
0.00	•	PROB>	9.6	90	'n	9	•	?-	•	: •	•	9	i.	•	יי יי	-	•	0.027		PROB>   T	0.00	0.0	0.37	0.0	2.0	0.3			0,32	0.79	0.6266	0.77	0.38	2
F RATIO	R-SQUARE	T RATIO	5.5122	-2.8165	0.6166	-4.4568	2.4560	-0.9199	961E 1	0.0484	0.9385	1.8657	-0.2741	0.4179	0.5767	F RATIO	PROBY	R-SQUARE		T RATIO	6.8087	2.7297	-0.8915	2.0313	-0.4679	— (	1367	<b>,</b> c	-0.9857		0.4867	-0.2871	-0.8636	#/ PI ::"
813.628944	1.053924	STANDARD	0.499152	0.059070	0.095139	0.063224	0.040192	0.111110	0.063316	0.037390	0.092851	0.023509	0.107820	0.119258	0.218196	638.88559	666	0.827572	STANDARD	ERROR											0.020832			
238 D10	NO.	Paradeter Estimate	2.751412	-0.563767	0.058667	-0.281775	0.098712	90	-0.033463 0.04446	0.001809002		0.043861	-0.029550	0.049838	0.125827	## ## ## ## ## ## ## ## ## ## ## ## ##		NS N	PARAMETER		3.011569	0.224843	-0.046673	0.171252	-0.026215	0.036003			0.032659		0.010139	-0.027426	٦	
-		ä		<b>-</b>	ı ~	-	⊶.	۰,	<b>→</b>	•	-	-	-	<b>~</b>	7	_				D	~	~	~	7	7	_	٦.	٠-	- ٠	• ~	• —	~	7	•
NODEL01	V144	•	t													TO TACOM		V145		••	<b>*</b>													
MODEL	DES VAR:	VARIABLE	INTERCEPT	24CT	V156W	V157C	V158	V159A	2412	5917	V169	V172	SES		<b>E</b>		1	DEP VAR		VARIABLE	INTERCEPT	SACTO	V152	V156W	V157C	V158	V159A	2912	6917	691A	V172	SH2	BMI.S	Ž

Table C.7--continued

MODEL: DEP VAR:	MODELO1		998 DFR	1015.604 772 1.315549	F RATIO PROB>F R-SQUARE	7.23 0.0001 0.1159
VARIABLE		8	Parameter Estinate	STANDARD	T RATIO	PROB> [T]
INTERCEPT SACTO V152 V156W V156W	<b>.</b>				3.0123 -2.8069 3.2141 0.6735 -0.2739	0.0027 0.0051 0.0014 0.00018 0.0001
V159 V159 V165 V169 V172 WHS BNHS		нааменааме	-0.052310 -0.010012 -0.050889 -0.025316 -0.025316 -0.025316 -0.230372 -0.230372	0.028508 0.028508 0.028508 0.021774 0.032788 0.130261 0.133241	-0.4202 -1.21222 -1.21222 -1.21222 -0.91406 -1.72157 -1.72157	0.000 0.1825 0.1825 0.1825 0.3601 0.0601 0.0601 0.0601
MODEL: DEP VAR:	MODEL01 V147	9	SSE DPE MSE PARAMETER PSTINTE	725.170378 772 0.939340 STANDARD	F RATIO PROBYF R-SQUARE F RATIO	5.31 0.0001 0.0879
NATERCEPT SACTO V155 V156 V156 V156 V156 V159 V169 V165 V169 V172 WHS	<b>B</b> a		3.166934 -0.2007111 -0.105981 -0.105451 -0.070469 -0.033854 -0.0388476 -0.088476 -0.088476	0.471238 0.0854784 0.0858784 0.0858688 0.037944 0.037944 0.037894 0.087659 0.087659		0.000000000000000000000000000000000000
OTH C		٠,		0.205993	-	0.4483

Table C.7--continued

NODEL: NO	HODEE01	388	764.472646	F RATIO	6.31
DEP VAR: V148	•	200	0.990250	R-SQUARE	0.0726
VARIABLE	ā	Parameter Estimate	STANDARD	T BATIO	PRO8>[7]
INTERCEPT SACTO V152	AAA	2.069783 -0.063203 0.008237791	. 69383 . 09010 . 05726	4.2778 -0.7015 0.1439 0.8240	0.0001 0.4832 0.8857 0.4102
V1594 V159 V159A	4 e4 e4 e	0.00582881	0.061285	4.4521 0.1496 -1.6012	0.0001 0.8811 0.1097 0.3594
V168 V168 V168	4 4 4 4 4	-0.17702 -0.177702 0.054463 -0.191138	03624	1.5027 2.1237	
VI 72 WHS BWHS OTH		0.201173 -0.183076 0.059172	11560	1.9249 -1.5837 0.2798	
MODEL: MODE DEP VAR: V149	MODELO1 V149	25W 24G 266	772.520222 772 1.000674	F RATIO PROB>F R-SQUARE	3.86 0.0001 0.0654
VARIABLE	Õ	Parameter Estimate	STANDARD	T RATIO	PROB>[T]
Intercept		200	.09057	5.9202 4.1342 -0.4197	
V152 V156W V157C	<b>→</b> , <b>→</b> ,-		09270		
V158 V160 V160	or prof prof		10856 .02486 .19678		
V168 V169 V172	1 e-1 e-1 e-1 e	0000	0.036434	-1.5624 1.3097 2.4949	0.1186 0.1907 0.0128 0.0012
whs BNHS Of H	<b></b>		11620		

Table C.7--continued

NODEL: NODEL01 DEP VAR: V150	<b>4</b>	888 DFR 888	1139.144 772 1.475576	F RATIO PROBYF R-SQUARE	4.90 0.0001 0.0815
VARIABLE	ä	Parameter Estimate	STANDARD ERROR	T RATIO	PROS> (T)
INTERCEPT SACTO V152 V156W	<b>ненен</b>	. 2000 . 2000 . 20016 . 20019		2002	00170
V1598 V165 V165 V165 V170 V170 V170 V170 V170 V170 V170 V170		0.031950 0.307479 0.217589 0.050517 0.020299	0.047557 0.0301930 0.238964 0.246262 0.109866	0.9124 0.9124 1.1419 0.1640 1.0400	00000000000000000000000000000000000000
MALS BOMES OTH		51971 04899 01877		073 072	220
MODEL: MODELO1 DEP VAR: PM26	=	338 130 130	373.432845 772 0.483721	F RATIO PROB>F R-SQUARE	5.85 0.0001 0.0960
VARIABLE	ă	Parameter Estimate	STANDARD	T RATIO	PROB>   T
INTERCEPT SACTO V152 V156W	нене	3.426544 -0.407159 0.037501 -0.059960	. 33816 .06297 .04002	.132 .465 .937	99.44
V157C V158 V159A V160		0.052570 -0.035039 -0.044875 C.007706295	.04283 .02722 .07548 .01728	1.227 1.286 0.594 0.445	25.50
V165 V168 V172 WHS BANKS		0.052494 -0.1084494 -0.108437 -0.098167 0.104565	0.025331 0.062904 0.015927 0.080794 0.147822	-1.7233 -1.7233 -1.3439 1.2942 0.5325	00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00

Table C.7 -- continued

PARAMETER STANDARD  1 2.105245 0.391210 1 0.049906 0.046303 1 0.049906 0.046303 1 0.051395 0.049553 1 0.051395 0.049553 1 0.021474 0.031500 1 0.021474 0.031500 1 0.021474 0.031500 1 0.023224 0.045033 1 0.053227 0.017472 PARAMETER STANDARD DE ESTINATE ERROR 1 0.052292 0.0646145 1 0.068403 0.041066 1 0.053291 0.041066 1 0.053291 0.041066 1 0.053291 0.041066 1 0.068403 0.041066 1 0.059391 0.041066 1 0.068403 0.0410948 1 0.013931 0.0140382 1 0.014948 0.064542	772 PROB>F 0.647364 R-8QUARE	0.0001 0.1041
0.049906 0.049906 0.049906 0.049906 0.0518535 0.0518535 0.0518535 0.0518535 0.018222 0.018222 0.018668 0.018668 0.018668 0.018668 0.018668 0.018668 0.018668 0.018668 0.018668 0.018668 0.018668 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.0186888 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688 0.018688	STANDARD T RATIO	PROB>   T
DE ESTINATE PARAMETER SET 1 0.061985	191210 5.3814 172853 -4.8721 146303 1.0778	0.0001
0.0016222 1.00.016222 1.00.031666 1.00.031666 1.00.031666 1.00.031666 1.00.031666 1.00.031666 1.00.03222 0.053227 0.053227 0.053227 0.053227 0.053227 0.053227 0.053227 0.053227 0.053227 0.053227 0.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.00.066403 1.		
0.017648 1 0.0176	•	
DE ESTIMATE  1 0.0284226  1 0.053227  DE ESTIMATE  1 2.980940  1 2.980940  1 0.08403  1 0.08403  1 0.091354  1 0.090928  1 0.090928  1 0.090928	•	
DE BSE 395  DE MSE  PARAMETER  1 2.980940 1 -0.282292 1 0.068403 1 -0.076754 1 0.013931 1 -0.130175 1 0.030928 1 0.030486	,	
PARAMETER S ESTIMATER S 1 2.980940 1 -0.282292 1 0.068403 1 0.076754 1 0.042600 1 -0.042600 1 0.013931 1 0.090928 1 0.030486		7.39
PARAMETER ESTIMATER -0.2880940 -0.068403 -0.191306 -0.130175 -0.130175 -0.19933 -0.19933 -0.19938	1. 509234 R-SQUARE	•
2.9809940 -0.082292 -0.0768292 -0.0768292 -0.191305 -0.130175 -0.3014931 -0.1499488 -0.1499488	STANDARD T RATIO	PROB> [T]
-0.0684894 -0.0684894 -0.0684894 -0.130145 -0.013931 -0.090988 -0.149988		0.
-0.076754 -0.191306 -0.130106 -0.130106 -0.130105 -0.090928 -0.149948		, 0
-0.0142400 -0.0142400 -0.014010 -0.014010 -0.014010 -0.0140000000000000000000000000000000000		
-0.130175 -0.0130175 -0.0301454 -0.030468 -0.030468		
-0.301454 -0.090928 -0.040928		,,
-0.149948 -0.30486		
-0.030486		
-0.042695	082898 -0.5150	0.6067

Table C.7--continued

MODEL:	HODET01		200	332.151703	F RATIO	6.11
DEP VAR:	PM30			0.430248	R-SQUARE	0.1282
VARIABLE	åg åg	-	araneter estimate	STANDARD	T RATIO	PROB>   T
INTERCEPT		m o	401213	0.318925	10.6646	0.0001
V152		00	029315	0.037747	0.7766 -0.5837	0.4376 0.5596
V157C		00	162662	0.040396	4.0267	0.0001
V159A		90	114809	0.071186	-1.6126	0.1072
V165		90	281266 041939	0.129036	-2.1797	0.0296 0.0796
V169		99	111364	0.059326	-1.6772	0.0609
MAKS		00	0.115260	0.068889	1.6731	0.0947
<b>3</b>		•	027824	0.139412	0.1996	0.8419

Table C.7--continued

HODEL: HODELO1		200	992.978851	F RATIO	5.71	
DEP VAR: PAYDETRA	*	4 <b>18 18 18 18 18 18 18 18</b>	1.299711	R-SQUARE	0.0885	
VARIABLE	10	Parameter Estimate	STANDARD ERROR	T RATIO	PROB> [T]	
INTERCEPT SACTO		3.446070	0.523036	6.5886 -0.8452	0.0001	
V152	<b></b> -	0.011001	0.065569	0.1690	0.8658 0.2244	
VISTC	• •	0.183342	0.069581	2.6349	0.0086	
V158 V159A	r4 r4	-0.112052 -0.182940	0.124449	-1.4700	0.1420	
V160	-	0.056235	0.028457	1.9761	0.0485	
V168	4-1	0.116194	0.042101	2.7599	0.0059	
V172	-	-0.062468	0.025459	-2.4537	0.0144	
SH3	-	0.658011	0.119900	2.4880	0.0001	
BNHS	-	0.163812	0.133196	1.2299	0.2191	
OTH.	<b>-</b>	-0.282440	0.240337	-1.1752	0.2403	

Table C.8

REGRESSION RESULTS FOR PRETEST VERSUS BASELINE SURVEY ALMINISTRATIONS AT SM-ALC

MODEL: M	HODET01		186	903.804215	F BATIO	5.01
DEP VAR: PI	PM02			0.61399	R-SQUARE	0
VARIABLE		2	Paracter Estimate	STANDARD	T RATIO	PROB> [T]
INTERCEPT			3.176615	0.205277	15.4747	0.0001
SUPER V152			0.140587	00	2.1170 -0.3845	. 28
V156W			0.282438		5.5822	000
V15/C V158		٦,	-0.022064	,,	-0.9070	364
V159A		<b>~</b> -	-0.081835		1. <b>4</b> 03 0.106	. 160 . 915
V165		·	90	, 0	1.1670	.243
V168		٦.	5		0.063	6 C
V169		<b></b>	o c	<i>.</i>	-2.2746	023
7/1A		<b>-</b>	-0.082449	, 0	1.106	.268
BNHS		-	ö	0	1.205	. 228
OTH.		-	-0.106314		-1.3656	. 172
 						-
MODEL: M	HODETO!		330	→	PROB>F	0.0001
DEP VAR: PI	PM03B		MSE	0.771	R-SQUARE	-
			PARAMETER	STANDARD		
VARIABLE		D.	ESTIMATE	ERROR	T RATIO	PROB>   T
INTERCEPT		~	4.536556	Ö	19.7104	000
ADMIN		<b>⊣</b> .	-0.532941	o c	nu	
SUPER		٦.	0.414647		-1.5084	131
W95[V		. ~	0.170586	0	3.0070	.002
V157C		<b>~</b>	0.019040	o o	0,	.670
V158		<b>-</b>	o c	Š	-4.56//	95
V159A V160		<b></b>	-0.00533657	0		741
V165		-	o	Ö	1.5420	. 123
V168		<b></b>	ŏ	o c	J ~	. 838 222
V169		<b>-</b>	-0.062236	9	4 (7)	9
WHS			ö	Ö	-0.8707	.384
BNHS		٦.	-0.178796	0.063303	-2.8245	0.0048
E S		4	******	•	,	

Table C.8--continued

MODEL: MODELO! DEP VAR: PHO4		83E DFT ROM	1247.947 1472 0.847790	F RATIO PROB>F R-SQUARE	18.10 0.0001 0.1557
VARIABLE	ð	Parameter Estimate	STANDARD ERBOR	T RATIO	PROBY [T]
Intercept Admin Super		2.553589 -0.018109 0.001927004	0.241214 0.098969 0.078033	10.5864 -0.1830 0.0247	0.0001
752 7152 7158		0.064381	0.032394	1.9875	0.0471 0.0001 0.0001
V158 V159A		-0.050998 -0.072586 -0.053771	0.028585	-1.7641 -1.0597 -3.1769	0.0746
7165 7165		0.144547	0.062559 0.022259 0.059769	2.3106 4.4156 0.1841	0.0210 0.0001 0.8540
V172 WHS BNHS OTH		-0.04169 -0.180597 0.037196 -0.136428	0.017100 0.087564 0.066343 0.091478	-2.5841 -2.0625 0.5607 -1.4914	0.0099 0.0393 0.5751

Table C.8--continued

HODEL: MC	HODEF01		<b>M S S S S</b>	1139.611	P RATIO	
DEP VAR: PH	PM06		NSE NOTE	0.774192	R-SQUARE	0.0729
VARIABLE		0£	Parameter Estimate	STANDARD	T RATIO	PROB>   T
		-	94153	23050	080	0.0001
LAIRNOST		- ۲	-0.320639	0.094576	-3.3903	0.0007
CIPER		•	40706	07456	458	.000
V152		-	.02992	.03095	996.	. 333
V156W		-	11156	.05681	.963	۰.
V.57C		<b>-</b>	.07939	.04479	.772	.076
7150		-	.04245	.02731	1.554	. 120
V159A		-	.19179	.06545	2.930	. 003
V160		_	.02506	.01617	. 549	-121
7165		-	.11603	.05978	.941	.052
7168		-	.01920	.02129	. 901	. 367
691/		-	.20737	.05711	. 630	900
1172		-	.05432	.01634	. 324	900.
TH3		-	0.01411	.08367	.168	. 866
SHAB		-	0355067	.06339	.056	. 955
HI		<b>,</b>	-0.01719	.08741	. 196	. 811
					+ + + + + + + + + + + + + + + + + + +	
HODEL: NO	HODEL01		388	1201.373	F RATIO	6.14
			DFE	147	PROB>F	0.0001
DEP VAR: PP	PM07		MSE	2	R-SQUARE	•
			PARAMETER	STANDARD		
VARIABLE		DF	ESTIMATE	ERROR	T RATIO	PROB>  T
TUTERCEPT		-	.37427	``	.257	000
LUMIN		-	12471	٦.	1.284	. 199
SUPER		-	.28087	٦.	.668	80.
7152		-	.01246	٦	. 392	. 695
M9511		-	.08416	٦.	. 442	. 149
V157C			07076	٦.	.53	0.1241
/158		_	.05553	٠.	086.	. 047
V159A		<b>~</b>	17257	٦,	2.567	25
V160		<b>~</b>	.02544	٠,	150.	120
7165		٦.	.05749	٠,	920	7
1168		٦.	0.0/95/	:`	,,,,	
200		٦.	66//1.00	: `	2.027	35
7/1/		- ب	0.0400	•	0.725	468
		- ۲	0026683		0.041	. 967
HLC				0.089755	1.179	238
::		,				

Table C.8--continued

F RATIO 16.33 PROB>F 0.0001 R-SQUARE 0.1426	T RATIO PROB> T	4.1700 -3.5950 -1.8860 -2.91325 -2.9453 0.6901 0.6901 0.6901 0.6903 -1.2607 -1.2607 0.2925 1.0531 0.2925 1.7543 0.0001
1636.665 1472 1.111865	STANDARD	0.276238 0.11340 0.089363 0.089086 0.089086 0.032735 0.078444 0.019383 0.088448 0.019583
838 DFE MSR	Parameter Estimate	2. 456790 -0. 321257 -0. 321257 -0. 321257 -0. 321257 -0. 32126 -0. 32126 -0
HODEL: HODELOI DEP VAR: PHOS	/ARIABLE	INTERCEPT ADMIN SUPER V152 V153 V1564 V1554 V1556 V156 V166 V166 V166 W169 W172

Table C.8--continued

19.04 0.0001 0.1625	PROB>   T	00000000000000000000000000000000000000	1001 1001 1001 1001 1001 1001 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1
90			, coccoccoccocco
F RATIO PROB>F R-SQUARE	T RATIO	12. 4779 -3.5984 -1.1782 -1.1782 -1.1782 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.0744 -1.07	F RATIO PROB>F R-SQUARE R-SQUARE 14.7024 -1.4531 -3.4989 -0.0889 -1.8539 -1.8539 -1.8539 -1.8539 -1.8539 -1.8539 -1.8539 -1.6549 -1.0549
1383.029 1472 0.939558	STANDARD ERROR	0.151933 0.1041833 0.0041843 0.0042588 0.0042588 0.0042588 0.00428180 0.005858 0.005858 0.005858 0.0058181	1486.461 1.009824 37ANDARD ERROR 0.108014 0.0155164 0.0155164 0.0155164 0.0155164 0.018472 0.068276 0.068276 0.068276 0.068276 0.068276 0.068276
SSW DFR MSR	PARAMETER ESTINATE	3.168551 -0.374908 0.4255108 0.1088137 -0.1198151 -0.00957465 -0.081568 -0.081568 -0.081568 -0.081568	8SE DEE MSE NSE ESTINATE 3.870514 -0.030514 -0.0305154 -0.0305154 -0.0305154 -0.0305154 -0.12029365 -0.0309365 -0.120283 -0.120283 -0.120283 -0.120283 -0.120283
	DF		& nanneadadada Q
MODELO1 PM11			MODELO1
MODEL: DEP VAR:	VARIABLE	INTERCEPT ADMIN ADMIN SUPER VISS VISS VISS VISS VISS VISS VISS VIS	MODEL: DEP VAR: VARIABLE INTERCEPT ADMIN VISS VISS VISS VISS VISS VISS VISS VI

Table C.8--continued

MODEL: M	MODEL 01		SSE	1472		0.0001
DEP VAR: PI	PM14			0.609362	R-SQUARE	•
VARIABLE	_	à	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>[T]
INTERCEPT			3.289217	0.204501	16.0841	0.0001
SUPER		ıı <i>-</i>	41418	.06615	260	900
V152 V156W		<b>-</b>	07970	05040	581	
V157C			01002	.03973 .02423	. 252	. 091
A159A		, ,	0.09342	.05807	608	100
V165			0.09155	.05303	726	100.
V168 V169			.01703 .13991	.01689 .05067	761	.005
V172		-	0.05073	.01449	199	.000
BNHS			.08136	.05624	116	148
OTH THE	1	-	.06506	.07755	. 839	. 401
M 1300M	MODEL01		100	617.761067	F RATIO	
DEP VAR: PI	PM15			0.419675	R-SQUARE	0.0745
VARIABLE		OF	Parameter Estimate	STANDARD	T RATIO	PROB> [T]
INTERCEPT				0.169713	17.4464	86
SUPER					. 189	.001
7127 V156W		<b>-</b> -			.97	9
V157C			0.05250		. 592	. 111 . 708
V159A		· ~- ~	-0.187	0.048194	-3.8810	88
V165					191	. 237
V168					. 154	.031
V172		. <del></del> .	0.05035		.185	.000
WHS BNHS					. 286	198
OTH		-			. 298	. 765

Table C.8--continued

MODEL: DEP VAR:	MODELO1		SSE	1187.213 1472 0.806531	F RATIO PROB>F R-SQUARE	7.43 0.0001 0.0704
VARIABLE		DF	Parameter Estimate	STANDARD	T RATIO	PROB>  T
INTERCEPT ADMIN SUPER V152	<b>6</b> 4		2.803163 -0.443940 0.313586 0.033878 -0.032109		********	000N
V157C V158 V160 V166 V168 V168		мамамам	0.067096 -0.108927 -0.125909 -0.00791528 0.057883	0.045718 0.027880 0.056811 0.05508 0.021736 0.058297	1.4676 -3.9070 -1.8846 -0.4795 1.1995 1.8749	0.1424 0.0001 0.05597 0.05317 0.06110
V172 WHS BNHS OTH			-0.044978 -0.042149 -0.022301 -0.079279		-2.6967 -0.4935 -0.3446 -0.8885	
MODEL: DEP VAR:	MODEL01 PM18D		SSE DFE MSE	675.458886 1472 0.458872	F RATIO PROB>F R-SQUARE	10.93 0.0001 0.1003
VARIABLE		DF	Parameter Estimate	STANDARD ERROR	T RATIO	PROB> T
INTERCEPT ADMIN SUPER VIS2	<b>L</b>			.07261 .07261 .05740	.527 .706 .853	0000
V157C V158 V159A V160				03448		,000,0
V165 V168 V172 WHS BNHS			0.082894 -0.129905 -0.052977 -0.0675112 0.043290	0.046045 0.016395 0.012581 0.064421 0.064808	1.4230 1.9540 -2.9540 -4.2110 -0.6638 -0.1793	0.0549 0.0509 0.00012 0.85069 0.8577

Table C.8--continued

MODEL: MODEL01		<b>10</b>	1561.801	F RATIO	24.08
DEP VAR: PH19		MSM	1.061006	R-SQUARE	0.1970
VARIABLE	å	Parameter Estimate	STANDARD	T RATIO	PROB>   T
INTERCEPT		2.279275	0.269847	8.4466	0.0001
SUPER	ı ,	29530	0872	382	•
V156W V156W		55288	.0665	.816	• •
V157C		13666 10863	0524	. 327	
V159A	•	.00750289	.0766	0.097	•
V160		.0090637	6690	578	
V168	-	77577	0249	.039	•
V169	<b>~</b> ,	<b>19363</b>	.0668	1.400 6.130	•
2/ 1/2 SH20	٦.	3008	9760	3.369	• •
BNHS	· ~	16842	.0742	964	•
OTH	-	10429	. 1023	1.019	•
MODEL: MODEL01		100 S	9:	F RATIO	_
DEP VAR: PH21B		MSE	0.659267	R-SQUARE	0.1285
VARIABLE	ğ	ESTIMATE	ERROR	T RATIO	PROB>   T
INTERCEPT	7	.0816	.2127	.487	.000
ADMIN		. 2694	.0872	3.087	.002
SUPER	<b>.</b>	.5584	.0688	8.115	.000
2517	<b>-</b>	1620.	7070	133	20
V157C		1155	.0413	. 795	.005
V158	-	.0316	.0252	1.253	. 210
V159A	<b>~</b>	0.1950	.0604	3.229	.00.
V160	<b></b> -	.0279	.0149 0551	9.5	96
070	<b>-</b>	7001	9610	703	088
V169	• ~	1041	0527	1.975	.048
V1.72	۳,	0.0423	.0150	.81	.005
PARIS	<b>-</b>	-0.070144	0.058503	-0.6363	0.5247
H	-	.1255	.0806	1.556	.119

Table C.8--continued

MODEL: MODELO1 DEP VAR: PH23		SSE	1540.761 1472 1.046713	F RATIO PROB>F R-SQUARE	11.48
VARIABLE	å	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>  T
INTERCEPT ADMIN SUPER VIS2	пппп	.13355 .09221 .55989		11.6914 -0.8386 6.4575 0.0909	8382
V156W V156W V159A		0.30334 0.05684 -0.14141		1.5918 -4.4523 -3.0472	8288
V165 V169 V172 WHS BNHS OTH		-0.012887 -0.000845887 -0.1677681 -0.072928 -0.061334 -0.016200	0.069512 0.0247512 0.019001 0.019001 0.073716 0.073716	-2.5262 -3.5262 -3.5262 -1.57662 -1.57662	0.000.000.000.000.000.000.000.000.000.
MODEL: MODELO1 DEP VAR: PH31B VARIABLE	ğ	SSE DFE MSE PARAMETER RSTIMATE	1286.399 1472 0.873912 STANDARD ERROR	F RATIO PROBSE R-SQUARE T RATIO	10.08 0.0001 0.0931
INTERCEPT SUPER SUPER SUPER V158 V158 V159 V159 V169 V172 WHS		0.009844 0.03384 0.03380 0.03380 0.0481034 0.06869 0.081680 0.081680 0.08869 0.08864 0.08864 0.08864	0.244902 0.1044902 0.100482 0.0503899 0.0603899 0.060545 0.063516 0.060833 0.060833 0.060833		0.000000000000000000000000000000000000
OTH	-	.03749	.09287	0.4037	0.6865

Table C.8--continued

Table C.8--continued

HODEL	HODET01		188	98.448706	P RATIO		
DEP VAR:	PM26		HSH	0.520893	R-SQUARE	0.1184	
VARIABLE		D.	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>[T]	
INTERCEPT ADMIN	<b>6</b> 4		1.867282	0.511004	3.6541	0.0003	
V152			5458	995	8.5	0.4246	
V157C			8605	560	18	0.00	
V158		<b></b>	<b>10148</b>	96	39	0.1652	
V160		٠.	2905	035	8	9907.0	
V165		<b>-</b> -	14261	131	7 O	0.7471	
V169			7986	126	2	0.1570	
V172		<b></b>	1892	.036	22	0.6024	
BNHS		•-	996	145	38	0.0051	
H		, ,-4	3401	194	20	0.2293	
MODEL	HODET01		100 00 00 00 00 00 00 00 00 00 00 00 00	104.203811	F RATIO		
DEP VAR:	PM27		4 10	0.551343	R-SQUARE	0.2501	
VARIABLE		D.F.	Parameter Estimate	STANDARD ERROR	T RATIO	PROB>[T]	
INTERCEPT	•	-		•	3.4947	0.0006	
ADMIN		-		•	-0.5327	0.5948	
V152		<b>,</b> 0		•	-1.6281	0.1052	
V156W		<b></b>		•	1.6337	0.1040	
V158		- ،			3.3803	0.000	
V159A		-		•	-2.7990	0.0057	
V160		, i		•	-0.9610	0.3378	
V165		<b>-</b>	0.029349	0.135//6	0.2152 -0.8265	1828.0	
69IA		٠,	Ö		-0.8239	0.4110	
V172		-	o.	•	-1.5273	0.1284	
		<b></b> ,	o c	•	-0.9873	0.3248	
STH C		<b>-</b>			1.3747	0.3020	
:		ŀ		,		1 1 1	

Table C.8--continued

MODEL: DEP VAR:	MODELO1 PM26D		288 250 150 150 150 150 150 150 150 150 150 1	91.933175 169 0.46619	F RATIO PROBY R-SQUARE	2.55 0.0023 0.1587
VARIABLE		ğ	Parameter Estimate	STANDARD	T RATIO	PROB>   T
INTERCEPT ADMIN V152 V1564	•		23205 23205 11901 03293	7.0.0	114 170 805 271 446	0.0001 0.2433 0.0726 0.0622
V15.7 V158 V165 V165			-0.547018 -0.547018 -0.022554 -0.040413	0.058445 0.034687 0.127531 0.045655	0.6502 0.6502 0.6502 0.8569	0.5272 0.0001 0.5163 0.517
V169 V172 WHS BURS OTH			02060 06675 01462 15865		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
MODEL: DEP VAR:	MODEL01 PM30		SSE DFR MSR	84.057742 189 0.444750	F RATIO PROB>F R-SQUARE	1.37 0.1731 0.0919
VARIABLE		<u>s</u>	Paraketer Estimate	STANDARD ERROR	T RATIO	PROB>   T
INTERCEPT ADMIN V152	<b>B</b> a				631 809 444	
V157C V159A V160			0.28255 0485777 0.34383 0076432		192 086 561 230	• • • •
V168 V168 V172 WHS WHS OTH			-0.096129 0.015166 0.026922 -0.069749 0.176072 0.089515	0.121946 0.121655 0.033521 0.131648 0.131041 0.179277	-0.7883 0.3474 0.3474 -0.8042 0.4005 1.3540 0.4993	0.4315 0.7287 0.4223 0.6892 0.1774 0.6181

Table C.9

RESULTS OF FACTOR ANALYSES

Alpha	Factor Name Questions					
	Questions Answered by All Resp	ondents				
.939	Satisfaction with Supervisor/ Work Unit	V4, V5, V11, V14, V15, V19, V21, V23, V28, V31, V34, V39, V50, V55, V75, V89, V94, V96, V100				
. 880	Organizational Climate	V7, V13, V20, V24, V40, V52, V66, V84, V98, V101, V102				
. 837	Organizational Involvement	V10, V16, V42, V44, V53, V62, V72, V73, V80, V95, V97, V120, V121, V123				
.813	Pay-Performance Link	V2, V27, V29, V79, V82, V114, V115, V116				
. 846	Importance of Intrinsic/ Extrinsic Rewards	V120, V121, V122, V123, V124, V125, V126, V127				
.801	Pay Satisfaction	V8, V22, V30, V70, V81, V87				
. 862	Satisfaction with Union	V45, V107, V108, V109, V110				
. 780	Intrinsic Job Satisfaction	V54, V58, V90				
	Supervisor Questions					
. 862	Support from Management/ Sufficient Authority	V128, V132, V133, V134, V136, V140, V141, V142, V146, V147, V148				
.710	Supportiveness of Personnel Office	V134, V137, V143, V149				
.532	Willingness to Recommend Staff Reductions	V130, V144				

## Table C.10

## RESPONSE DISTRIBUTIONS FOR INDIVIDUAL QUESTIONS

## (In percent)

("OTHNON" = Comparison sites, nonsupervisors,
"OTHSUP" = Comparison sites, supervisors,
"SMNON" = Sacramento, nonsupervisors,
"SMSUP" = Sacramento, supervisors)

GENERAL ITEMS

OBNER	112.10						
VI	MISSING = 7	ı 1ı	2	3	Ι Δ	51	TOTAL
						) +	
	OTHNON				•		
	OTHSUP	1.91	7.96	3.18	62.74	24.20	628
	SMNON	4.41	12.43	5.37	55.49	22.29	1247
	SMSUP	3.01	9.64	2.41	56.63	28.31	166
		++			+	+ <b></b> +	
V2	MISSING = 10						
						5   5	
	OTHNON	27.63	40.86	7.30	19.74	4.47	1520
	OTHSUP	18.98	39.39	3.35	33.17		627
	SMNON	36.47	37.99	7.07	14.62	3.86	1245
	SMSUP	27.71	39.76	7.23	22.29		166
		++			<b></b>	++	
V3	MISSING = 11						
						5	
	OTHNON	2.90	23.27	34.87	29.33	9.62	1517
	OTHSUP	5.73	39.49	17.52	29.78		628
	SMNON	5.70	23.60	41.57	21.27	7.87	1246
	SMSUP	6.02	34.94	21.08	28.92		166
		++	·		<b>+</b>	++	
V4	MISSING = 7	, 1,	2.1	2			mom. 1
					4	5   ++	
	OTHNON	10.93	21.20	6.78	47.93	13.17	1519
	OTHSUP		7.64	3.18	60.51	24.36	
	SMNON	12.74	23.96	9.62	42.71	10.98	
	~~~~~~						

SMSUP | 4.82 | 19.88 | 6.63 | 45.78 | 22.89 |

166

Table C.10--cont-inued

V5	MISSING = 9						
		1	2	3	4	5	TOTAL
	OTHNON	21.86	43.78	7.90	22.51	3.95	1519
	OTHSUP	5.74	45.14	6.38		3.83	627
	SMNON	30.71	44.43	7.30		•	1247
	SMSUP	15.66	51.81	4.22		4.22	166
V6	MISSING = 10	1	2	3	,	5	TOTAL
	OTHNON	7.65	24.67	13.59	36.54	17.55	1516
	OTHSUP	4.78	28.03	7.01	41.72	18.47	628
	SMNON	7.69	20.83	13.62	35.34	22.52	1248
	SMSUP	8.43	19.88	9.04	45.78	16.87	166
V 7	MISSING = 26	+-					
V /	.11331.10 - 20	1	2	3	4	5	TOTAL
	OTHNON	1.72	24.37	23.71	35.63	14.57	1510
	OTHSUP	10.86	51.28	12.94	18.85	6.07	626
	SMNON	1.05	11.76	25.38	37.23	24.58	1241
	SMSUP	6.67	36.36	21.82	24.24	10.91	165
V8	MISSING = 25	1	2	3	4	5	TOTAL
	OTHNON	21.99		•	+ 33.49	 4.56	1514
	OTHSUP	13.62		3.04	+ 46.79	6.41	624
	SMNON	29.49	35.70	5.72	+ 26.19	2.90	1241
	SMSUP	14.63 		· ·	•	,	164
						,	

Table C.10--continued

V9	MISSING = 25						
		•	2			5	
	OTHNON		33.05	20.82	27.36	•	1513
	OTHSUP	9.76	41.12	12.00	31.36	•	625
	SMNON	18.55	34.11	25.48	16.45		1240
	SMSUP	15.76	41.82	16.36	18.79	•	165
V10	MISSING = 22			·		·	
		•	2		4	5	TOTAL
	OTHNON	•	•	'		23.66	1513
	OTHSUP	0.80	1.76	3.85	49.52	44.07	624
	SMNON	4.26	8.12	16.24	50.40	20.98	1244
	SMSUP	•			•	40.00	
V11	MISSING = 22				•		
		1	2	3	4	5	TOTAL
	OTHNON	9.31	22.59	14.93	44.32	8.85	1514
	OTHSUP	1.60	12.64	6.72	61.28	17.76	625
	SMNON	9.98	23.91	18.92	40.50	6.68	1242
	SMSUP	6.67	18.79	12.73	50.91	10.91	165
V12	MISSING = 25	'	•	_		,,	
		1	2	•	4 +	5 	
	OTHNON	11.70	•	•	•		
	OTHSUP	4.64	24.96	17.12	44.32	8.96	625
	SMNON	17.42	32.02	18.87	24.44	7.26	1240
	SMSUP	•	•	•	,	7.27	
		•	•	•	•	. ,	

Table C.10--continued

V13	MISSING = 23						
		1	2	3	4	5	TOTAL
	OTHNON	3.77	18.58	11.84	38.62	27.18	1512
	OTHSUP	6.56	33.60	11.36	36.32	12.16	625
	SMNON	2.41	9.25	13.76	37.17	37.41	1243
	SMSUP	1.21	16.36	13.33		26.67	
V14	MISSING = 27	++			'	·	
		1	2	3	4	5 +	TOTAL
	OTHNON	9.86	21.97	5.56	50.96	11.65	1511
	OTHSUP	2.56	16.32	6.40	56.80	17.92	625
	SMNON	17.18	27.02	7.50	39.27	9.03	1240
	SMSUP	9.09	24.85	13.33	43.03	9.70	165
V15	MISSING = 27	, ,		,	'	•	
. 20		1	2	3	4	5	TOTAL
	OTHNON	16.29	35.50	12.12	30.07	6.03	1510
	OTHSUP	5.77	28.85	8.49	47.60	9.29	624
	SMNON	25.68	35.75	12.24	22.14	4.19	1242
	SMSUP	13.33	27.27	11.52	41.21	6.67	165
V16	MISSING = 26	,			,	, ,	
		1	2] 3	4	5	TOTAL
	OTHNON	4.63	20.52	15.42	46.46	12.97	1511
	OTHSUP	1.28	14.74	8.97	55.61	19.39	624
	SMNON	† 7.65	22.46	17.39	41.79	10.71	1242
	SMSUP	1.82	•	9.09	45.45	29.70	165
		T	T	T	T	T	-

Table C.10--continued

V17	MISSING = 23						
						5	TOTAL
	OTHNON	6.55	20.70	4.76	53.04		1512
	OTHSUP	2.24	17.76	2.72	58.40	•	625
	SMNON	9.01	21.00	5.95	52.05		
	SMSUP	5.45	22.42	2.42	51.52	18.18	165
V18	MISSING = 24	1	2	3		5	
	OTHNON	+	+-	+		+	
		+			+		
	OTHSUP				•	6.08 +	
						3.78	
	SMSUP	11.52	40.00	10.91	32.73	4.85	165
V19	MISSING = 25			•	'	'	
		1	2	3	4	5 -	TOTAL
	OTHNON	14.62	22.75	11.31	39.09	12.24	1512
	OTHSUP	4.33	18.27	6.73	54.81	15.87	624
	SMNON	19.32	21.58	15.78	33.74	9.58	1242
	SMSUP	8.48	18.18	15.15	46.06	12.12	165
V20	MISSING = 23	,			,		
120		1	2] 3	4	5	TOTAL
	OTHNON	36.00	32.69	7.61	20.71	2.98	1511
	OTHSUP	16.48	31.52	6.72	37.92	7.36	625
	SMNON	47.19	31.11	8.68	10.85	2.17	1244
	SMSUP	26.67	29.70	9.09	26.67	7.88	165
		T		T	T		•

Table C.10--continued

V21	MISSING = 25						
		1 +					TOTAL
	OTHNON	16.07	28.17	8.73	39.48	7.54	1512
	OTHSUP	5.44	24.96	8.80	51.68	9.12	625
	SMNON	24.58	31.83	10.48	27.40	5.72	1241
	SMSUP	13.33	30.91	10.30	38.18	7.27	165
V22	MISSING = 34		·	·	·	·	mom 4 v
		1 ++	•		-		TOTAL
		5.78	•	-	•	•	1506
	OTHSUP	4.96	24.96	22.24	32.64	15.20	625
	SMNON	3.63	14.78	27.38	29.64	24.56	1238
	SMSUP	4.85	18.18	22.42	36.97	17.58	165
1/23	MISSING = 36	,	,	·	·	·	
V23		1					TOTAL
		12.82	26.51	23.72		7.77	1505
		5.59	20.13	14.38	46.17	13.74	626
	SMNON	16.18	26.38	25.81	24.27	7.36	1236
	SMSUP	7.27	20.61	19.39	40.61	12.12	165
V24	MISSING = 35	+ -		,	,		
V 24	11331NG - 33	1	2	3	4	5	TOTAL
	OTHNON	34.02	35.95	8.17	16.15	5.71	1505
	OTHSUP	12.80	30.88	6.56	39.84	9.92	625
	SMNON	41.03	33.68	8.32	12.92	4.04	1238
	SMSUP	23.64	23.64	11.52	33.33	7.88	165
		, - -	- · 		, - 1	-: T	

Table C.10--continued

V25	MISSING = 37						
		1	2	3	4	5	TOTAL
	OTHNON	5.38	13.36	8.11	56.74	16.41	1505
	OTHSUP	1.76	8.47	7.51	64.06	18.21	626
	SMNON	8.91	14.82	11.26	51.09	13.93	1235
	SMSUP	3.64				26.06	165
V26	MISSING = 34	7					
120		1	2	3	4	5	TOTAL
	OTHNON	5.98	15.42	15.88	36.08	26.64	1505
	OTHSUP	8.16	24.64	16.96	35.3 6	14.88	625
	SMNON	7.10	15.01	18.16	30.35	29.38	1239
	SMSUP					24.85	
V27	MISSING = 33	'				, ,	
127		1	2	3	4	5	TOTAL
	OTHNON	25.65	36.74	12.09	19.27	6.25	1505
	OTHSUP	9.44	34.08	14.08	33.12	9.28	625
	SMNON	34.60	36.94	11.45	13.06	3.95	1240
	SMSUP	21.21	27.27	16.36	27.27	7.88	165
V28	MISSING = 33					,	
V20	111551110 - 55	1	2	3	•	5	
	OTHNON	5.64	18.66	•	•	12.88	
	OTHSUP	0.80	9.27	9.90	62.30	17.73	626
	SMNON	9.77	24.15	15.11	41.84	9.13	1238
	SMSUP	•	,	14.55	,	17.58	165
		, 	, 	,	T	T	-

Table C.10--continued

V29	MISSING = 34						
		1	2	3	4	5	TOTAL
	OTHNON	29.59	48.60	7.85	12.30	1.66	1504
	OTHSUP	20.29	49.20	6.23	20.77	3.51	626
	SMNON	42.45	43.34	6.62	6.78	0.81	1239
	SMSUP	27.88	53.94	7.88	8.48	1.82	165
1/20	MICCING - 20	++			+ -	+	
V30	MISSING = 38	1	2	3	4	5	TOTAL
	OTHNON	11.23	37.28	24.58	21.33	5.58	1505
	OTHSUP	11.70	40.38	21.31	23.56	3.04	624
	SMNON	7.69	24.43	29.37	27.83	10.68	1236
	SMSUP	12.73	26.67	20.61	30.91	9.09	165
W2.1	MICCING - 22	++			+	r+	
V31	MISSING = 32	1	2	3	4	5	TOTAL
	OTHNON	11.28	19.18	12.28	43.40	13.87	1507
	OTHSUP	5.76	15.68	7.84	54.72	16.00	625
	SMNON	16.06	21.63	14.04	37.93	10.33	1239
	SMSUP	7.88	14.55	13.33	52.73	11.52	165
uaa.	MICCING - 05	++			+	++	•
V32	MISSING = 35	1 			4	5	TOTAL
	OTHNON		32.89	20.20	•	•	1505
	OTHSUP		28.43	13.10	-	3.35	626
	SMNON	31.50	32.39		-	1.53	1238
	SMSUP	25.61	31.71		•		
		++			+	-	•

Table C.10--continued

V33	MISSING = 32						
		1	2	3	4	5	TOTAL
	OTHNON		23.77		44.69	•	1506
	OTHSUP		13.42	8.63	58.95	•	626
	SMNON	23.41	27.76	13.40	29.94	•	1239
	SMSUP	7.88	20.61	9.70	47.88	13.94	165
V34	MISSING = 32		·		·	•	
		1	2	3	4	5	TOTAL
	OTHNON			14.66	37.96		1507
	OTHSUP			9.92	52.64	•	625
	SMNON	22.20	24.54	18.72	28.81		1239
	SMSUP	7.88	15.76	14.55	47.88	13.94	165
V35	MISSING = 32	·				·	
			2		4	5	TOTAL
	OTHNON				36.76	5.24	1507
	OTHSUP	5.92	28.00	9.76	49.28	7.04	625
	SMNON	33.09	33.01	12.19	19.77	1.94	1239
•	SMSUP	23.03	33.94	11.52	25.45	6.06	165
V36	MISSING = 35	'	'	•	'	,	
		1	2	3	4	5	TOTAL
	OTHNON	32.14	42.10	12.55	10.42	2.79	1506
	OTHSUP	24.60	45.85	13.42	13.42	2.72	626
	SMNON	20.79	21.20	31.15	21.36	5.50	1236
	SMSUP	13.94		24.85	•	7.88	165

Table C.10--continued

′37	MISSING = 36						
<i>3.</i>		1	2	3	4	5	TOTAL
	OTHNON	9.99	36.22	17.38	30.76	5.66	1502
	OTHSUP	4.34	27.33	11.09	49.04		622
	SMNON	15.62	39.86	15.30	22.95	6.28	1242
	SMSUP	•	-	•		9.04	166
V38	MISSING = 29	,		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		-	
		1	2	3	4	5	TOTAL
	OTHNON	2.72		•	44.99	15.79	1507
	OTHSUP	1.77	25.68	11.24	45.91	15.41	623
	SMNON	2.09	13.03	13.76	44.97	26.15	1243
	SMSUP					29.52	166
V39	MISSING = 30	,				,	
		1	2	3	4	5	TOTAL
	OTHNON	10.76	33.42	17.74	34.68	3.39	1505
	OTHSUP	3.69	21.31	12.18	55.61	7.21	624
	SMNON	18.42	32.50	18.74	27.51	2.82	1243
.	SMSUP	4.22	31.33	18.67	40.36	5.42	166
V40	MISSING = 30	,	,	,	,	,	
• • • •		1			4	•	TOTAL
	OTHNON	28.35	'			1.66	1506
	OTHSUP	8.83	25.52	19.58	40.45	5.62	623
	SMNON	42.64	32.66		7.48	0.80	1243
	SMSUP	16.27		18.07		•	166
		+		r		++	

Table C.10--continued

V41	MISSING = 28		- •				
	*********	1 ++-			•	•	TOTAL
	OTHNON	12.86	39.52	17.37	*	5.17	1508
		3.05	20.22	11.40	53.13	12.20	623
		15.45	34.51	21.24	•	6.60	1243
		6.02	25.90	15.06	44.58	8.43	166
V42	MISSING = 29	•	·	·	4	·	TOTAL
	OTHNON	++- 2.85		•	•	•	1508
		+	- -				
		0.96 ++-	•	•	•	•	624
	SMNON	4.43	•	•	49.28	•	1242
		1.82	3.64	6.06	46.67	41.82	165
V43	MISSING = 30		·	·	•	·	
• • • • • • • • • • • • • • • • • • • •		1					TOTAL
	OTHNON	8.96			50.17	· ·	1507
	OTHSUP	3.37			55.77		624
	SMNON	10.88	•	•		•	1241
		3.61			•	•	166
V44	MISSING = 31		·	•			
*		1	2	3	41	5]	TOTAL
	OTHNON	1.40	4.72	8.78	57.58	27.53	1504
	OTHSUP	0.32	3.04	3.85	55.29	37.50	624
	SMNON	2.41	5.15	10.62	58.89	22.93	1243
	SMSUP	0.60	3.01	4.22	51.20	40.96	166

Table C.10--continued

V45	MISSING = 34						
	[3		5	TOTAL
	OTHNON	18.14	21.00	•	14.62	2.13	1505
	OTHSUP	•	37.08	29.70	12.68	.48	623
		24.58	21.60		10.88	1.37	1241
			29.09	35.15	13.33	2.42	165
V46	MISSING = 30	· .	·		·	·	
		1 ++				5	TOTAL
		12.02		•		3.32	1506
	OTHSUP	•	33.65	14.26	41.35	4.65	624
	SMNON	,	39.37	17.95	18.28	2.74	1242
	SMSUP	16.27	42.17	18.67	18.67	4.22	166
V/. 7	MISSING = 33	, ,		, ,	•	•	
V47	111351110 - 33					5	TOTAL
	OTHNON	9.50	23.79	11.76	37.08	17.87	1505
			26.12	12.50	41.51	15.06	624
	SMNON	•	22.24	14.67	33.04	16.68	1241
	SMSUP	•	30.30	15.15	33.33	15.15	165
V48	MISSING = 35			,		,	
770	iniboling 33	1	2	3	1 4	5	TOTAL
	OTHNON	13.71	31.80	22.95	27.48	4.06	1503
	OTHSUP	11.06	31.89	14.26	37.02	5.77	624
	SMNON	22.79	33.57	19.48	20.05	4.11	1242
	SMSUP	21.95	36.59	19.51	18.90	3.05	164
				•	•	•	

Table C.10--continued

V49	MISSING = 32						
		1	2	3	4	5	TOTAL
	OTHNON	2.46	11.49	3.78	57.30	24.97	1506
	OTHSUP	1.77	8.67	3.53	64.04	21.99	623
	SMNON	3.30	12.56	6.44	55.07	22.62	1242
	SMSUP	0.61	9.09	5.45	55.76	29.09	165
V50	MISSING = 32	1	2	3	4	5	TOTAL
	OTHNON	+- 12.28	33.47	12.62	36.25	5.38	1506
	OTHSUP	++- 4.17	24.24	14.13	48.80	8.67	623
	SMNON	20.61	39.13	14.73	22.54	2.98	1242
	SMSUP	6.67	33.33	17.58	35.15	7.27	165
V51	MISSING = 36	1	21	31	4	5	TOTAL
	OTHNON	 14.89	+	·			1504
	OTHSUP	16.08	53.86	9.65	17.68	2.73	622
	SMNON	15.15	40.77	16.28	21.11	6.69	1241
	SMSUP	14.55	43.03	15.76	22.42	4.24	165
	WIGGING OF	+	+		++	+	
V52	MISSING = 30	1	2	3	4!	5	TOTAL
	OTHNON	1.93	9.83	14.08	40.37	33.80	1506
	OTHSUP	3.51	20.57	16.27	42.11	17.54	627
	SMNON	2.58	5.08	15.81	40.16	36.37	1240
	SMSUP	4.24	10.91	12.12	44.24	28.48	165
	SMNON	2.58	5.08	15.81	40.16	36.37	1240

Table C.10--continued

V53	MISSING = 26						
		1	2	3	4	5	TOTAL
	OTHNON	1.59	6.96	7.95	67.53	15.97	1509
	OTHSUP	0.48	1.11	2.55	67.52	28.34	628
	SMNON	2.90	7.50	12.82	60.56	16.21	1240
	SMSUP	0.61	1.21	4.24	61.82	32.12	165
NE/	MICCINC - 20	+ 	*****				
V34	MISSING = 28	1 1	2	3	4	5	TOTAL
	OTHNON	6.43	8.61	11.07	55.67	18.22	1509
	OTHSUP	1.59	4.62	5.89	56.37	31.53	628
	SMNON	10.02	12.52	15.35	49.84	12.28	1238
	SMSUP	4.24	9.70	10.30	52.73	23.03	165
VEE	MISSING = 26	r			+	+ 	
V > >		1	2	3	4	5	TOTAL
	OTHNON	12.61	35.30	9.62	34.04	8.43	1507
	OTHSUP	4.30	16.56	5.57	52.23	21.34	628
	SMNON	21.34	35.91	10.63	25.60	6.52	1242
	SMSUP	7.88	23.64	4.85	46.67	16.97	165
V56	MISSING = 28	++			+	++	
V 3 0	MISSING - 20	1	2	3	4	5	TOTAL
	OTHNON	9.16	33.91	19.97	32.18	4.78	1507
		2.88	22.04	14.54	50.80	•	
		12.64			27.86	4.19	
		3.03	25.45			9.09	165
		++				++	

Table C.10--continued

V57	MISSING = 28						
		1	2	3	4	5	TOTAL
	OTHNON	3.92	28.14	10.82	36.96	20.17	1507
	OTHSUP	8.61	46.09	10.53	28.23	6.54	627
	SMNON	5.72	21.60	13.30	34.73	24.66	1241
	SMSUP	8.48	31.52	14.55	•	14.55	
V58	MISSING = 27	++			+ -		
		1	2	3	4	5	TOTAL
	OTHNON	7.63	16.51	11.67	51.72	12.47	1508
	OTHSUP	2.87	7.32	7.64	60.67	21.50	628
	SMNON	11.45	22.42	15.73	43.55	6.85	1240
	SMSUP	3.03	16.36	11.52	52.12	•	165
V59	MISSING = 30	,				,	
V 3 3	1133114 - 30] 1]	2	3	4	5	TOTAL
	OTHNON	28.42	44.36	9.96	15.60	1.66	1506
	OTHSUP	17.54	41.63	10.69	25.84	4.31	627
	SMNON	38.63	41.21	9.03	9.68	1.45	1240
	SMSUP	26.67	46.06	8.48	17.58	1.21	165
V60	MISSING = 31	+				r	•
V 00	M1221M2 - 31	1	2	3	4	5	TOTAL
	OTHNON	18.86	39.91	12.95	22.91	5.38	1506
	OTHSUP	9.57	44.66	12.92	27.75	5.10	627
	SMNON	20.82	32.93	20.90	19.94	5.41	1239
	SMSUP	14.55	33.33	20.61	24.85	6.67	165
		+			T	T	-

Table C.10--continued

V61	MISSING = 30						
		1	2	3	4	5	TOTAL
	OTHNON	9.62	26.21	8.43	42.87	12.87	1507
	OTHSUP	3.19	13.58	5.91	57.51	19.81	626
	SMNON	12.98	27.58	13.31	36.94	9.19	1240
	SMSUP	5.45	15.15	13.33	48.48	17.58	165
V62	MISSING = 31						
102		1	2	3	4 [5	TOTAL
	OTHNON	4.12	16.95	15.29	51.93	11.70	1504
	OTHSUP	0.48	6.05	7.96	60.19	25.32	628
	SMNON	6.04	19.18	21.68	44.00	9.11	1241
	SMSUP	1.83	9.76	7.32	53.66	27.44	164
V63	MISSING = 31	,,		,		,	
, , ,		1	2	3	4	5	TOTAL
	OTHNON	14.02	43.65	23.39	15.15	3.79	1505
	OTHSUP	10.86	53.83	17.25	16.29	1.76	626
	SMNON	25.54	42.22	21.03	8.62	2.58	1241
	SMSUP	20.00	52.73	16.36	7.88	3.03	165
V64	MISSING = 31	r				r	
¥04	11351NG = 31	1	2	3	4	5	TOTAL
	OTHNON	9.09	22.89	27.60	29.13	11.28	1507
	OTHSUP	7.18	30.62	20.57	30.14	11.48	627
	SMNON	4.85	10.99	25.28	36.27	22.62	1238
	SMSUP	1.82	13.33	13.33	46.06	25.45	165
					, 	T	-

Table C.10--continued

V65	MISSING = 33						
	1	1	2	3	4	5	TOTAL
	OTHNON	16.81	39.47	27.91	14.75	1.06	1505
	OTHSUP	7.53	48.08	20.03	23.08	1.28	624
	SMNON	20.63	40.45	31.35	6.69	0.89	1241
	SMSUP	12.73	46.06	31.52	•		165
V66	MISSING = 28	, , , , , , , , , , , , , , , , , , ,	+		•	+	mom 4 t
			+		+	5	TOTAL
	OTHNON	18.59	25.50	27.29	27.03	1.59	1506
	OTHSUP	6.21	10.99	12.74	54.46	15.61	628
	SMNON	28.04	24.17	32.39	13.94	1.45	1241
	SMSUP	12.12	13.33	31.52	34.55	8.48	165
V67	MISSING = 34	,					
•07	111001110 34	1	2	3)	41	5	TOTAL
	OTHNON	10.08	27.45	28.12	31.23	3.12	1508
	OTHSUP	2.08	10.08	19.36	55.52	12.96	625
	SMNON	11.31	29.89	27.79	25.12	5.90	1238
	SMSUP	6.13	12.27	20.25	44.79	16.56	163
V68	MISSING = 31	+					
V 00	11551N3 - 31	1	2	3	41	5	TOTAL
	OTHNON	6.49		'	49.57	6.16	1509
	OTHSUP	1.77	19.10	9.95	63.72	5.46	623
	SMNON	7.65	29.15	13.45	43.16	6.60	1242
	SMSUP	3.07	21.47	15.95	53.37	6.13	163
		,			,	1	

Table C.10--continued

V69	MISSING = 29						
		1	2	3	4	5	TOTAL
	OTHNON	2.58	14.98	5.83	50.23	26.38	1509
	OTHSUP	0.96	17.92	7.36	58.40	15.36	625
	SMNON	5.31	22.06	6.76	42.51	23.35	1242
	SMSUP	3.68	34.36	13.50	35.58	12.88	163
V70	MISSING = 33	r=+		+			
• 70	.11001110 - 33	1	2	3	4	5	TOTAL
	OTHNON	7.10	23.56	22.16	40.54	6.64	1507
	OTHSUP	6.56	25.76	17.44	43.52	6.72	625
	SMNON	15.32	28.63	22.98	28.23	4.84	1240
	SMSUP	14.11	27.61	23.31	28.83	6.13	163
V71	MISSING = 31	,	,			,	
***		1	2	3	4	5	TOTAL
	OTHNON	8.35	25.71	17.76	41.68	6.49	1509
	OTHSUP	3.68	20.64	9.76	55.36	10.56	625
	SMNON	18.15	30.40	18.79	26.77	5.89	1240
	SMSUP	9.82	38.04	15.95	34.97	1.23	163
V72	MISSING = 38	,					
* / -		1	2	3	4	5	TOTAL
	OTHNON	1.26	4.32	3.65	65.25	25.51	1505
	OTHSUP	0.64	0.96	1.28	62.72	34.40	625
	SMNON	2.51	6.87	6.95	62.65	21.02	1237
	SMSUP	1.23		3.07		32.52	163

Table C.10--continued

V73	MISSING = 34						
		1	2	3	4	5	TOTAL
	OTHNON	3.19	21.70	20.17	46.25	·	1507
	OTHSUP	1.12	10.08	12.32	61.60	•	625
	SMNON	5.33	21.63	23.24	42.05		1239
	SMSUP	2.45	11.04	16.56	54.60		163
V7 /:	MISSING = 31	,					
V / -	i	1	2	3	4	5	TOTAL
	OTHNON	10.27	30.95	10.54	40.23		
	OTHSUP	2.72	13.62	7.05	60.58	•	624
	SMNON	17.41	34.49	12.01	31.51		1241
	SMSUP	4.29	19.02	10.43	53.37	12.88	163
V75	MISSING = 33	,			,		
V / J			2		4 +	5	TOTAL
	OTHNON				•	8.81	1509
	OTHSUP	2.88	13.76	5.76	61.44	16.16	625
	SMNON	13.41	24.96	11.87	44.10	5.65	1238
	SMSUP					9.82	163
V76	MISSING = 33	,			,		
V76	1135114 - 55	1	2	3	4	5	TOTAL
	OTHNON	8.96	24.22	21.96	40.15	4.71	1507
	OTHSUP	3.37	12.50	9.62	59.62	14.90	624
	SMNON	14.26	26.67	22.97	31.51	4.59	1241
	SMSUP	7.98	17.79	12.88	52.15	9.20	163
					T		

Table C.10--continued

V77	MISSING = 32						
						5	TOTAL
	OTHNON	3.31	17.63	11.66	59.11	•	1509
	OTHSUP	2.40	13.28	6.72	61.44	•	625
	SMNON	7.18	21.87	15.98	48.99		
	SMSUP	6.75	17.79	13.50	52.15	•	163
V78	MISSING = 40	,			·	·	
		++			h	5 +	
	OTHNON					5.58	
	OTHSUP	4.96	23.84	15.04	47.68	•	625
	SMNON	11.17	26.88	28.74	29.47		1235
	SMSUP	7.98	31.29	22.09	34.97	'	163
V79	MISSING = 36	, - ,		,	'		
•••		1	2	3	4	5	TOTAL
	OTHNON	28.15	49.14	12.68	8.50	1.53 +	1506
	OTHSUP	16.00	50.08	13.60	17.28	3.04	625
	SMNON	26.17	41.44	23.10	8.08	1.21	1238
	SMSUP	11.04	38.65	25.15	22.09	3.07	163
V80	MISSING = 36	,			,	, ,	
100	midding 30] 1	2] 3	4	5	TOTAL
	OTHNON	1.06	2.52	7.90	64.08	24.44	1506
	OTHSUP	0.64	0.48	2.40	56.89	39.58	624
	SMNON	1.78	3.55	9.69	60.94	24.05	1239
	SMSUP	0.00	1.84	4.29	51.53	42.33	163
		T		T	,	,	

Table C.10--continued

V81	MISSING = 35						
		1	2	3	4	5	TOTAL
	OTHNON	14.61	31.61	11.29	38.78	3.72	1506
	OTHSUP	7.37	26.28	8.49	51.60	6.25	624
	SMNON	23.21	33.52	13.05	27.64	2.58	1241
	SMSUP	12.96	26.54	8.02		8.02	162
V82	MISSING = 39	, , , , , , , , , , , , , , , , , , , ,		,	7		
		1	2	3	4	5	TOTAL
	OTHNON	25.92	54.83	9.13	8.26	1.87	1501
	OTHSUP	14.06	59.58	9.27	13.42	3.67	626
	SMNON	30.43	46.41	16.55	5.57	1.05	1239
	SMSUP	17.18	51.53	14.72	12.88	3.68	163
V83	MISSING = 42	, ,			,		
103	111001110 - 42	1	2	3	4	5	TOTAL
	OTHNON	9.61	39.63	13.74	28.95	8.07	1499
	OTHSUP	2.24	27.36	9.28	45.28	15.84	625
	SMNON	10.81	33.23	17.02	27.98	10.97	1240
	SMSUP	9.26	37.65	11.11	27.78	14.20	162
V84	MISSING = 43	,			, , , , , , , , , , , , , , , , , , , ,	,	
¥04	11351NG - 45	1	2	3	4	5	TOTAL
	OTHNON	4.27	18.67	11.93	38.13	27.00	1500
	OTHSUP	5.93	41.83	8.17	33.49	10.58	624
	SMNON	3.31	14.05	11.87	35.38	35.38	1238
	SMSUP	7.36	24.54	8.59	38.65	20.86	163
		, 	_ _ _	, = = = = = = = •	, ·	, - - -	

Table C.10--continued

V85	MISSING = 39						
		1	2	3	4	5	TOTAL
	OTHNON	20.80	39.87	11.47	19.27	8.60	1500
	OTHSUP	29.55	41.69	9.27	14.22	5.27	626
	SMNON	14.11	29.11	13.79	26.45	16.53	1240
	SMSUP	22.70	•	12.27	19.02	11.04	163
1104	MICCINC - /1	+				+	
V86	MISSING = 41	1	2	3	4	5	TOTAL
	OTHNON	10.27	23.82	9.14	45.83	10.94	1499
	OTHSUP	1.60	7.99	4.95	52.88	32.59	626
	SMNON	19.13	27.93	11.86	34.06	7.02	1239
	SMSUP	4.91	16.56	7.36		22.09	163
VQ7	MISSING = 39	, , , , , , , , , , , , , , , , , , , ,				,	
VO7		1	2	3	4	5	TOTAL
	OTHNON	10.21	28.02	27.89	31.62	2.27	1499
	OTHSUP	10.38	33.23	17.25	34.19	4.95	626
	SMNON	12.65	25.30	32.31	27.88	1.85	1241
	SMSUP	14.11	26.38	22.70	31.90	4.91	163
V88	MISSING = 39	,				,	
V 00	111551NG = 57	1		3		5	
	OTHNON	12.88		17.14	•		
	OTHSUP			11.50	54.95	9.58	
	SMNON	23.21	36.42	18.86	19.02		1241
	SMSUP	8.59	31.29	•	40.49		163
		T					

Table C.10--continued

V89	MISSING = 40						
		1	2	3	4	5	TOTAL
	OTHNON	4.14	12.75	8.61	57.68	16.82	1498
	OTHSUP	2.08	12.16	9.44	57.92	18.40	625
	SMNON	8.05	21.26	9.02	50.00	11.67	1242
	SMSUP	4.91	17.18	17.18	50.92	9.82	163
V90	MISSING = 40			· • • • • • • • • • • • • • • • • • • •			
V 90		1	2	3	4	5	TOTAL
	OTHNON	5.47	14.00	9.20	56.60	14.73	1500
	OTHSUP	1.44	4.31	5.11	60.06	29.07	626
	SMNON	8.88	18.64	11.62	49.31	11.54	1239
	SMSUP	3.68	10.43	7.36	58.90	19.63	163
VO 1	MISSING = 43	,				,	
V)1	111331NG - 43	1	2	3	4	5	TOTAL
	OTHNON	9.55	24.83	8.14	45.66	11.82	1498
	OTHSUP	2.08	12.32	5.92	60.32	19.36	625
	SMNON	14.85	31.96	11.86	35.43	5.89	1239
	SMSUP	6.13	24.54	6.75	47.24	15.34	163
V92	MISSING = 42	,	,		*****	T	•
V 7 2	MISSING - 42	1	2] 3	4	5	TOTAL
	OTHNON	15.49	34.11	10.35	31.84	8.21	1498
	OTHSUP	4.63	21.88	8.63	54.15	10.70	626
	SMNON	23.16	34.95 	10.90	25.26	5.73	1239
	SMSUP	21.47	26.38	9.82	35.58	6.75	163
		T	T	T	+	T	-

Table C.10--continued

V93	MISSING = 47						
		1	2 [3	4	5	TOTAL
	OTHNON	12.68	25.55	49.30	11.61	0.87	1499
	OTHSUP	6.57	25.96	39.58	25.32	2.56	624
	SMNON	17.56	25.73	40.29	14.97	1.46	1236
	SMSUP	12.96	25.93	29.63	29.01	2.47	162
V94	MISSING = 44	r			r = = = = = - 		•
		1	2	3	4 	5	TOTAL
	OTHNON	17.55	36.96	12.01	30.89	2.60	1499
	OTHSUP	4.48	19.36	8.32	60.32	7.52	625
	SMNON	21.83	38.24	13.18	24.82	1.94	1237
	SMSUP	8.59	24.54	8.59	51.53	6.75	163
V95	MISSING = 45	,				,	•
V 9 3	11351NG 43	1	2	3	4	5	TOTAL
	OTHNON	5.61	22.11	15.23	48.10	8.95	1497
	OTHSUP	1.76	16.61	7.83	58.95	14.86	626
	SMNON	9.30	20.94	20.86	40.34	8.57	1237
	SMSUP	4.29	7.36	17.18	53.37	17.79	163
V96	MISSING = 45	,			,	, , , , , , , , , , , , , , , , , , ,	•
V 90	M1831NG - 43	1	2	3	4	5	TOTAL
	OTHNON	15.33	20.80	17.20	37.87	8.80	1500
	OTHSUP	6.55	12.94	14.06	53.83	12.62	626
	SMNON	20.24	23.32	20.81	29.55	6.07	1235
	SMSUP	8.64	17.90	17.90	45.68	9.88	162
		T			T	r -	•

Table C.10--continued

V97	MISSING = 48						
			-		•	5	TOTAL
	OTHNON	1.14		16.98	63.57	11.97	
	OTHSUP	0.64	3.04	8.16	72.64	15.52	
	SMNON	1.46	5.82	21.83	55.05	•	1237
	SMSUP	0.00	1.85	12.96	63.58	•	162
V98	MISSING = 39	'	·	•		, , , , , , , , , , , , , , , , , , , ,	
	ļ	1			4	5	TOTAL
	OTHNON	1.86	11.95		44.95	9.36	1506
	OTHSUP	4.94	32.70	22.81		5.26	
	SMNON			28.76	45.74	16.08	
	SMSUP			29.09	39.39	•	165
V99	MISSING = 36			,	•	·	
		1 	-	3	4	5	TOTAL
	OTHNON	8.29			39.26	6.37	1508
	OTHSUP	3.68	25.28	8.16	55.52	7.36	625
	SMNON	12.88	35.17	17.99	29.01	4.94	1234
	SMSUP	5.45	29.70	13.33	44.24	7.27	165
V100	MISSING = 32	,	,			,	
1100	111001110 J2	1	2	3	4	5	TOTAL
	OTHNON	7.76	22.48	14.19	49.67	5.90	1508
	OTHSUP	2.23	11.48	7.97	66.83	11.48	627
	SMNON	11.97	25.97	18.45	39.89	3.72	1236
	SMSUP	6.06	19.39	13.33	•		165
		+		·	+	·	

Table C.10--continued

V101	MISSING = 36						
		1	2	3	4	5	TOTAL
	OTHNON	1.59	15.13	14.00	49.77	19.51	1507
	OTHSUP	4.79	38.18	8.63	40.10	8.31	626
	SMNON	2.76	8.27	13.21	46.43	29.34	1234
	SMSUP	4.85	21.82	13.33	42.42	17.58	165
V102	MISSING = 35						
1102	11001110 33	1	2	3	4	5	TOTAL
	OTHNON	33.44	39.22	12.48	13.87	1.00	1507
	OTHSUP	16.61	32.43	13.26	34.03	3.67	626
	SMNON	39.97	35.68	16.75	7.12	0.49	1236
	SMSUP	25.00	34.76	15.85	20.73	3.66	164
7102	MISSING = 32	r+		r		r -	•
V103	M1551NG - 32	1	2	3	4	5	TOTAL
	OTHNON	6.70	19.03	15.45	53.18	5.64	1508
	OTHSUP	2.07	11.64	7.97	65.87	12.44	627
	SMNON	9.22	17.31	18.04	49.51	5.91	1236
	SMSUP	4.85	6.06	15.15	62.42	11.52	165
W10/	MICCING - 26	+ -		+	+	++	•
V104	MISSING = 36	1	2	3	4	5	TOTAL
	OTHNON	11.69	32.87	14.41	22.31	18.73	1506
	OTHSUP	7.97	37.32	+ 8.93	29.98	+ 15.79	627
	SMNON	17.67	27.07	18.07	19.94	 17.26	1234
	SMSUP	15.15	25.45	11.52	24.24	23.64	165
		+		+	+	+	•

Table C.10--continued

V105	MISSING = 42						
		1	2	3	4	5	TOTAL
	OTHNON	12.58	31.23	22.50	18.91	14.78	1502
	OTHSUP	24.64	39.36	15.04	13.44	7.52	625
	SMNON	11.34	23.72	27.21	19.27	18.46	1235
	SMSUP		23.17			14.02	
V106	MISSING = 38						
		1	2	3	4	5	TOTAL
	OTHNON	12.55	20.32	11.29	40.77	15.07	1506
	OTHSUP	4.63	15.95	8.13	52.31	18.98	627
	SMNON	17.05	21.92	13.47	36.36	11.20	1232
	SMSUP	7.27	15.76	10.30	44.85	21.82	165
V107	MISSING = 86	·	·	,	,	,,	
. 20.		1	2	3	4	5	TOTAL
	OTHNON	13.46	14.40	57.13	13.39	1.62	1486
	OTHSUP	15.51	17.29	52.50	12.60	2.10	619
	SMNON	20.76	18.45	53.05	7.00	0.74	1214
	SMSUP	17.79	17.79	52.76	10.43	1.23	163
V108	MISSING = 86	,				γ	
1100	mbbino = 00	1	2	3	4	5	TOTAL
	OTHNON	16.99	23.60	41.74	16.79	0.88	1483
	OTHSUP	15.99	21.32	42.49	18.90	1.29	619
	SMNON	22.51	23.66	43.39	9.86	0.58	1217
	SMSUP	20.86	19.63	49.08	10.43	0.00	163
		, · = = = -	- -	, - -	, ==========	, =======	

Table C.10--continued

V109	MISSING = 87						
		1	2	3	4	5	TOTAL
	OTHNON	25.13	27.96	34.57	11.25	1.08	1484
	OTHSUP	20.58	•			•	617
	SMNON	32.70	25.23		7.07	0.74	1217
		23.93	20.25	44.17	10.43		163
V110	MISSING = 88	1	·	·	·	•	TOTAL
		++		+			
	OTHNON	17.23		50.61		•	1486
		17.05				•	616
	SMNON	22.96	18.52	48.23	9.63	0.66	1215
	SMSUP	17.18	18.40	48.47	14.72	1.23	163
V114	MISSING = 60		·	·			
						5 +	TOTAL
		19.76					1488
	OTHSUP	9.55	15.05	21.04	27.83	26.54	618
	SMNON	22.70	17.61	21.08	18.98	19.63	1238
	SMSUP	16.46	17.07	17.68	18.29	30.49	164
V115	MISSING = 65						
		1 ++	2	3	4	5 	TOTAL
	OTHNON	24.46	19.54	25.40	19.27	11.32	1484
	OTHSUP	12.94	11.97	24.60	24.92	25.57	618
	SMNON	30.56	18.03	23.69	16.09	11.64	1237
	SMSUP	23.17	16.46	16.46	18.90	25.00	164
		•			•		

Table C.10--continued

V116	MISSING = 56						
		1 					TOTAL
	OTHNON	18.39	18.26	25.10	24.16	14.09	1490
	OTHSUP	8.71	10.65	21.29	33.55	25.81	620
	SMNON	21.49	17.37	26.17	22.13	12.84	1238
	SMSUP	14.02	11.59	20.12	27.44	26.83	164
V117	MISSING = 58	1	·	·	·	'	TOTAL
		++-	+	+		+	
	UTHNON	25.39	19.88	24.04 	1/.66	13.03	1489
		26.66 					619
	SMNON	27.38	18.50	24.23	15.67	14.22	1238
	SMSUP	33.54	25.00	15.24	10.37	75.85	164
V118		1					
	OTHNON	28.41	71.59	1482			
	OTHSUP	++- 40.94 ++	59.06	618			
	SMNON	35.42	64.42	1229			
	SMSUP	47.85	52.15	163			
V119	MISSING = 63	1	2	3	4	! 51	TOTAL
	OTHNON	+ 0.74	1.08		59.52	28.85	1487
			+			++	
	OTHSUP	0.16 ++-	0.81	5.68	57.47 	35.88	616
	SMNON	0.57	2.10	12.92	58.24	26.17	1238
	SMSUP	0.00	2.44	7.93	54.88	34.76	164
					, - -	, -	

Table C.10--continued

V120	MISSING = 60						
		1	2	3	4	5	TOTAL
	OTHNON	1.55	3.77	25.08	40.08	29.52	1487
	OTHSUP	0.16	2.42	15.51	46.20	35.70	619
	SMNON	1.78	5.98	27.22	37.24	27.79	1238
	SMSUP	0.00	4.27	19.51		· ·	164
V121	MISSING = 58	++			+ +	+	
V121		1	2	3	4	5	TOTAL
	OTHNON	0.87	3.03	19.23	36.79	40.08	1487
	OTHSUP	0.16	1.94	11.31	40.06	46.53	619
	SMNON	1.69	3.31	19.84	33.87	41.29	1240
	SMSUP	0.00	3.05	13.41	30.49	53.05	164
V122	MISSING = 58	*			,		
,,,,,		1	2	3	4	5	TOTAL
	OTHNON	1.08	3.63	19.17	36.92	39.21	1487
	OTHSUP	0.48	1.29	18.23	43.87	36.13	620
	SMNON	1.13	4.36	23.41	34.95	36.16	1239
	SMSUP	0.61	3.66	18.29	36.59	40.85	164
V123	MISSING = 61	+			T		
V123		1		3		5	
	•	0.81	2.96	15.79	33.20	•	1488
	OTHSUP	0.16	0.65	10.55	36.04	•	616
	SMNON	1.45	2.91	15.09	33.82	46.73	1239
		0.00	1.22	11.59	30.49	56.71	164
		T+			T		

Table C.10--continued

V124	MISSING = 61						
		•	•		,	5	TOTAL
	OTHNON	1.28	2.82	13.24	•	54.64	1488
		0.32	2.42	13.09	31.02	53.15	619
	SMNON	1.86	3.72	16.02	26.54	51.86	1236
	SMSUP	0.61	4.88	20.12	27.44	46.95	
V125	MISSING = 60			·		5	
	OTHNON	1.34				+ 58.24	1487
		+					
		1.62			+	+	
		1.86					1238
	SMSUP	3.05	4.88	25.61	22.56		
V126	MISSING = 61						
		1	2		4	5	TOTAL
	OTHNON	0.67	'	15.01	•	52.62	1486
	OTHSUP	0.48		15.35	•	47.17	619
	SMNON	1.62		•	•		1238
		1.22					
V127	MISSING = 79	1			•	•	TOTAL
	OTHNON	2.43	2.43	 14.66	+ 23.31	++ 57.16	1480
	OTHSUP	5.01	2.26	17.61	+ 25.20	+ 49.92	619
	SMNON	6.52	2.93	19.15	+ 20.05	++ 51.34	1227
	SMSUP	17.79	3.68	23.93	+ 14.72		163
		+			+	++	•

Table C.10--continued

SUPERVISOR ITEMS

V128	MISSING = 8						
						5	TOTAL
	OTHSUP	3.85	35.42	8.49	42.15		624
	SMSUP	1.84	13.50	11.04	52.15	21.47	163
V100		·	•	·	•	•	
V129						5	TOTAL
	OTHSUP	9.40	43.76	8.43	32.25	6.16	617
	SMSUP	13.21	44.65	8.81	30.19	3.14	159
W120	·		7		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
V130	MISSING = 22					5	TOTAL
	OTHSUP	29.11	49.59	5.37	13.82	2.11	615
	SMSUP	25.95	34.81	9.49	25.32		158
Wisi	MISSING = 22				,	, , , , , , , , , , , , , , , , , , , ,	
V131						5	TOTAL
	OTHSUP	14.63	41.30	9.43	33.17	1.46	615
	SMSUP	21.52	39.24	12.03	25.95	1.27	158
V122	MISSING = 22						
V132		1	2	3	4	5	TOTAL
	OTHSUP	20.16	41.63	5.85	27.15	5.20	
						3.16	158
V122	MISSING - 22	,	,		,	,,	
V133	MISSING = 23	1	2	3	4	5	TOTAL
	OTHSUP	5.53	16.59	15.45	52.52	9.92	
	SMSUP	12.10	26.75	21.02	35.67	4.46 4.46	157
		++			+	++	

Table C.10--continued

V134	MISSING = 22						
		1	2	3	4	5	TOTAL
	OTHSUP	12.66					616
	SMSUP		42.68	18.47	18.47	•	
V135	MISSING = 26		·			•	
		1 	2 	3	4 	5	TOTAL
	OTHSUP						
	SMSUP					14.74	
V136	MISSING = 24						
V150	.11331,10 - 24	1	2	3	4	5	TOTAL
	OTHSUP	10.59	28.34	18.89	39.41	2.77	614
	SMSUP	15.92	35.03	29.30	18.47	1.27	157
V137	MISSING = 25				r		
V137		1	2	3	4	5	TOTAL
	OTHSUP				•	•	
	SMSUP	10.83	35.03	17.20	32.48	4.46	157
V130	MISSING = 26			+	+	++	
V136		1	2	3	4	5 	TOTAL
	OTHSUP	•	12.42	4.41	64.22	•	612
	SMSUP	5.73	12.10	10.19	56.05	15.92	157
V120	MISSING = 24	-				r -	,
A 1 3 3		1	2	3	4	5 	TOTAL
	OTHSUP	1.79	16.45	8.79	46.91		614
	SMSUP	1.91	8.92	6.37	45.22	37.58	157
					T		•

Table C.10--continued

V140	MISSING = 25	• 1	0.1	0.1	. 1	- 1	mom 4.t
	 ++	1	2 +	3	4 +	5	TOTAL
	OTHSUP	6.85	•	·	•	•	613
	SMSUP		32.48	16.56	33.12	4.46	157
V141	MISSING = 24	·					
	1	1				5	TOTAL
	OTHSUP		49.19	5.86	16.29	1.30	614
	SMSUP	42.68	43.95	8.28	5.10	0.00	157
V142	MISSING = 18	·	,	,	,	·	
V1-4-2	İ	1				5	TOTAL
	OTHSUP	7.62	28.85	15.56	42.14	•	617
	SMSUP	15.00	33.75	16.88	30.00	4.38	160
V143	MISSING = 18	·	·	,	·	·	
1143	•	1	2	3	41	5	TOTAL
		3.08	19.61		53.97	4.38	617
		13.75	23.13	30.63	29.38	3.13	160
V1/4/4	MISSING = 20	,		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, , , , , , , , , , , , , , , , , , , ,		
1144		1	2	3	4	5	TOTAL
	OTHSUP	15.26	55.36	12.01	14.45	2.92	
	SMSUP	11.32	32.70	15.09	30.82	10.06	159
V145	MISSING = 19	,,	,		,	, ,	
۷ ۲۴۵		1	2	3	4	5	TOTAL
	OTHSUP	6.16	59.64	18.15	14.10	1.94	
	SMSUP	6.29	45.28	24.53	18.24	5.66	159
		T		,		,	

Table C.10--continued

V146	MISSING = 21						
						51 +	
	OTHSUP	14.15	35.93	5.53	40.49	3.90	
	SMSUP	20.75	38.99	8.18	30.19	1.89	159
47		,	,	,	,	,	
V:4/	MISSING = 22					51	TOTAL
	OTHSUP	4.23	16.75	6.99	65.53	6.50	615
	SMSUP	6.33 I	24.05	9.49	56.96	3.16	158
					,	*	
V148	MISSING = 21					51	
	OTHSUP	12.82	43.18	17.86	25.49	0.65	
	SMSUP	17.09	38.61	23.42	20.25	0.63	158
		327					
V149	MISSING = 22						
						5	
	OTHSUP	1.63	22.44	17.24	46.02	12.68	615
	SMSUP	1.90	8.86	15.19	48.10	25.95	158
		,	, , , , , , , , , , , , , , , , , , , ,		,	,,	
V150						5	
	OTHSUP	13.66	29.11	9.43	41.46	6.34	615
	SMSUP	28.48	36.08	6.33	24.05	5.06	158
		· +	+				

Table C.10--continued

BACKGROUND ITEMS

BACKG	ROUND ITEM	S						
V152		1 1						
	OTHNON	++ 5.21	25.76	17.44	51.59 (1479		
	OTHSUP	++ 0.49 ++	9.12	8.47	81.92	614		
	SMNON	8.35 	25.87	17.36	48.43	1210		
	SMSUP	2.50	11.88	10.00	75.63	160		
V153	MISSING		,	·				
		++ 19.16	+	•				
		++	+	-				
		27.82 ++	+	-				
		63.17 +- - +						
		70.00 +						
V154	MISSING	= 2252 1	2.1	TOTAL				
		+ +	+					
		23.64 ++						
		16.37 ++						
	SMNON	28.29	71.71	760				
	SMSUP	40.00 	60.00	110				
		+		-				
V155		1 11						TOTAL
	OTHNON	++ 20.00	10.77	21.54	29.23	6.15	12.31	65
		+ + 18.52						27
		++ 8.80	+	+	+	+	+	216
		++ 11.36	+-	+-	+-	+-	+	44
	5M5UP							44

Table C.10--continued

156 MI	ISSING = 24		21	3	4	51	6	TOTAL
		1 50.66		•			•	1431
		1 53.44 1	·	-	,		· ·	582
	SMNON	1 52.23	0.00	46.31	1.03	0.34	0.09	1166
	SMSUP	60.14	10.81	0.00	0.00 1	29.05	0.00	
	ISSING = 15	1 21	3	4 (5	61	7	
OTHNON	1 0.89	0.96	2.33	10.62	15.76	17.00	29.75	3.77
OTHSUP	0.33	0.00	0.33	1.15	3.95	8.24	22.73	3.13
SMNON	1.17	0.75	4.10	11.56	18.68	14.49	28.14	3.52
SMSUP		0.00	0.65	1.95	5.84	9.09	15.58	2.60
	NTINUED) 9			12	131	141	151	
	•	+		+			+	TOTAL
	10.08	3.08	4.59	1.17	0.00	0.00	0.00	1459
OTHSUP	10.08	3.08	4.59 + 14.99	1.17 18.95	0.00 6.26	0.00 + 2.47	0.00	1459
OTHSUP	10.08	3.08 +	4.59 14.99 5.36	1.17 18.95 0.67	0.00 6.26 0.17	0.00 + 2.47 +	0.00 + 1.15 + 0.08	1459 607
OTHSUP SMNON SMSUP	10.08 14.00 9.97 12.99	3.08 	4.59 14.99 5.36	1.17 18.95 0.67 20.13	0.00 6.26 0.17 7.79	0.00 + 2.47 + 0.00 + 2.60	0.00 + 1.15 + 0.08 + 0.65	1459 607 1194
OTHSUP SMNON SMSUP	10.08 14.00 9.97 12.99	3.08 	4.59 14.99 5.36	1.17 18.95 0.67 20.13	0.00 6.26 0.17 7.79	0.00 + 2.47 + 0.00 + 2.60	0.00 + 1.15 + 0.08 + 0.65	1459 607 1194
OTHSUP SMNON SMSUP	10.08 14.00 9.97 12.99	3.08 	4.59 14.99 5.36 16.88	1.17 18.95 0.67 20.13	0.00 6.26 0.17 7.79	0.00 	0.00 + 1.15 + 0.08 + 0.65	1459 607 1194
OTHSUP SMNON SMSUP	10.08 14.00 9.97 12.99	3.08 	4.59 14.99 5.36 16.88	1.17 18.95 0.67 20.13	0.00 6.26 0.17 7.79	0.00 2.47 0.00 0.00 + 2.60 + 4 26.65	0.00 + 1.15 + 0.08 + 0.65 +	1459 607 1194
OTHSUP SMNON SMSUP	10.08 14.00 9.97 12.99	3.08 	4.59 14.99 5.36 16.88 16.88 20.12	1.17 18.95 0.67 20.13 25.29 23.37	0.00 6.26 0.17 7.79 	0.00 2.47 0.00 0.00 2.60 2.60 2.65 26.65	0.00 + 1.15 + 0.08 + 0.65 + TOTAL 1471 612	1459 607 1194
OTHSUP SMNON SMSUP	10.08 14.00 9.97 12.99	3.08 	4.59 14.99 5.36 16.88 16.88 20.12 20.26	1.17 18.95 0.67 20.13 25.29 23.37	0.00 6.26 0.17 7.79 	0.00 2.47 0.00 0.00 2.60 2.60 2.60 2.614 19.77	0.00 + 1.15 + 0.08 + 0.65 + TOTAL 1471 612 1209	1459 607 1194

Table C.10--continued

9								
		1+	2 	3 	4 ++	5 ++	TOTAL	
	OTHNON	0.54	1.16	21.87	75.54	0.89	1468	
	OTHSUP	2.78	2.29	9.48	85.13	0.33	612	
	SMNON	1 4.23	2.74	17.84	73.86	1.33	1205	
	SMSUP	5.66	1.89	3.14	86.16	3.14	159	
0	MISSING =				·	·		TOTAL
		+	+	+	+	+	+	•
		13.81						
	OTHSUP	11.60	13.56	18.30	19.61	22.39	14.54	612
	SMNON	24.19	13.50	17.23	23.20	18.06	3.81	1207
	SMSUP	14.47	14.47	24.53	27.04	15.09	4.40	159
1	MISSING =		,,	, ,				
		1	2	3	4	5	61	TOTAL
	OTHNON	0.75	16.58	33.90	17.46	26.09	5.23	1472
	OTHSUP	0.00	2.46	17.87	13.61	49.02	17.05	610
	SMNON	2.57	18.74	33.25	18.91	21.72	4.81	1206
	SMSUP	0.62	4.97	18.01	18.63	47.20	10.56	161
2	MISSING =		,					
٤.			2					
	OTHNON	9.00	6.34	12.75	23.18	48.74	1467	
	OTHSUP	8.36	7.38	17.70	29.84	36.72	610	
	SMNON	1 9.55	7.56	12.62	23.17	47.09	1204	
	SMSUP	13.66	12.42	23.60	22.36	27.95	161	
		+		+	·+	+		

Table C.10--continued

V163	MISSING =							
		1	2 ++	31	4	TOTAL		
	OTHNON	64.96	17.86 ++	10.43	6.75	1467		
	OTHSUP	73.53	14.71	7.19	4.58	612		
	SMNON	64.54	15.99	10.60	8.86	1207		
	SMSUP	76.40	++ 9.32 ++	7.45	6.83	161		
V165	MISSING =	158	1 21	TOTAL				
	OTHNON	15.53	84.47	1449				
	OTHSUP	1 2.97	++ 97.03	607				
	SMNON	23.04	++ 76.96	1198				
	SMSUP	6.41	++ 93.59 ++	156				
V166	MISSING =	42		2		4 TOTA +	L	
			.50 15.				0	
	SMSUP	1 20	.92 16. +	99 30.	07 32.	03 15	3	
	MISSING =	43 1	21 3	i 4	1 5	ı 61	7	TOTAL
OTHSUP	1 0.50	1.67	16.86	20.70	43.40	10.18	6.68	599
	1.32	1.97	19.08	34.87	33.55		5.26	

Table C.10--continued

	1 ++					
OTHNON	16.46 	34.18	26.09	11.18	7.24	4.85
OTHSUP	2.68	21.48	40.10	22.65	8.89	4.19
SMNON	11.10	34.88	31.21	10.75	7.95	4.11
SMSUP	++ 5.16 ++	21.94	41.94	17.42	10.32	3.23
MISSING =	225	·		·	·	·
	1 ++		TOTAL			
	49.90 ++		1435			
OTHSUP	71.76 ++	28.24	602			
SMNON	53.73	46.27	1152			
	1 60.39 1	•	154			
	++					
MISSING =	264	+		TOTAL		
MISSING =	264 1 ++ 14.26	2 l + 73.75 l	3			
MISSING = OTHNON OTHSUP	264 1 ++ 14.26 ++ 12.17	2! + 73.75 +	3 + 12.00 + 9.83	1417		
MISSING = OTHNON OTHSUP SMNON	264 1 ++ 14.26 ++ 12.17 ++ 18.87	2! 	3 + 12.00 + 9.83 + 15.08	1417 600		
MISSING = OTHNON OTHSUP SMNON SMSUP	264 1 ++ 14.26 ++ 12.17	73.75 78.00 76.05	3 	1417 600 1134		
MISSING = OTHNON OTHSUP SMNON SMSUP	264 1 1 1 1 26 1 1 2 17 1 2 17 1 1 2 1 1 1 1 1 1	73.75 78.00 76.05	3 	1417 600 1134		
MISSING = OTHNON OTHSUP SMNON SMSUP	264 1 1 1 1 26 1 1 2 17 1 2 17 1 1 2 1 1 1 1 1 1	73.75 78.00 76.05	3 	1417 600 1134		
MISSING = OTHNON OTHSUP SMNON SMSUP MISSING =	264	2 73.75 78.00 78.05 66.05 74.51 2 76.63	3 + 12.00 + 9.83 + 15.08 +	1417 600 1134		
MISSING = OTHNON OTHSUP SMNON SMSUP	264 1 1 ++ 14.26 ++ 12.17 ++ 18.87 ++ 14.38 ++ 574 1 1 1 1 1 1 1 1 1	73.75 78.00 78.00 66.05 74.51 76.63 76.63	3 + 12.00 + 9.83 + 15.08 + 11.11	1417 600 1134		
MISSING = OTHNON OTHSUP SMNON SMSUP MISSING = OTHNON	264	2 73.75 78.00 78.05 66.05 74.51 2 76.63	3 	1417 600 1134		

Table C.10--continued

		11	21	31	4	5	61
	OTHNON	1.33	4.68	6.08	22.64	12.72	34.17
	OTHSUP	0.33	3.32	4.81	17.74	9.45	36.15
	SMNON (0.34	2.58	3.00	15.71	7.90	40.69
	SMSUP	0.00	3.25	1.95	14.29	5.19	38.31
72	(CONTINUED	·	·	·	·	·	·
	OTHNON	10.76	5.17	1.33	0.77	0.35	1431
	OTHSUP		7.79	3.15	4.15	0.17	603
	SMNON	18.97	6.78	2.66	1.20	0.17	1165
	SMSUP						
	SHARE ITEMS		,	+	*	+	+
	SHARE ITEMS MISSING = 1	2206 (ASK	ED AT SAC	TO ONLY)			
	SHARE ITEMS MISSING = :	2206 (ASF +	ED AT SAC	TO ONLY) 2	31	4	5 TOTAI
	SHARE ITEMS MISSING = : SMNON	2206 (ASK + 23.17	ED AT SAC	TO ONLY) 2 -+ 1 17.25	3 -+ 28.1	4 + 7 3.8	5 TOTAI + 33 1200
	SHARE ITEMS MISSING = : SMNON SMSUP	2206 (ASK + 23.17	ED AT SAC 1 -+ 27.58	TO ONLY) 2	3 -+ 28.1 -+ 33.9	4 + 7 3.8 + 5 10.4	5 TOTAL + 33 1200 +
73	SHARE ITEMS MISSING = : SMNON SMSUP MISSING = :	2206 (ASK + 23.17 + 16.05 +	ED AT SAC 1 27.58 5 27.16 	TO ONLY) 2 -+ 1	3 -+ 28.1 -+ 33.9 -+	4 + 7 3.8 + 5 10.4 +	5 TOTAL+++++++
.73	SHARE ITEMS MISSING = : SMNON SMSUP MISSING = : SMNON	2206 (ASK 	ED AT SAC 1 27.58 2 27.16 2 27.16 3 27.16 3 27.16 4 26.19	TO ONLY) 2	3 -+ 28.1 -+ 33.9 -+	4 + 5 10.4 + 4 + 7 3.7	5 TOTAL 33 1200 + 19 162 + 5 TOTAL
.73	SHARE ITEMS MISSING = : SMNON MISSING = : SMNON SMSUP SMNON SMSUP	2206 (ASK 	ED AT SAC 1 27.58 2 27.16 3 27.16 5 27.16 6 26.19 6 26.19 6 25.93	TO ONLY) 2	3 -+ 28.1 -+ 33.9 -+ 23.2 -+ 29.6	4 +	5 TOTAL 33 1200 + 19 162 + 5 TOTAL + 25 1199 +
173	SHARE ITEMS MISSING = : SMNON MISSING = : SMNON SMSUP SMNON SMSUP	2206 (ASK 23.17 16.05 16.05 2207 (ASK 20.10	ED AT SAC 1 27.58 6 27.16 6 27.16 7 26.19 8 26.19	TO ONLY) 2 -+ 1	3 -+ 28.1 -+ 33.9 -+ 23.2 -+ 29.6	4 +	5 TOTAL 33 1200 + 19 162 + 5 TOTAL + 25 1199 +
73	SHARE ITEMS MISSING = : SMNON SMSUP SMNON SMSUP MISSING = : SMNON MISSING = :	2206 (ASK 23.17 16.05 16.05 2207 (ASK 14.20 14.20	ED AT SAC 1 27.58 2 27.16 2 27.16 3 27.16 4 26.19 4 25.93 5 25.93 6 25.93	TO ONLY) 2	3 -+ 28.1 -+ 33.9 -+ 23.2 -+ 29.6	4 + 5 10.4 + 7 3.7 + 3 8.0	5 TOTAL+ 5 TOTAL 5 TOTAL
73	SHARE ITEMS MISSING = : SMNON MISSING = : SMNON MISSING = : SMNON MISSING = :	2206 (ASK 23.17 16.05 -+	ED AT SAC 1 27.58 27.16 2	TO ONLY) 2	3 -+ 28.1 -+ 33.9 -+ 23.2 -+ 29.6 -+	4 +	5 TOTAL 33 1200 + 19 162 + 5 TOTAL + 125 1199 + 5 TOTAL + 15 TOTAL

Appendix D

ADDITIONAL RESULTS FOR QUALITY MEASURES

This appendix presents OLS regression results and annual ALC rates for the measures of work quality discussed in Sec. V of the report. Table D.1 shows regression results for the DSQ measures in Table 25; Table D.2 shows regression results for the DSM measures in Table 26. Dependent variables are as specified in Tables 25 and 26: error rate (as a percentage) for the first 11 measures; RODs initiated as a percentage of receipts and received as a percentage of issues; and, for the last six measures, percent of actions accomplished within time standards (except 2C, high-priority requisitions as percentage of total).

The model used in the regressions is the same in each case. The reference group (intercept) represents the 1985-86 quality level for the comparison ALCs. The "SM8586" coefficient indicates how the 1985-86 quality level at SM-ALC differed from that of the reference group. Similarly, the "SM87" coefficient indicates how the 1987 SM-ALC quality level differed from that of the reference group (1985-86 level). Finally, the "NONSM87" coefficient shows the change in the 1987 quality level for the comparison group relative to its 1985-86 level.

Three significance tests follow the regression results. They evaluate the extent to which the coefficients for the variables in the model differ from each other. The "SMNONSM" test evaluates the significance of the difference between the 1987 results for SM-ALC relative to the 1987 results for the comparison ALCs. The "SM85SM87" test evaluates the 1987 SM-ALC quality level relative to its 1985-86 level. Finally, and of lesser interest, the "SM85NON" test evaluates the difference between the 1985-86 SM-ALC coefficient and the "NONSM87" coefficient (the 1987 results for the comparison ALCs).

For example, the regression results for measure BL7 indicate that the expected error rate for the comparison ALCs in 1985-86 was about 3.4 percent. The SM-ALC error rate in 1985-86 was about 8.9 percentage

points higher (about 12.3 percent) according to the model. This difference was statistically significant (t = 7.89, p < .0001). The 1987 SM-ALC error rate was about 1.7 percentage points higher than the 1985-86 rate for the comparison ALCs (about 5.1 percent). The difference did not quite reach statistical significance (p < .0622). Finally, the 1987 comparison ALC error rate was about 1.7 percentage points lower than its 1985-86 rate (about 1.7 percent). The reduction was significant (t = -2.53, p < .0134).

The significance tests below the regression indicate that: (a) the 1987 BL7 error rate at SM-ALC was significantly higher than the comparison group's 1987 rate (1.66 - (-1.70) = 3.36 percentage points, p < .0001); (b) the improvement in quality at SM-ALC between 1985-86 and 1987 was significant (1.66 - 8.86 = -7.20 percentage points in the error rate, p < .0001); and (c) the 1987 comparison ALC error rate was lower than the 1985-86 SM-ALC error rate (-1.70 - 8.86 = -10.56 percentage points, p < .0001).

Overall, then, the regression results indicate that in 1985-86 the BL7 error rate at SM-ALC was higher than the average rate at the other ALCs. In 1987, the error rate was reduced throughout the system. The improvement at SM-ALC was greater than for the comparison group. Nonetheless, the SM-ALC error rate remained significantly higher than at the other ALCs.

Tables D.3 and D.4 show each ALC's quality rates in 1985, 1986, and 1987 for each measure in Tables 25 and 26, respectively. These are the annual rates referenced in the weighting discussion in Sec. II and combined in the baseline quality analysis. The tables show the average rate for each year and the number of months on which the average is based.

Table D.1

RECRESSION RESULTS FOR DSQ MBASURES

DEP VARIABLE: BL7

						ANAL	ANALYBIS OF VARIANCE	5		
			BOUBCE	8	2	SUN OF SQUARES	POLAN	F VALUE	PROB>F	
			HODEL KREOR C YOZAL	- A	E 17 %	552.34764 323.47881 875.82645	184.11588 4.55603955	40.411	0.0001	
				BOOF HSE DEP IGEAN C.V.		2.134400 3.100796 66.93711	R-SQUARE ADJ R-8Q	0.6307		
						PARA	PARAMETER ESTIMATES	•		
			VARIABLE	2	PAR	Paraketer Estinate	STANDARD ERROR	T FOR HO: PARAMETER=0	PROB > T	
			INTERCEP BUB 5 86 BUB 7 MCMSUB 7		3.39. 1.656	3.39775962 8.86000718 1.65678584 -1.69993353	0.59200049 1.12324196 0.8744268 0.67045426	5.739 7.888 1.895 -2.535	0.0001 0.0001 0.0622 0.0134	
12371	TEST: SPECKEM	MINERATOR: DENOMINATOR:	100.024		111	F VALUE:	21.9542			
TEST	TEST: SM85SM87	MUGGRATOR, DENOMINATOR,	178.359 ii 4.55604	DF:	11	F VALUE:	39.1479			
TEST	TEST: SM85NOW	NUMERATOR: DENOMINATOR:	502.899 1 4.55604	500	12	F VALUE:	110.3807			

Table D.1--continued

	D ep variable, pl4	•				AMAE	ANALYSIS OF VARIANCE	ĸ		
			BOUNCE	8	2	SUN OF SQUARES	SQUARE	P VALUE	PROB>F	
			NODRL KRROR C YOZAL		152	44.61473049 99.67121901 144.28595	14.87157683	22.679	0.0001	
				ROOF MSE DEP HEAM C.V.	ES	0.8097726 1.371532 59.04148	R-SQUARE ADJ R-80	0.3092		
						PARA	PARAMETER ESTIMATES			
			VARIABLE	2	72	Parameter Estinate	STANDARD ERROR	T FOR HO. PARAMETER=0	PROB > 1	
			INTERCEP BARS 56 BAR 7 MORSHR 7		1-0-1-	1.82204800 -1.21261048 -0.10386618 -1.05821821	0.08942443 0.22131416 0.2601673 0.14815015	20.375 -5.479 -0.399 -7.143	0.0001 0.0001 0.6901 0.0001	
7187:	Test Species	MUMERATOR: DENOMINATOR:	8.11857 0.655732	ăă	152	F VALUE:	12.3809			
7687:	TEST: SMS58MB7	MUMERATOR: 0.01331 DENCHINATOR: 0.655732	6.01331 0.655732		152	F VALUE:	12.2204			
TEST	TEST: SMSSNOW	MUMIL ATOR: 0.28453 DENOMINATOR: 0.655732	0.28453	ää	152	F VALUE:	0.4339			

Table D.1--continued

1.54976 DP: 154 PROB >P :	DEP VARIABLE: RL2	PROB>F 0.0001 PROB > F 0.0001 0.0001 0.0001	F VALUE 0.1463 0.1296 T FOR HO! PARAMETER=0 16.954 -3.171 -4.366 -2.378	RCAN BOUARE 13.62827552 1.54975606 1.54975606 ADJ R-BQ ADJ R-BQ BTANDARD BTANDARD BTANDARD BTANDARD 0.13664465 0.30408626 0.39944796 0.23390724 7.9734 7.9734 2.8314		28 De 154 154 154 154 157 154 157 157 157 157 157 157 157 157 157 157	ARIABLE NESSES 12.3569	MAGRATOR: DENOMINATOR: MIMERATOR:
4.38799 DF: 1 F VALUE:	### BOUNCE DF SQUARES SQUARE F VALUE PROBE NOOTEL			0.0945				DENCHINATOR
	BOUNCE DF SQUARE SQUARE F VALUE F SQUARE SQUARE F VALUE F SQUARE SQUARE SQUARE F VALUE F TRROW			2.8314		DF: 154	4.38799	MUMERATOR: DENOMINATOR:
10 2660 AB. 1 0 1/ATCHE.	UNCE DF SQUARES SQUARE F VALUE PROBEDED. DEL. 3 40.88482655 13.62827552 8.794 0.000 ROR 154 238.66243 1.54975606 ROCAL 157 279.54726 ROCAL 157 279.54726 ROCAL 157 279.54726 ROCAL 157 279.54726 ROCAL 157 279.64726 DEP MAN 1.915726 ADJ R-SQUARE 0.1463 DEP MAN 1.915726 DEP	0.0001	-4.366	0.23390724 0.23390724			BH487 BORSH87	
MB586. 1 -0.96430262 0.30408826 -3.171 MB7 1 -1.74395630 0.39944796 -4.366 CMBMB7 1 -0.55621846 0.23390724 -2.378	UNCE DF SQUARE SQUARE F VALUE POLICE SQUARE 154 238.66243 1.54975606 6.794 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0001	16.954	0.13664465			INTERCEP	
MASSE. 1 2.31668358 0.13664465 16.954 16.954 16.954 16.954 17.1395630 0.39944796 -4.366 17.3569 1 -0.55621846 0.23390724 -2.378	SUM OF SQUARE SQUARE P VALUE 3 40.88482655 13.62827552 8.794 154 238.66243 1.54975606 157 279.54726 R-SQUARE 0.1463 MEAN 1.915726 ADJ R-SQ 0.1296 64.98277 R-STINATES	PROB > T	T FOR HO. PARAMETER=0	STANDARD ERROR	rameter 19tinate			
ARIABLE DF ESTINATE STANDARD T FOR HO! RESCR. 1 2.31668358 0.13664465 16.954 MASS. 1 -0.96430262 0.30408826 -3.171 MASS. 1 -1.74395630 0.39944796 -4.366 CMSMS. 1 -0.55621846 0.23390724 -2.378	SUM OF SQUARES SQUARE F VALUE 3 40.88482655 13.62827552 8.794 154 238.66243 1.54975606 157 279.54726 R-SQUARE 0.1463 MEAN 1.915726 ADJ R-SQ			GTER ESTINATES	PARAN			
ARIABLE DF ESTINATE STANDARD T FOR HO: PARAMETER STANDARD T FOR HO: MTSG. 1 2.31668358 0.13664465 16.954 MST. 1 -0.96430262 0.3040826 -3.171 MST. 1 -1.74395630 0.39944796 -4.366 MST. 1 -0.5561846 0.23390724 -2.376	SUM OF PEAN BQUARES SQUARE F VALUE 3 40.88482655 13.62827552 8.794 154 238.66243 1.54975606 157 279.54726		0.1463 0.1296	R-SQUARE ADJ R-SQ	1.244892 1.915726 64.98277	MOOF MER MEP PERAN N.V.	=00	
ARIABLE DF ESTINATE STINATES ARIABLE DF 0.1463 C.V. 64.96277 PARACTER ESTINATES PARACTER ESTINATES ARIABLE DF ESTINATE ERROR PARACTER=0 NATABLE 1 -0.9643026 -3.171 ORSM87 1 -1.74395630 0.3390724 -2.378	SUM OF PURAN DF SQUARES SQUARE P VALUE	0.0001	B . 794	13.62827552 1.54975606	40.88482655 238.66243 279.54726	154 157	HERBORY C. TOT	
NODEL 3 40.88481655 13.62827552 8.794 0.0000		PROB>P	F VALUE	BOUARE	SUN OF		BOUBC	

Table D.1--continued

					_				
	PROBY	0.0001			PROB > [T]	0.0001 0.0001 0.0001			
8	F VALUE	16.423	0.3887	•	T FOR HO: PARAKETER=0	16.000 -5.213 -5.509 -2.678			
AMALYSIS OF VARIANCE	SQUARK	70.97618183 4.32169766	R-SQUARE ADJ R-SQ	PARAMETER ESTIMATES	STANDARD ERROR	0.26191292 0.55560120 0.65478229 0.51481956	8.1189 0.0052	0.8416 0.3609	4.5866
ANAL	SUM OF SQUARES	212.92055 479.70844 692.63699	2.078869 3.077351 67.55386	PARA	Parameter Estimate	4.19050192 -2.89640484 -3.60716859 -1.48141101	F VALUE:	F VALUE:	F VALUE:
	2	1111	HER		a	4444	111	111	111
	ğ	EBECE EBECE C FOTAL	C.V.		à		100	DE	200
	Boneci	MODEL KREOR C TOTA			VARTABLE	INTERCEP BARS S 6 BARS 7 MOMSWB 7	35.0875	3.63733	19.6219
57					-		NUMERATOR: DENOMINATOR:	MUMERATOR: DENOMINATOR:	MUMERATOR: DENOMINATOR:
DEP VARIABLE: BLS							Test: Sphonsh	test: emb59M87	TEST: BM85NOM
							TEST	1831:	1881:

Table D.1--continued

OEC .	DEP VARIABLE: SLI	1				SAMA	ANALYSIS OF VARIANCE	M		
			SOURCE	8	à	SUN OF SQUARES	MEAN	F VALUE	PROB>F	
			HODEL ERROR C TOTAL	3	121	3.58188471 241.62064 245.20253	1.19396157	0.583	0.6313	
				BOOF MBK DEP HEAN C.V.		1.430955 1.713031 83.49451	R-SQUARE ADJ R-BQ	0.0146		
						PARA	PARAMETER ESTIMATES			
			VARIABLE	à	44	Parameter Estimate	STANDARD ERROR	T FOR HO! PARAMETER=0	PROB > T	
			INTERCEP BNG 506 BNG 7 NONSNG 7	пппп	0.00	1.78532764 0.08204721 0.22578347 -0.31505737	0.17748814 0.46653023 0.50893690 0.29469215	10.059 0.176 0.444 -1.069	0.0001 0.8607 0.581 0.2872	
TEST :	TEST: SHOWSM	NUMERATOR: DENOMINATOR:	2.11751	ää	118	F VALUE: PROB >F :	1.0341			
Test	TEST: SK859K87	MJGERATOR: DENOMINATOR:	0.102268 : 2.04763	àà	110	F VALUE:	0.0499			
TEST	TEST: SM85NOW	MUNERATOR: DENOMINATOR:	1.3371	22	110	F VALUE:	0.6530			

Table D.1--continued

	PROB>F	0.0001		
•	P VALUE	16.583	0.2595	
AMALTSIS OF VARIANCE	HEAN SQUARE	9.74277390	R-SQUARE ADJ R-80	PAPAMETER PSTIMATES
AMALY	SCUARES	29.22832169 83.4255315 112.65387	0.766488 1.462568 51.70002	DARAM
	2	142 145	MSR Gan	
	SOURCE	HEDEL ERBOR C TOTAL	BOOT MSE DEP MEAN C.V.	
776				
DEP VARIABLE: S				
ă				

0.0001 0.0001 0.8697 0.0001 PROB > |T| 20.941 -5.451 0.164 -5.402 T FOR HO! 0.08792221 0.19262790 0.24726455 0.15097853 STANDARD ERROR 1.84118365 -1.04993365 0.04063453 -0.81554263 Parameter Kstimate INTERCEP SMS 506 SMS 7 NONSMS 7 VARIABLE

10.7054 0.0013	14.3667	1.2363
DF: 1 F VALUE: 10.7054 DF: 142 PROB >F: 0.0013	F VALUE: 14.3667 PROB >F : 0.0002	F VALUE:
142	DF: 142	DF: 142
	DE	200
6.28948 0.587504	8.44047 0.587504	0.726314
MMERATOR: 6.28948 DENCHINATOR: 0.587504	MEMERATOR: 8.44047 DENOMINATOR: 0.587504	MUMERATOR: 0.726314 DENOMINATOR: 0.587504
Test: Sproken	Test: Sabssabt	TEST: SM85NOW
TEST	TEST	TEST

Table D.1--continued

					=	0271			
	PROBSF	0.1257			PROB > [T]	0.0001 0.2627 0.1502 0.2104			
Ħ	P VALUE	1.939	0.0494		T FOR HO! PARAMETER=0	12.101 1.126 -1.449			
ANALYSIS OF VARIANCE	MEAN	0.36256790 0.18698467	R-SQUARE ADJ R-BQ	PARAMETER ESTIMATES	STANDARD ERROR	0.05996548 0.13408689 0.13848435 0.09159879	0.3567	4.1254	3.6988
ANALY	SUN OF BOUARES	1.08770370 20.94228285 22.02998655	0.4324172 0.683008 63.31071	PARA	Parameter Estinate	0.72563858 0.15095569 -0.20063858 -0.11538217	F VALUE:	F VALUE:	F VALUE:
	2	112	F MSK MEAN		Y W	0000 7.19.1	DF: 112	DF: 112	DF:
	BOURCE	MODEL ERBOR C TOFAL	BOOF DEP H		VARIABLE DP	INTERCEP 1 848586 1 8487 1	NUMERATOR: .0667006 DI DENOMINATOR: 0.186985 DI	MUMERATOR: 0.77138 DI	MUNICIPATION: 0.691625 DI
976							NUMERA DENOMI	MUMERA DENOMI	MUNICIPAL
DEP VARIABLE: SL6							TEST: SMONSM	TEST: SM85SM87	TEST: SM85NON
IV 4300							TEST	TEST	TEST

Table D.1--continued

DEP VARIABLE: TL3

						THAT	ANALYSIS OF VARIANCE	5		
			BOUNCE	8	3	SUN OF SQUARES	SQUARE	P VALUE	PROBY	
			HODEL ERBOR C TOTAL		1396	11.01635917 149.31550 160.33186	3.67211972 1.09790809	3.345	0.0210	
				BOOT NEED DEEP HEADE C.V.	TO THE	1.0478111.169412	R-SQUARE ADJ R-SQ	0.0687		
						PARA	PARAMETER ESTIMATES	•		
			VARIABLE	à	72	Paracter Estinate	STANDARD IRROR	T FOR HO: PARANETER=0	PROB > T	
			INTERCES BHS 586 BHS 7 HORSHS 7	-	4000	1.32321504 -0.84154719 -0.87321504 -0.07104112	0.12019218 0.38946716 0.35247265 0.19573892	11.009 -2.161 -2.477 -0.363	0.0001 0.0325 0.0145 0.7172	
TEST	TEST: SMOONSM	MUNICRATOR: DENOMINATOR:	5.28575 ii 1.09791	ā	136	FROB >F	4.8144			
1887:	1887: SK8 59 KB 7	MUMERATOR: DENOMINATOR:	.0044571	200	136	F VALUE:	0.0041			
TE37:	TEST: SMESNOW	MUMERATOR: DEDICATIVATOR:	4.04562	22	136	P VALUE:	3.6850 0.0570			

Table D.1--continued

DEP VARIABLE: VLI

						TYNT	ANALYSIS OF VARIANCE	M	
			BOTHCE	ij	8	SON OF	BOUARE	P VALUE	PROB>F
			HODEL HEROR C YOFAL		123 126	0.66944873 26.55851163 27.22796036	0.22314958 0.21592286	1.033	0.3012
				BOOF HSE DEP ARAN C.V.	15 E	0.464675 0.3532447 131.5440	R-SQUARE ADJ R-SQ	0.0246	
						PARA	Parameter estimates		
		-	VARIABLE	à	4	Parameter Estimate	STANDARD	T FOR HO: PARAMETER=0	PROB > T
			INTERCEP SM8 5 8 6 SM8 7 MORSH 8 7	-	0000	0.39634595 -0.11160768 -0.25834595 -0.03897095	0.05635012 0.12600270 0.15737732 0.09961388	7.069 -0.886 -1.642	0.0001
7637	TEST: SMONSK	MERCRATOR	0,36667			į	6687		
		DENOMINATOR	0.215923	ā	123	PROB >F	0.1950		
TEST	TEST: BM858M87	NUMERATOR: DENOMINATOR:	0.135573	0 <u>0</u> 0	123	F VALUE: PROB >F:	0.6279		
TEST	TEST: SMESNON	NUMBRATOR: DENONTMATOR:	.0585754	20	123	F VALUE:	0.2713		

Table D.1--continued

Table D.1--continued

	#<8084	0.0001			PROB > T	0.0001 0.0030 0.0109 0.0544			
8	F VALUE	9. 036	0.1451	22	T FOR HO! PARAMETER=0	9.109 -3.018 -2.579 1.940			
ANALTEIS OF VARIANCE	SQUARE	33.544 08 270 4.1744 8 999	R-SQUARE ADJ R-SQ	PARAMETER ESTIMATES	STANDARD ERROR	0.2328933 0.51277544 0.68677737 0.40156240	12.3978 0.0006	0.0798	17.1408
AMAE	SUM OF	100.63465 592.77758 693.41223	2.043157 1.995773 102.3742	PARA	Parameter Estimate	2.12093738 -1.54740270 -1.77093738 0.77906262	F VALUE:	F VALUE:	F VALUE:
	2	142	BOOF HAR DEP HEAD C.V.		2-	4440	DF: 142	F: 142	1
	BOUNCE	HODEL HENOR C TOTAL	0 a a c		VARIABLE DF	INTERCEP 1 8440 5 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	51.7546	0.333110 DF: R: 4.17449 DF:	71.5543 DF: 1
1.3							MAGRATOR: DENOMINATOR:	MUMERATOR: DEDICHINATOR:	KREER TOR :
DEP VARIABLE: VL3							Test, spoken	TEST: SM85SM87	TEST: SW65NOM
DEP VA							1E371	12871	TEST:

Table D.1--continued

DEP VARIABLE, INITE	t	3	FOUNCE	2	ANALA OF SALANDS	ANALYSIS OF VARIANCE OF STAN RES SQUARE	CR F VALUE	PROBY	
			MODEL REBOR C TOPAL	171	0.000347972 0.005062986 0.005410958	0.000115991	3.910	8 600.0	
			,	NO.	0.005441333 0.008135141 66.88677	R-SQUARE ADJ R-80	0.0643		
						PALACETER ESTIMATES	•		
		VARTABLE	2	24	Paraketer Estimate	STANDARD KRROR	T FOR HO: PARANETER=0	PROB > T	
		118758CEP 2445 5 8 6 2443 7 800 248 7		9999	0.008814577 -0.003265645 -0.003908061 0.000064694	0.000567298 0.001268517 0.001670081 0.000968846	15.538 -2.538 0.064	0.0001 0.0109 0.0204 6.046	
TEST: SMONSH	MUNICERATOR: DENOMINATOR:	1.5E-04 E: 3.0E-05	25 25	171	F VALUE:	5.1173			
Test: 84858467	Nederator: Denominator:	3.3K-06 R: 3.0K-05	20 20 20 20 20 20 20 20 20 20 20 20 20 2	171	F VALUE:	0.1099			
TEST: SM65NON	MUMERATOR: DENOMINATOR:	1.7E-04 R: 3.0E-05	50 00 00 00 00	171	F VALUE:	5.8247			

Table D.1--continued

DEP VARIABLE: RECVE

AMALYSIS OF VARIANCE

PROB>F	0.0014			PROB > T	0.0001 0.0136 0.0007 0.5776			
P VALUE	5.466	0.0875		T FOR HO: PARAMETER=0	24.159 -3.494 -3.494 -4.459			
REAL	.00000810941	R-SQUARE ADJ R-SQ	PARAMETER ESTIMATES	STANDARD ERROR	0.000126991 0.000283960 0.000373850 0.000216878	8.9518 0.0032	1.8435	3.6147
BUN OF BOUNES	0.000024328 0.000253704 0.000278032	0.001218051 0.002890863 42.13453	PAR	Paracter Estimate	0.003106099 -0.000708301 -0.001297228 -0.000121016	F VALUE:	F VALUE, PROB >F ,	F VALUE:
2	171			2"	9999	171	171	171
5	SCHOOL STREET	BOOP NSR DEP MEAN C.V.		2		200	200	i i
	PERSON C. SOLL			VARIABLE	INTERCEP BM556 SM67 NONSW97	1.3E-05 1.5 E -06	2.7E-06 1.5E-06	5.4E-06 1.5E-06
				>	-043	W.BCERTOR: DESCRIBATOR:	Menerator: Denoninator:	NUMERATOR: DENOMINATOR:
						TEST: SMOMSH	test: Sn859A87	TEST: SM85WOW
						1631.	TEST	TEST

Table D.2

REGRESSION RESULTS FOR DSM MEASURES

DEP VARIABLE: PIE

AMALYS SCURCE DF SQUARES BECKEL 3 685.96660 ERROR 136 3484.37083 2 C TOTAL 139 4170.33743 ERROR 136 3484.37083 2 C TOTAL 139 4170.33743 ERROR 136 3484.37083 2 C.V. BECKER 5.061657 DEF SEAMETER FARANCEER ENTRACED 1 91.71875000 0 MASS6 1 5.69375000 0 MASS6 1 5.69375000 1 MASS 1 1 5.69375000 1 122.408 DF: 1 5.89375000 1 25.6204 DF: 1 1 F VALUE: 25.6204 DF: 2								TEST: SPENOMEN MUERRATOR: DEMONINATOR:	TEST: SMS5SMS7 NUMERATOR: DENOMINATOR:	TEST: SM85NON MUKRATOR: DENOMINATOR:
SUM OF SQUARE SQUARE FULUE PROBE		anos					Intercep angse6 BNB7 NONSNB7			152.653
### SUM OF HEALM F VALUE PROB ###################################		ŭ	196	C. 4		à				ā
AMALYSIS OF VARIANCE WHERE SQUARE F VALUE PROB 16650 228.65553 8.925 0.00 17083 25.62037377 8.925 0.00 17083 25.62037377 0.1645 2229 R-SQUARE 0.1645 2229 R-SQUARE 0.1661 2229 R-SQUARE R-STIMATES PARAMETER ESTIMATES 87.04.962 1.61477620 7.166 1.59227608 7.704 2.408 LUE: 0.0000 >F: 0.9963 UE: 5.9583		8	136 136			72	5.65 2.32	136	136	136
T VALUE PROB 8.925 0.00 0.1645 0.1645 0.1645 1.146.962 1.146.962 2.408	AWAI	SCIARES	685.96660 3484.37083 4170.33743	5.061657 93.69571 5.402229	PARA	AMETER STIMATE	1375000 1375000 1791667 1708333	F VALUE:	F VALUE:	F VALUE:
T VALUE PROB 8.925 0.00 0.1645 0.1645 0.1645 1.146.962 1.146.962 2.408	YSIS OF VARIAN	MEAN		R-SQUARE ADJ R-SQ	HETER ESTIMATE	STANDARD ERROR	0.63270715 1.41477620 1.59227608 0.96647614	4.7778	0.0000	5.9583 0.0159
PROB>F 0.0001 PROB > T 0.0001 0.0001 0.0001 0.0001	MO	F VALUE	928	0.1645	•	T FOR HO: PARAMETER=0	144-952 9-166 3-704 2-408			
		PROBY	0.0001			PROB > [T]	0.0001 0.0001 0.0003 0.0174			

Table D.2--continued

DEP VARIABLE: PIG

	DEP VARIABLE: PIG	9				ANALI	ANALYBIS OF VARIANCE	Ħ		
				8	ā	SUN OF BOUNES	SQUARE	P VALUE	PROBY	
			MODEL EPROP C TORAL		136	2768.79529 14825.65443 17594.44971	922.93176 109.01216	997.	0.0001	
				BOOF HSE DEP HEAN C.V.	#3	10.44089 75.10857 13.90106	R-SQUARE ADJ R-SQ	0.1574		
						PARA	PARAMETER ESTIMATES			
		,	VARIABLE	2	7	Parameter Estimate	STANDARD	T FOR HO! PARACETER=0	PROB > T	
			INTERCEP BNG 5 86 BNG 7 NORSW8 7		74.51 11.07 3.17	74.51718750 11.87656250 3.17447917 -3.02760417	1.30511114 2.91831722 3.2845766 1.99359019	57.096 4.070 5.967 -1.598	0.0001 0.0001 0.3355 0.1312	
TEST	TEST: SABONSM	MJMERATOR: DENOMINATOR:	369.272	20	136	F VALUE:	3.3874			
1687:	Test: 8M858M87	MUMERATOR: DENOMINATOR:	519.266 109.012	25	136	FROB >F 1	4.7634			
TEST	TEST: SMESNON	MUNCRATOR: DENOMINATOR:	2665.61 109.012	25	136	F VALUE:	24.4524			

2.3897

F VALUE: PROB >F :

131

g G G

125.782 52.6354

NUMERATOR: DENOMINATOR:

TEST: SM85SM87

F VALUE:

DF: 131

MUMERATOR: 100.862 DENOMINATOR: 52.6354

TEST: SHOWSH

0.2638

F VALUE: PROB >F :

131

DF: DF:

13.8862

NUMERATOR: DENOMINATOR:

TEST: SM85NON

Table D.2--continued

DEP VARIABLE: P2C

VARIABLE FAL				TYNY	AMALYSIS OF VARIANCE	5		
	DOS	SOURCE	2	SUM OF SQUARES	MEAN	P VALUE	PROB>F	
		MODEL ERROR C TOTAL	3 131 134	640.91417 6895.24266 7536.15683	213.63806 52.63544012	4.059	0.0086	
		ROOT HSE DEP HEAN C.V.	KSE CZAN	7.255029 30.90797 23.47301	R-SQUARE ADJ R-SQ	0.0850		
				PARA	PARAMETER ESTIMATES	57		
	VARIABLE	à	42	Parajeter Estimate	STANDARD ERROR	T FOR HO: PARAMETER=0	PROB > T	
	INTERCEP SH8586 SN87 NONSM87		64.00 0.400	33.0666667 -2.48520976 -6.82886565 -3.58750000	0.93662017 2.09434636 2.29424149 1.40493025	35.304 -1.187 -2.977	0.0001 0.2375 0.0035 0.0118	

ANALYSIS OF VARIANCE

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DEP VARIABLE: P2D1

		BOOMER	M	2	SUM OF	MEAN	P VALUE	PROBS	
		HODEL KEROR C TOE	NOOKL KRROR C TOTAL	3 171 174	1181.20620 5159.74157 6340.94777	393.73540 30.17392731	13.049	0.0001	
			ROOT MSE DEEP HEAN C.V.	MSK	5.49308 92.53314 5.936338	R-SQUARE ADJ R-8Q	0.1720		
					PARA	PARAMETER ESTIMATES	on:		
		VARIABLE	à	4	Parameter Estinate	STANDARD EBROR	T FOR HO:	PROB > [T]	
		INTERCEP SM8586 SM87 NONSM87		94.5 -7.0 -4.9	94.57291667 -2.01041667 -7.88958333 -4.97756783	0.56063512 1.25361825 1.68190537 1.00798362	168.689 -1.604 -4.938	0.0001 0.1106 0.0001 0.0001	
TEST: SMONSM	MUMERATOR: DENOMINATOR:	79.5563	i do	171	F VALUE:	1.6366 0.1063			
TEST: 3M858M87	NUMERATOR: DENOMINATOR:	276.517	D D	171	F VALUE:	9.1641 0.0029			
TEST: SM85NOW	NUMERATOR: DENOMINATOR:	135.608	000	171	F VALUE:	4.4942			

Table D.2--continued

VEP VARIABLE: P2D2			THRY	ANALYSIS OF VARIANCE	M	
	SOURCE	2	SUM OF BOUARES	MRAN	P VALUE	PROBY
١	HOUSEL ESPOS C FORAL	171 174	637.52734 2228.04043 2865.56777	212.50911 13.02947619	16.310	0.0001
	ECONT DECONT	BOOT HSE DEP MEAN C.V.	3.609637 96.41886 3.743704	R-SQUARE ADJ R-80	0.2225	

PARACTER ESTIMATES

PROB > [T]	0.0001 0.6541 0.0002 0.0001
T FOR HO: PARAMETER=0	265.419 -0.449 -4.0449 -4.048 -6.286
STANDARD KRROR	0.36840699 0.82378307 1.10522097 0.66237058
PARAMETER Estimate	97.78229167 -0.36979167 -4.22395833 -4.16368702
ð	неле
VARIABLE	Intercep Sad 5 66 Sal 5 7 North

0.0026	9.1206 0.0029
F VALUE:	F VALUE:
171	171
1 do	or.
13.0295	118.837
MUMERATOR: DENOMINATOR:	NUMERATOR: DENOMINATOR:
SPENORSH	SM8 5 SM8 7
TEST	TEBT

17.0157
F VALUE:
171
DP:
221.705 13.0295
MUMERATOR: DENOMINATOR:
TEST: SM85NOM

	0.0026	E VALIE.		-	0340807 DF.	AT BUTTO A POOD.	MONCONO
	0.36840699 0.82378307 1.10522097 0.66237058	97.78229167 -0.36979167 -4.22395833 -4.16368702	6 1 1 1 C C C C C C C C C C C C C C C C		Intercep She 5 0 6 Bhe 7 Norshe 7		
:			,	;			

Table D.2--continued

	PROBSF	0.1961		
	P VALUE	1.573	0.0269	
ANALYBIS OF VARIANCE	MEAN	97.50125427 61.97628543	R-SQUARE ADJ R-SQ	PAPAMETER RSTMATES
ANALY	SUM OF SQUARES	10597.94481 61 10890.44857	7.872502 97.37714 8.084548	PARAM
	23	3 171 174	HSE GLE	
	BOUNCE	HODEL ERROR C TOTAL	ROOF MSE DEP MEAN C.V.	
P2D3				
DEP VARIABLE:				
۵				

			VARIABLE DF	J Q	PARE	Parameter Estimate	STANDARD KREOR	T FOR HO! PARAMETER=0	PROB > [T]
			INTERCEP		97.761	145833	0.80348386	121.672	0.0001
			SM87 MONSM87	1 pri pri	-2.640	-0.07812500	2.41045157	-0.032	0.9742
TEST	rest: Sanonsm	NUMERATOR: DENOMINATOR:	52.3594 DF: R: 61.9763 DF:	DF:	171	F VALUE:	0.8448		
TEST	IBST: SM853M87	NUMERATOR: DENOMINATOR:	22.7812 Ri 61.9763	DF:	171	F VALUE:	0.3676		
TEST	TEST: SM85NOW	MUMERATOR: DENOMINATOR:	252.635 Ri 61.9763	D. J.	171	F VALUE:	4.0763		

Table D.3 ANNUAL RESULTS FOR DSQ MEASURES

		MIC			ALC		
		-	00	8	84	- HS	Š
YEAR							
98	187	MEAN		•	•	•	•
		-	0.00	100.0	! ! ! !	} } ! !	
98	BL7	MEAN	0.78	2.69.5			* 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		1 2	3.00	100.8	; ; ; ; ;	5.00	! ! !
37	BL7	MEAN	0.43	, , , ,	i i i i	! ! !	2.57
		3	12.001	11.00	11.00	100.11	

Table D.3--continued

			i		ALC		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
			8	8	48	- NS	\$
YEAR							
65	PL4	MEAN	2.27	2.79	1.73	0.68	2.00
		7	00.6	; ; ; ;			
90	PLA	HEAN	1.66	! ! !	! ! !	0.52	
		2	11.00	11.00			
10	PL4	HEAN	1.03	į			1
		-	12.001		12.001	11.00	1

Table D.3--continued

			1		ALC		
			8	8	SA .	HS.	
YEAR			1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	; ; ; ; ; ; ;
9.0	RL2	MEAN	3.16				2.19
		3	100.6	; ; ;	100.6	100.6	! ! !
90	RL2	HEAN	4.13		i i		
		! ! !	11.00	12.00		:	!
67	RL2	NEAN	2.53		1.50	0.57	1.43
		-	11.00			!	

Table D.3--continued

				!	ALC	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
			3	8	1 48		*
YEAR			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
85	RLS	MEAN	6.47		2.87	1.28	9.69
		3	100.6	:			9.00
86	IRES	MEAN	101.5		† 		3.33
		3	5.001		! ! !		12.00
87	RES	MEAN	1.25	9 30	2.75	0.58	2.58
	_	-	100.4				12.00

Table D.3--continued

	; ; ; ; ; ; ; ;				ALC		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
			30	8	48	- WS	\$
YEAR		1	1				
88	31.1	MEAN	3.44				
		*	8.00		i !		1 1
98	1811	MEAN	3.17		; ; ;		
		2	1.00.		<u>.</u>	 	10.00
87	1361	MEAN	1.74	0.45	0.94	2.01	
		2	12.00				11.00

Table D.3--continued

					ALC		
		 ·	8	8	V8	NS	Z.
YEAR			1		+	+	1
98	814	MEAN	2.02	1.35			1.86
		3	100.6	1	100.6	1	• • •
98	776	MEAN	1.04	1.47	i !	196.0	• • • •
		3	11.00	1	i !		} ! !
0.0	18	HEAN	1.43	1			1
		3	12.00	! !		<u>.</u>	12.00

Table D.3--continued

		_			ALC		
			8	8	84	NS.	£
YEAR							1
6.5	976	MEAN	0.50	0.67	1.04	1.47	
		1	9.00	; ; ; ; ;	! ! !	\ 	; ; ; ;
90	976	HEAN	0.55	105.0		0.36	t
	·	3	1.00.		1.00.7		! ! !
97	976	MEAN	0.37	0.80	; ; ; ; ;	0.52	! ! ! !
		3	12.001	 			12.00

Table D.3--continued

	· · · · · · · · · · · · · · · · · · ·		 		ALC	ALC	
•			8	8	48	- W8	%
YEAR			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	t		
85	11.3	MEAN	3.79			0.13	1.04
		1 2	9	 	! ! :	, 	9.00
98	TL3	MEAN	2.41	!	; !	; ; ;	1.37
		****	100.11	12.00	100.6	9.001	12.00
87	TL3	MEAN	1.56	! !	i	, 1 t 1	1.58
		3	12.00	! !	i	; ; !	12.00

Table D.3--continued

				1	ALC		
		,	8	8	48	- NG	Z.
YEAR	_			·	1	1	1
50	VL1	MEAN	0.32				
		3	100.8	1		! !	
98	VL1	MEAN	0.20	0.41	0.45	0.19) ; ;
		2	11.00	! !	1		11.00
187	VLI	HEAN	0.22				1
		3	100.6) \ \ \ \	11.00

Table D.3--continued

_	 				ALC		
		•	8	8	- A8	NS	\$
YEAR			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
98	VL2	MEAN	00.00				0.12
		1	3.00	3.00	1 1 1 1	 	
96	VL2	HEEN	0.91	!	! ! !	 	0.00
			5.00	; ; ; ;	 	! ! ! !	
101	VL2	HEAN	1.25	: 	00.0	0.00	
		3	4.001	100.0			

Table D.3--continued

					ALC	ALC	1 —— 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
		•	8	8	48	- HS	K
YEAR		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	*	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	VL3	MEAN	0.73				1.33
		7	100.8	100.6	100.6	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00.6
98	VL3	MEAN	2.00	; ; ;	; ; ; ;	;	0.88
		2	10.00	100.11	100.01	100.11	11.00
10	VL3	HEAN	2.61	; ; ;	; ; ;	1 ! !	1.44
	_	2	12.00]	3.001	12.00	100.01	12.00

Table D.3--continued

					AIC	\$ 9 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
			8	8	- WB	- HS	\$
YEAR							
85	INITA	MEAN	0.56	1.07	0.35	0.63	0.04
		2	12.00	•			
98	INITE	HCEAN	0.55	!			
		3	11.00	11.00[11.00	11.001	
67	INITE	HEAL	0.44	1.61			0.74
		2	12.001	! !	12.00 12.00 12.00	12.00	
		4 4 4 4 1 1 1 1 1 1		1	;		

Table D.3--continued

					AIC		
			8	8	1	-	\$
YEAR							
99	EBCV9	SEAS.	0.30				0.34
		-	12.001	12.00	12.00		12.00
•	BECVE	MEAN	0.37				0.38
			11.00[11.00	11.00		11.00
0.	BECT		0.30		!!	0.10	0.30
			12.00	12.00	12.00[

Table D.4 ANNUAL RESULTS FOR DSM MEASURES

					ALC	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
			8	8	- Y8	- WS	M.W.
YEAR							
1985	PIE	MEAN	86.50		88.25		86.25
		3	100.4	!		4.00	
1986	PIE	HEAN	90.33	!	96.67		
		3	12.00	12.00			
1987	PIE	HEAN	92.17	1	98.50	97.62	87.74
			12.00	! ! !	12.00		

able D.4--continued

				ALC	ALC		
			8	8	AS	- WS	E.B.
YEAR				+ + + + + + + + + + + + + + + + + + +			# # # # # # # # # # # # # # # # # # #
1985	P1G	MEAN	55.25	:			70.62
		2	4.00	4.00	4.001		4.00
1986	P1 G	KEAN	65.75			84.79	
		2	12.00				
1987	PIG	MEAN	63.08	64.67	86.08	77.69	72.12
		7	12.00	12.00	12.00		12.00

Table D.4--continued

	•		 		ALC		1
		•	8	8	-	- 16	3
777							
1905	P2C	1421	33.00				36.77
			3.00				3.00
1906	120	NEAN	20.92	33.00			31.40
			12.00				12.00
1967	P2C	HEAN	20.03		30.17	26.24	20.03
		=======================================	12.00	12.00			12.00

Table D.4--continued

					AIC	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1
			8	8	78		\$
TEAR							
1905	1024	200	92.42				
		2	12.00	į			
1906	1024	jeran j	91.75				94.62
			12.00	13.00	12.00	12.00	
1907	1024	j evroj	99.60				91.19
			7.001	į			

Table D.4--continued

					ALC		
	!		8	8	1	- 5	5
77.				1 1 1 1 1 1 1 1 1 1		1	1 1 1 1 1 1 1 1 1
1965	P202	1	97.50		,		98.42
		78	12.00				12.00
1906	1202	1	97.33	99.05	97.25	97.02	96.11
		=	12.00				
1967	7200	-	95.29			93.56	
			7.00	12.00		 	

Table D.4--continued

_					ALC		
			8	8	3	100	\$
77.							
1905	7203		99.00	96.94	97.42		
			12.00		12.00		12.00
1906	P203	1720	100.66	98.00			
		3	12.00				
1907	1203		100.66			97.60	
		=	7.00	12.00	12.00		12.00

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